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**POLARIZED RADIANCE. VOLUME III:  
WAVELENGTH DEPENDENCE OF POLARIZED  
BIDIRECTIONAL REFLECTANCE**

**J. R. Maxwell, et al**

**Environmental Research Institute of Michigan**

**Prepared for:**

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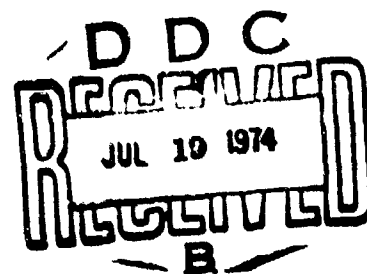
POLARIZED RADIANCE VOL III: WAVELENGTH  
DEPENDENCE OF POLARIZED BIDIRECTIONAL  
REFLECTANCE

Prepared by

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Volume III of this report provides the Ballistic Research Laboratories with a method for extracting information from a limited set of directional and bi-directional reflectance measurements so as to provide a wavelength-corrected input to the volume component of the bidirectional reflectance model described in Volume I. It is shown that the surface component of the bidirectional reflectance has little wavelength dependence for the materials studied from 0.63 $\mu$ m through 3.39 $\mu$ m. Data resulting from extensive measurements performed (Continued on reverse side)		



**Block 20. Abstract**

at 0.63 $\mu$ m, 1.06 $\mu$ m, 3.39 $\mu$ m and 10.6 $\mu$ m under this contract are included and are used for the model validation which is also described.

## FOREWORD

The work reported herein, covering the period 10 April 1972 to 31 May 1973, was carried out by the Infrared and Optics Division of the Environmental Research Institute of Michigan (formerly the Willow Run Laboratories of The University of Michigan), Ann Arbor, Michigan. The work was performed under Contract DAAD05-72-C-0216 for the Army Ballistic Research Laboratories, and was done in three parts, each of which represent one volume.

The three volumes are:

- I - Polarized Bidirectional Reflectance With  
Lambertian or Non-Lambertian Diffuse Component.
- II - Polarized Spectral Emittance From 4 to 14  $\mu\text{m}$ .
- III - Wavelength Dependence of Polarized Bidirectional  
Reflectance.

The internal number of volume III of this report is 192500-1-T(III).

## TABLE OF CONTENTS

FORWORD.....	3
LIST OF FIGURES.....	7
LIST OF TABLES.....	9
1.0 INTRODUCTION.....	11
2.0 MEASUREMENTS.....	16
2.1 Beckman Spectrometer Directional Reflectance Measurements.....	17
2.2 Gonireflectometer Bidirectional Reflectance Measurements.....	21
3.0 MODEL DESCRIPTION.....	23
3.1 Extraction From Directional Reflectance Data.....	26
3.2 Extraction From Bidirectional Reflectance Data.....	28
4.0 MODEL VALIDATION.....	28
REFERENCES.....	50
APPENDIX A: MEASUREMENT DATA FOR A01610, A02022 AND A02023 AT 0.63 $\mu\text{m}$ , 1.06 $\mu\text{m}$ , 3.39 $\mu\text{m}$ AND 10.6 $\mu\text{m}$ .....	51
DISTRIBUTION LIST.....	325

# LIST OF FIGURES

1.	SPECTRAL BIDIRECTIONAL REFLECTANCE FOR GREEN PAINT (SAMPLE NO. 1027) FOR A SPECULAR GEOMETRY WHERE $\theta_i = 55^\circ$ .....	12
2.	SPECTRAL BIDIRECTIONAL REFLECTANCE FOR GREEN PAINT (SAMPLE NO. 1027) FOR A SPECULAR GEOMETRY WHERE $\theta_i = 55^\circ$ .....	13
3.	SPECTRAL BIDIRECTIONAL REFLECTANCE FOR GREEN PAINT (SAMPLE NO. 1027) FOR NORMAL INCIDENCE AND $\theta_r = 50^\circ$ .....	14
4.	SPECTRAL BIDIRECTIONAL REFLECTANCE FOR GREEN PAINT (SAMPLE NO. 1027) FOR NORMAL INCIDENCE AND $\theta_r = 50^\circ$ .....	15
5.	SPECTRAL DIRECTIONAL REFLECTANCE FOR AO 1610.....	18
6.	SPECTRAL DIRECTIONAL REFLECTANCE FOR AO 2022.....	19
7.	SPECTRAL DIRECTIONAL REFLECTANCE FOR AO 2023.....	20
8.	SURFACE COMPONENT OF SPECTRAL DIRECTIONAL REFLECTANCE FOR AO 1610.....	29
9.	SURFACE COMPONENT OF SPECTRAL DIRECTIONAL REFLECTANCE FOR AO 2022.....	30
10.	SURFACE COMPONENT OF SPECTRAL DIRECTIONAL REFLECTANCE FOR AO 2023.....	31
11(a).	FIXED BISTATIC BIDIRECTIONAL REFLECTANCE FOR AO 1610 AT $0.63 \mu\text{m}$ .....	33
11(b).	FIXED BISTATIC BIDIRECTIONAL REFLECTANCE FOR AO 1610 AT $0.63 \mu\text{m}$ .....	34
12(a).	FIXED BISTATIC BIDIRECTIONAL REFLECTANCE FOR AO 1610 AT $1.06 \mu\text{m}$ .....	35
12(b).	FIXED BISTATIC BIDIRECTIONAL REFLECTANCE FOR AO 1610 AT $1.06 \mu\text{m}$ .....	36
13(a).	FIXED BISTATIC BIDIRECTIONAL REFLECTANCE FOR AO 2022 AT $0.63 \mu\text{m}$ .....	37
13(b).	FIXED BISTATIC BIDIRECTIONAL REFLECTANCE FOR AO 2022 AT $0.63 \mu\text{m}$ .....	38
14(a).	FIXED BISTATIC BIDIRECTIONAL REFLECTANCE FOR AO 2022 <sup>2</sup> AT $1.06 \mu\text{m}$ .....	39
14(b).	FIXED BISTATIC BIDIRECTIONAL REFLECTANCE FOR AO 2022 <sup>2</sup> AT $1.06 \mu\text{m}$ .....	40
15.	BIDIRECTIONAL REFLECTANCE MEASUREMENT FOR AO 1610 AT $0.63 \mu\text{m}$ with $\theta_i=0..$	42
16.	BIDIRECTIONAL REFLECTANCE, CROSS-POLARIZED COMPONENT CALCULATION FOR AO 1610 AT $0.63 \mu\text{m}$ WITH $\theta_i=0$ .....	43

17.	BIDIRECTIONAL REFLECTANCE MEASUREMENT FOR AO 1610 AT 0.63 $\mu\text{m}$ WITH $\theta_1 = 40^\circ$ .....	44
18.	BIDIRECTIONAL REFLECTANCE, CROSS-POLARIZED COMPONENT CALCULATION FOR AO 1610 $\mu\text{m}$ WITH $\theta_1 = 40^\circ$ .....	45
19.	BIDIRECTIONAL REFLECTANCE MEASUREMENT FOR AO 2022 AT 0.63 $\mu\text{m}$ WITH $\theta_1 = 0$ .....	46
20.	BIDIRECTIONAL REFLECTANCE CROSS-POLARIZED COMPONENT CALCULATION FOR AO 2022 AT 0.63 $\mu\text{m}$ WITH $\theta_1 = 0$ .....	47
21.	BIDIRECTIONAL REFLECTANCE MEASUREMENT FOR AO 2022 AT 0.63 $\mu\text{m}$ WITH $\theta_1 = 40^\circ$ .....	48
22.	BIDIRECTIONAL REFLECTANCE CROSS-POLARIZED COMPONENT CALCULATION FOR AO 2022 at 0.63 $\mu\text{m}$ WITH $\theta_1 = 40^\circ$ .....	49

LIST OF TABLES

1. POLARIZATION CODE CORRECTIONS FOR 3.39  $\mu\text{m}$  BIDIRECTIONAL  
REFLECTANCE REFLECTANCE AND DATA..... 22
2. ACTUAL RECEIVED POLARIZATION ANGLES FOR 3.39  $\mu\text{m}$   
BIDIRECTIONAL REFLECTANCE DATA..... 24

## 1.0 INTRODUCTION

The comprehensive bidirectional reflectance modeling which has been described in Volume I of this report [1] was performed without regard to wavelength dependence. Measurements were made at 1.06  $\mu\text{m}$ , and model calculations were made on the basis of the fixed bistatic data of those measurements plus the assumption of a purely real index of refraction,  $n = 1.65$ .

Based on measurements made under other contracts [2] there was, at the outset of this effort, reason to believe that the surface reflectance has no discernible wavelength dependence between .63  $\mu\text{m}$  and 1.06  $\mu\text{m}$ . The volume component, however, does.

The foregoing statements are supported by Figures 1 - 4 where the spectral bidirectional reflectance for a green paint is given in two different source-receiver geometries and with two different source polarizations in each case.

Figures 1 and 2 illustrate the situation for a specular geometry with  $\theta_i = \theta_r = 55^\circ$ . For the perpendicular source polarization (Figure 1) the parallel-polarized receiver return is about two orders of magnitude below that of the perpendicular-polarized receiver. In this case, the surface reflectance ( $\rho_{\perp,\perp} - \rho_{\perp,\parallel}$ ) (see Volume I, [1]) is approximately the same as the like-polarized component ( $\rho_{\perp,\perp}$ ) which is seen to be essentially flat between 0.63 and 1.06  $\mu\text{m}$ . (If the cross-polarized component is subtracted out, it becomes even flatter.) Therefore, with a perpendicular-polarized source, the bidirectional surface reflectance in a specular geometry for this sample appears wavelength independent from .63 to beyond 1.06  $\mu\text{m}$ .

The spectral return with a parallel-polarized source (Figure 2) looks different. This is so because at  $\theta_i = 55^\circ$  we are very close to the Brewster angle and the reflectance from a parallel-polarized source nears its minimum. However, in this case too, when the surface component is calculated by subtracting the cross-polarized component from the like-polarized component ( $\rho_{\parallel,\parallel} - \rho_{\parallel,\perp}$ ) it is seen to be essentially wavelength independent

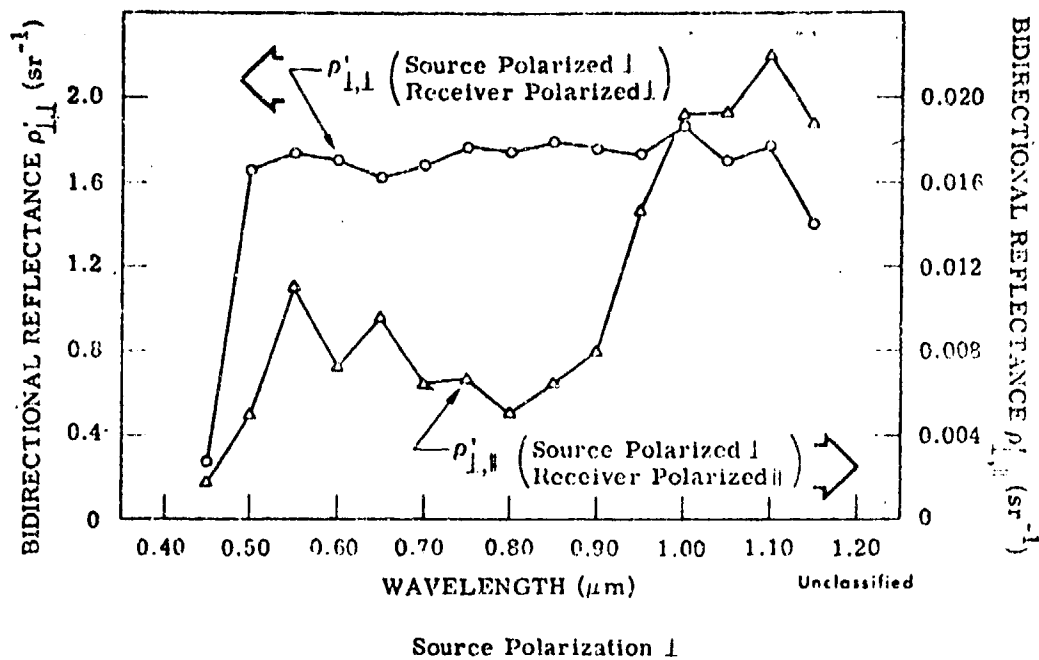


FIGURE 1 SPECTRAL BIDIRECTIONAL REFLECTANCE FOR GREEN PAINT (SAMPLE NO. 1027) FOR A SPECULAR GEOMETRY WHERE  $\theta_i = 55^\circ$



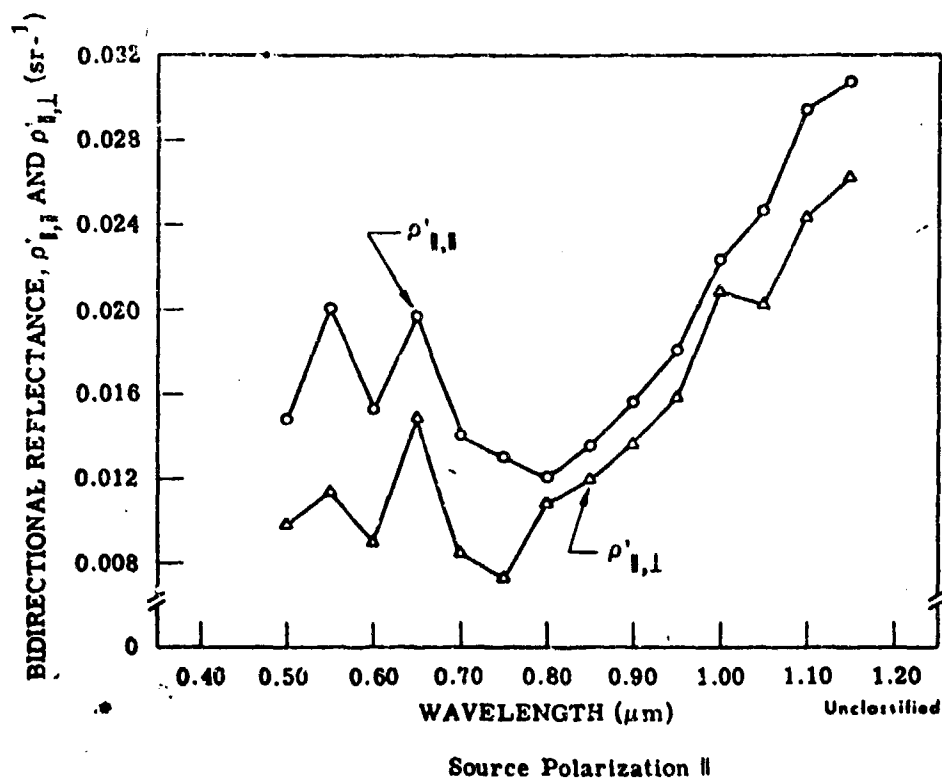


FIGURE 2 SPECTRAL BIDIRECTIONAL REFLECTANCE FOR GREEN PAINT (SAMPLE NO. 1027) FOR A SPECULAR GEOMETRY WHERE  $\theta_i = 55^\circ$

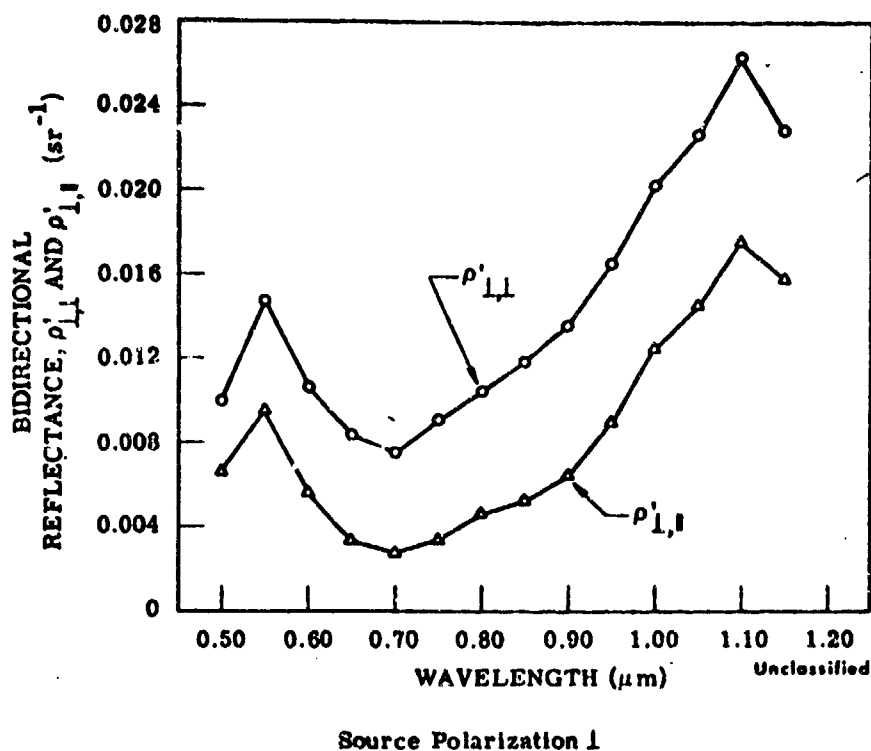


FIGURE 3 SPECTRAL BIDIRECTIONAL REFLECTANCE FOR GREEN PAINT (SAMPLE NO. 1027) FOR NORMAL INCIDENCE AND  $\theta_r = 50^\circ$

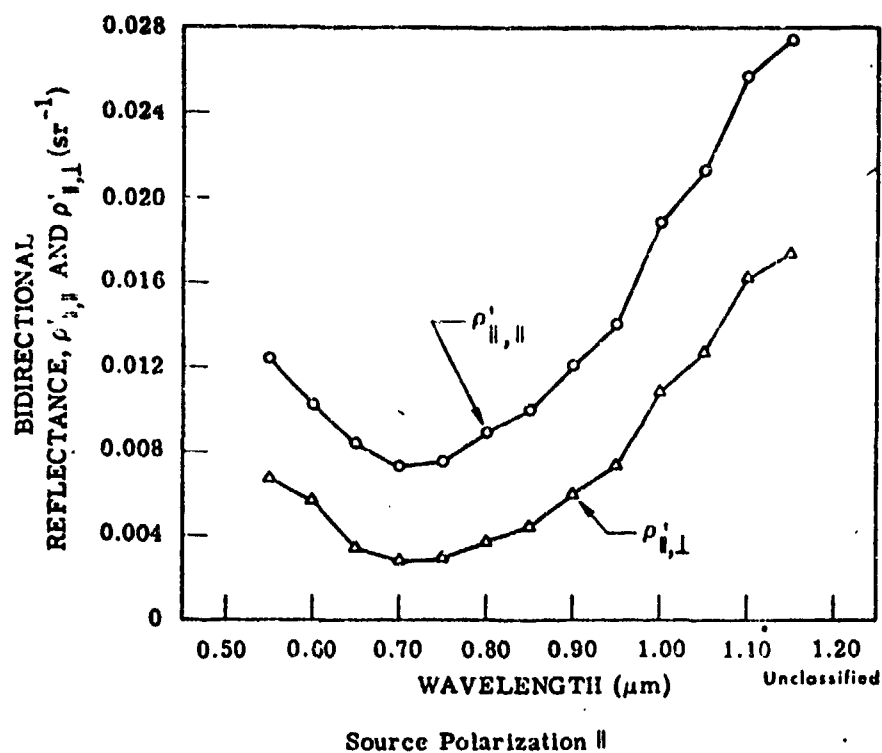


FIGURE 4 SPECTRAL BIDIRECTIONAL REFLECTANCE FOR GREEN PAINT (SAMPLE NO. 1027) FOR NORMAL INCIDENCE AND  $\theta_i = 50^\circ$

between .63 and 1.06  $\mu\text{m}$ . However, it is obvious in both Figure 1 and Figure 2 that there is a spectral dependence in the volume, or cross-polarized, component itself.

The same sample is described in Figure 3 and 4 with a different source-receiver geometry; this time  $\theta_i = 0$  and  $\theta_r = 50^\circ$ . Now the case with perpendicular source polarization (Figure 3) looks almost identical to that with parallel source polarization. In both cases, the surface component ( $\rho'_{\alpha\alpha} - \rho'_{\alpha\beta}$ ) is clearly flat throughout the graph, while the volume (cross-polarized) component contains the spectral dependence. It will be seen in Section 2 that a similar situation exists for the samples studied in this work.

The program for this modeling effort was to assume that the wavelength variation of the volume component of the bidirectional reflectance was the same as that for the directional reflectance. If the bidirectional volume reflectance for a given surface is known at one wavelength and the directional reflectance can be obtained at that wavelength and a second wavelength, then the bidirectional volume reflectance for the second wavelength can be obtained from:

$$\rho'_V(\theta_i, \phi_i, \theta_r, \phi_r; \lambda_2) = \frac{\rho_D(\lambda_2)}{\rho_D(\lambda_1)} \rho'_V(\theta_i, \phi_i, \theta_r, \phi_r; \lambda_1)$$

Description of the model is given in Section 3 and of the validation in Section 4. Measurement data are discussed in Section 2.

## 2.0 MEASUREMENTS

The purpose of the measurement program was to obtain sufficient data to validate the model and to extract input information, based on wavelength dependence, for the RHOPRIME program described in Volume I. In particular, it was important to determine a) the surface reflectance dependence on wavelength in the wavelength region of .63  $\mu\text{m}$  to beyond 3.39  $\mu\text{m}$  and, b) whether the assumption that the bidirectional reflectance varies as the directional reflectance in the volume component is valid.

To accomplish the above objectives extensive measurements were performed on three different sample surfaces at four different wavelengths. The samples are code-numbered: A01610, A02022, and A02023. All are metallic surfaces coated with varying shades and textures of green paint.

The measurements carried out under this contract were bidirectional reflectance measurements performed on the ERIM gonireflectometer [3]. However, in order to determine directional reflectance ratios, it was necessary to have direct directional reflectance measurement data. Such measurements have been performed by ERIM on the same samples with a Beckman DKII spectrometer under other contracts. (Samples A02022 and A02023 were measured under Contract DAAF03-72-C-0115 with Rock Island Arsenal [4] while Sample A01610 was measured under Contract F33615-68-C-1281 with the Air Force Avionics Laboratory [5].)

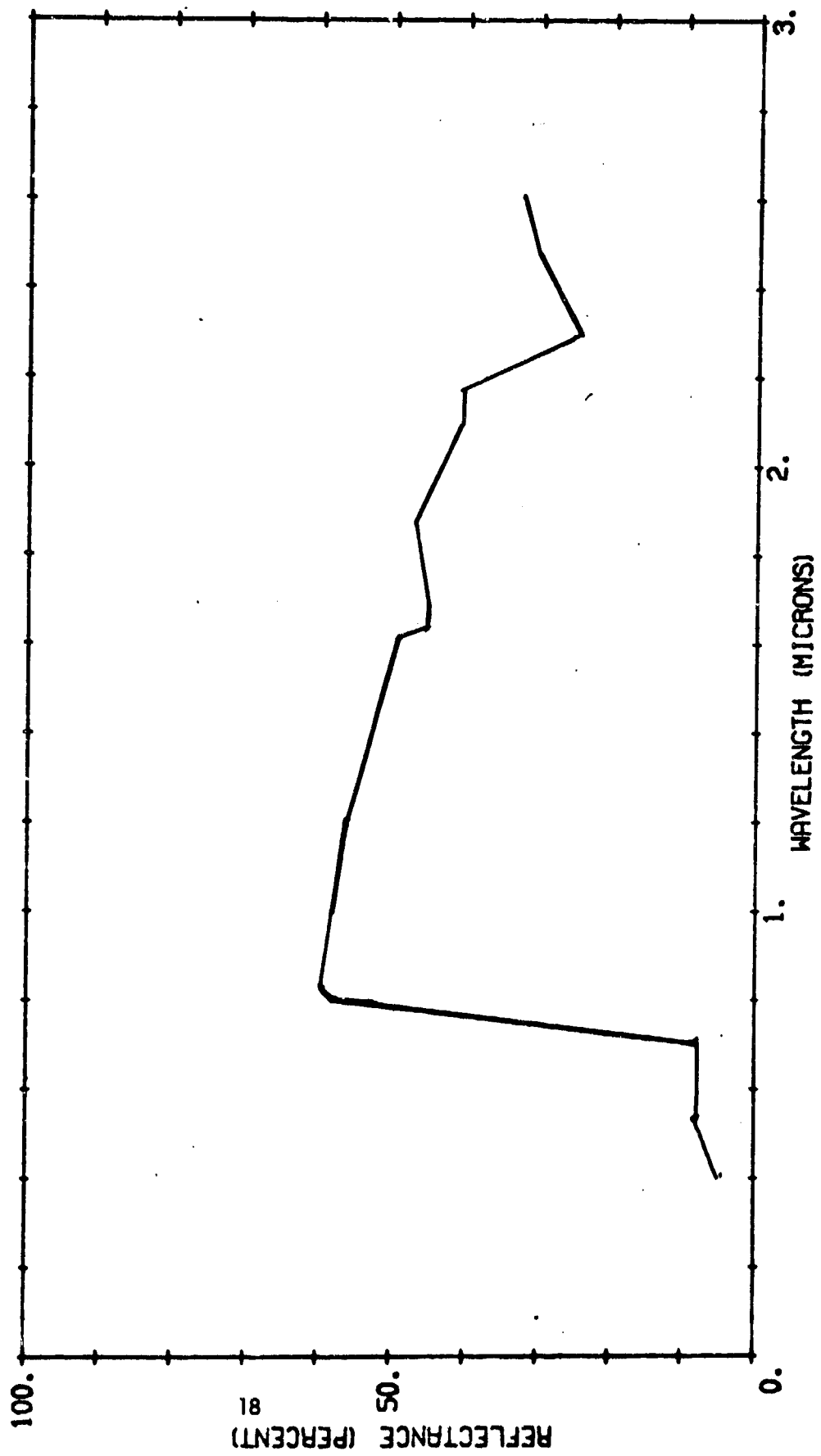
#### 2.1 Beckman Spectrometer Directional Reflectance Measurements

The purpose of these measurements was to obtain data for  $\rho_D(\lambda)$  so that the ratio of the directional reflectances at two different wavelengths could be used to predict the bidirectional reflectance at one of the wavelengths, given the bidirectional reflectance at the other. (The description of the model is detailed in Section 3.)

Figures 5, 6, and 7 show the directional reflectance measurements from .4  $\mu\text{m}$  to 2.6  $\mu\text{m}$  for samples A01610, A02022 and A02023, respectively. All three samples are shades of green in color and should be expected to increase reflectance sharply in the green wavelength range. That this happens between about .49 and .53  $\mu\text{m}$  is shown in all three figures. In the infrared, A01610 becomes extremely bright at about .75  $\mu\text{m}$  and remains highly reflecting to the 2.6  $\mu\text{m}$  limit of the Beckman measurement. Both A02022 and A02023 show no further rise beyond the increase at .49  $\mu\text{m}$ .

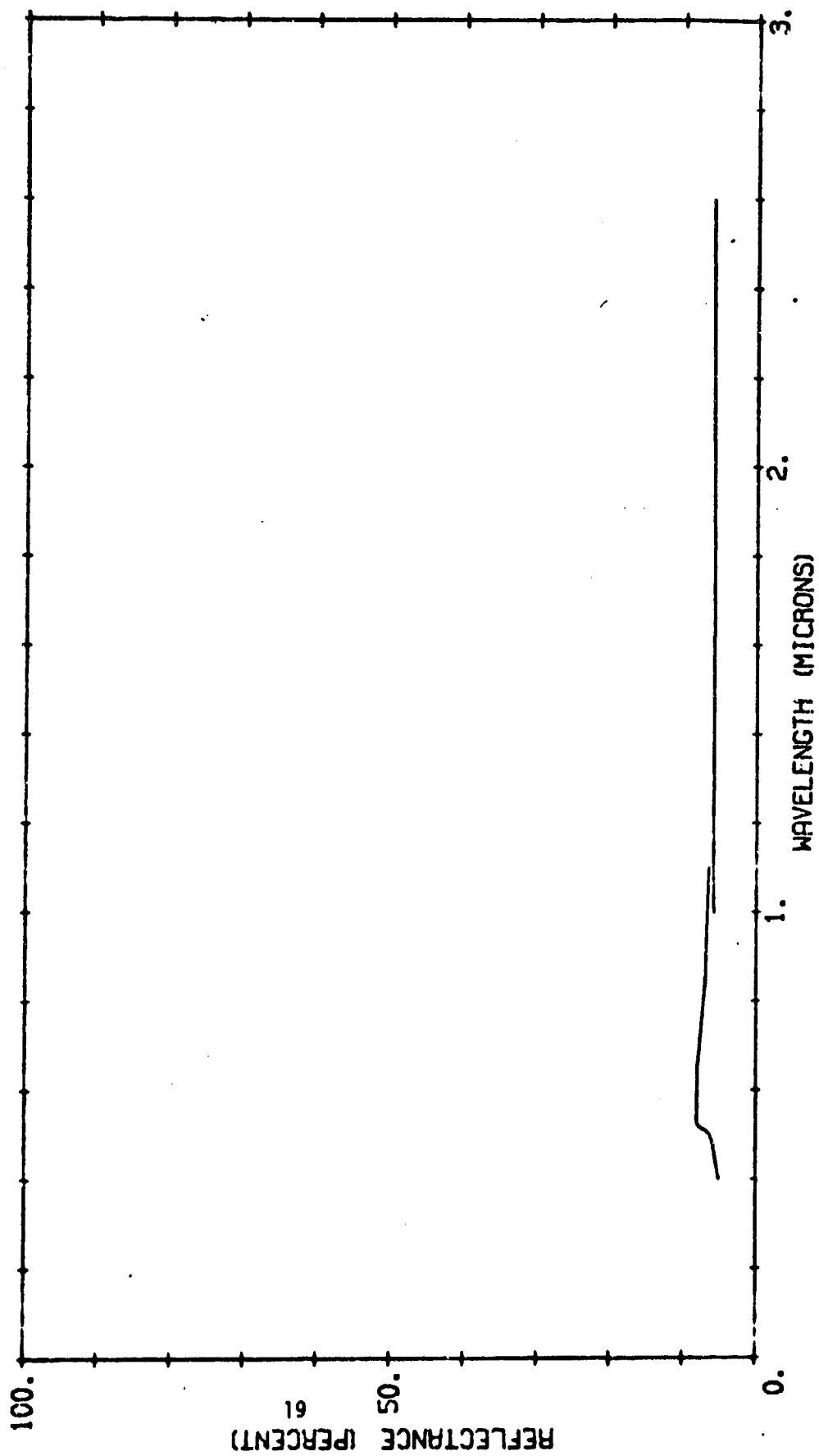
In all three cases, reflectance includes both surface and volume contributions and further reduction had to be performed before the data could be used.

A01610 002

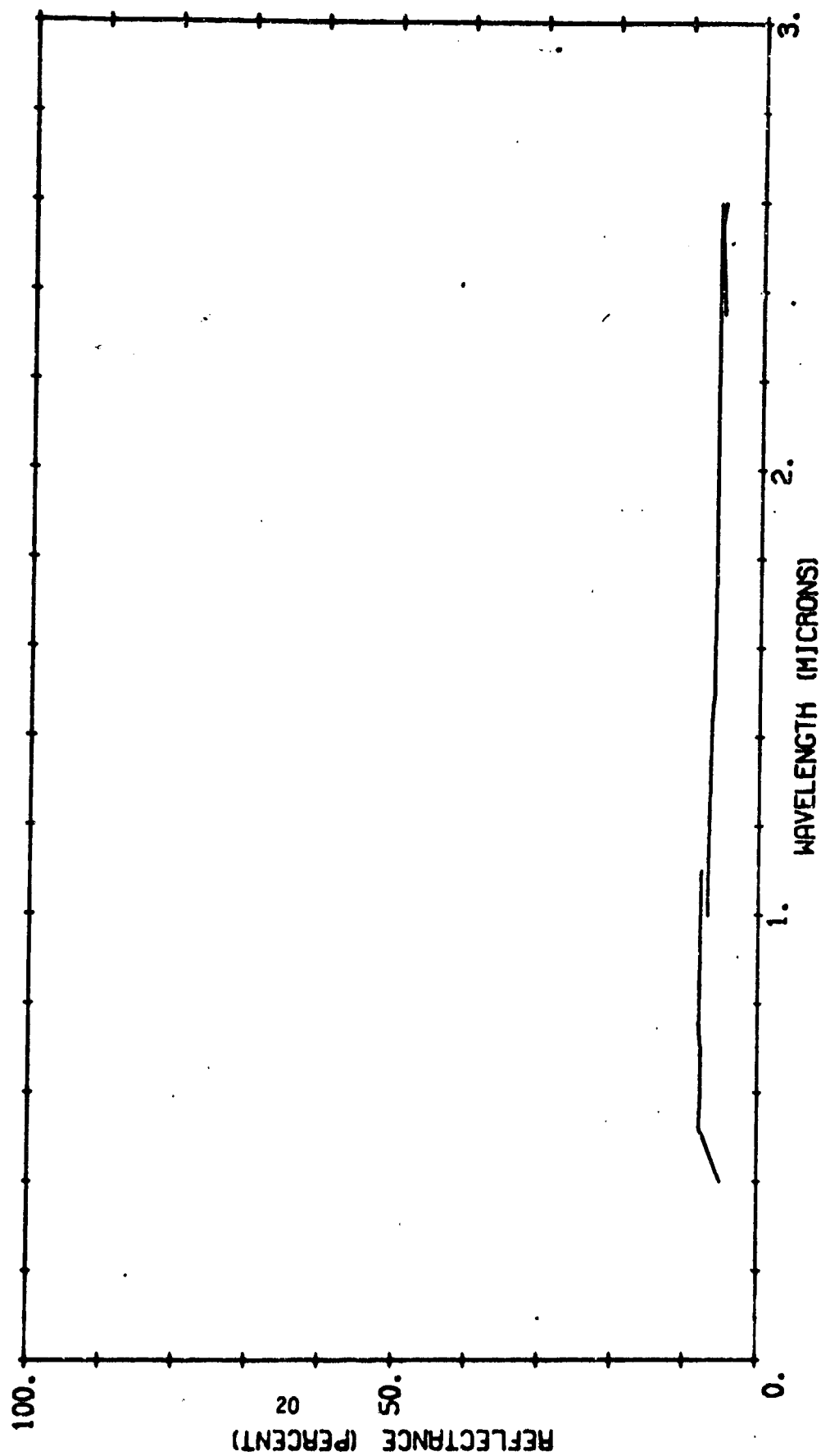


A02022 001

FIGURE 6



A02023 003





## 2.2 Gonioreflectometer Bidirectional Reflectance Measurements

Data from the bidirectional reflectance measurements are given in Appendix A. When using the bidirectional reflectance data, the following observations should be noted:

1. There is no significant variation of the surface component of  $\rho'$  as a function of wavelength between 0.63  $\mu\text{m}$  and 1.06  $\mu\text{m}$ . (There are, however, significant variations in the volume components in the same spectral region.) That a linear relation is reasonable between 0.63  $\mu\text{m}$  and 10.6  $\mu\text{m}$  is discussed in section 4 where it is shown that for sample A01610, the greatest error is about 40% and for the other two samples, the greatest error is about 17%. Therefore, we conclude that for the surface component there is no more than a weak wavelength dependence which is approximately linear with a small enough slope that variations are not significant between 0.63  $\mu\text{m}$  and 10.6  $\mu\text{m}$ .
2. For Samples A01610 and A02022, the volume component varies with wavelength and the measurements are unambiguous and suitable for parameter extraction at 0.63  $\mu\text{m}$  and 1.06  $\mu\text{m}$ . However, at 3.39  $\mu\text{m}$  and 10.6  $\mu\text{m}$ , the volume component falls to below the noise level of the system and hence cannot be used for validation. At 0.63  $\mu\text{m}$  the volume component for Sample A02023 is also below the system noise and therefore this sample was not used in the validation.

The result is that two samples (A01610 and A02022) were used for model validation at two wavelengths (0.63  $\mu\text{m}$  and 1.06  $\mu\text{m}$ ).

3. Difficulties encountered in aligning the receiver polarization analyzer for the 3.39  $\mu\text{m}$  measurements make necessary the following corrections when working with the data:
  - a) All  $\pm 45^\circ$  source polarization data must be multiplied by a scale factor of 0.38.
  - b) Polarization symbols on the 3.39  $\mu\text{m}$  data are incorrect because of the alignment problems. Table 1 shows what the symbols, as they are, represent and what the correct symbols (with their representative polarizations) should be.

TABLE 1. POLARIZATION CODE CORRECTIONS FOR 3.39  $\mu\text{m}$   
BIDIRECTIONAL REFLECTANCE AND DATA

<u>Present Code</u>	<u>Correct Code</u>
• ( $\perp$ , 45)	$\diamond$ ( $\perp$ , -45)
$\times$ ( $\parallel$ , 45)	K ( $\parallel$ , -45)
X (45, $\perp$ )	A (-45, $\perp$ )
B (45, 45)	M (-45, -45)
$\square$ (45, $\parallel$ )	$\star$ (-45, $\parallel$ )
$\diamond$ ( $\perp$ , -45)	$\ast$ ( $\perp$ , 45)
K ( $\parallel$ , -45)	$\times$ ( $\parallel$ , 45)
A (-45, $\perp$ )	X (45, $\perp$ )
M (-45, -45)	B (45, 45)
S (-45, $\parallel$ )	$\square$ (45, $\parallel$ )

c) Nominal receiver polarization angles are presented with the actual polarization angles in Table 2.

Because the receiver is not really at  $90^\circ$  ( $||$ ) when so referred to, there is no pure cross-polarized measurement with the source at  $0^\circ$  ( $\perp$ ). Therefore, there appears to be a larger cross-polarized component than there should be in these cases. The increase, however, really represents that part of the  $0^\circ$  polarized return which is not stopped by the analyzer and should be disregarded.

4. In the fixed bistatic data for Sample A02022 at  $3.39 \mu\text{m}$  it should be noted that the  $\perp, \perp$  component truncates at about  $\theta_r = 7^\circ$  because of instrumental saturation.

### 3.0 MODEL DESCRIPTION

The wavelength dependence model for the volume component of the bidirectional reflectance is based on the assumption that the volume bidirectional reflectance varies with wavelength in the same manner as the directional reflectance. (This assumption has been discussed in [2].) The plausibility of this assumption is borne out by the measurements as described in Section 2. Therefore, if we are able to obtain the directional reflectance,  $\rho_D(\lambda)$ , at two wavelengths, we can take the ratio of the two and say that the volume bidirectional reflectance varies by the same ratio. In mathematical terms:

$$\rho'_V(\theta_1, \phi_1, \theta_r, \phi_r; \lambda_1) = \frac{\rho_D(\lambda_1)}{\rho_D(\lambda_2)} \rho'_V(\theta_1, \phi_1, \theta_r, \phi_r; \lambda_2)$$

where  $\rho'_V$  is the volume component of the bidirectional reflectance.

As shown in Volume I, the volume component of the bidirectional reflectance always contains a multiplicative factor,  $\rho_V$  in the non-Lambertian case and  $\rho_\chi$  in the Lambertian case, where  $\rho_V$  (or  $\rho_\chi$ ), is a constant model parameter which is extracted from a fixed-bistatic bidirectional reflectance scan.

TABLE 2.

Actual Receiver Polarisation Angles for 3.39  $\mu\text{m}$   
Bidirectional Reflectance Data

<u>Nominal Polarisation Angle</u>	<b>FIXED BISTATIC</b>	<u>Actual Polarisation Angle</u>
0 ( $\perp$ )		-7
-45		-58.5
-90 ( $\parallel$ )		-90
	<b>IN-PLANE</b>	
0 ( $\perp$ )		0
+45		+41.5
+90 ( $\parallel$ )		+83
	<b>OUT-OF-PLANE</b>	
0 ( $\perp$ )		0
+45		+41.5
+90 ( $\parallel$ )		+83

Therefore, the wavelength dependence is included in the model as a wavelength dependent variation of the parameter,  $\rho_v$  (or  $\rho_x$ ), which is extracted from directional reflectance data. No modification of the model as described in Volume I is necessary.

#### Parameter Extraction

The model depends upon the assumption that the surface bidirectional reflectance (also the surface directional reflectance) varies linearly with wavelength. Under this assumption, if one knows the surface reflectance at two points, it is possible to interpolate at any point in between. Therefore, it is possible to eliminate the surface component from the directional reflectance at any point. The volume directional reflectance is then used to construct the ratio of directional reflectances at two wavelengths. This ratio is then used to derive the bidirectional reflectance at one of the wavelengths if it is known at the other.

The parameter to be extracted consists of the directional reflectance ( $\rho_D$ ) at two different wavelengths for a material of interest. It is clear that measurements on a spectrometer such as the Beckman DKII are ideal for this purpose, if they can exclude the surface component or if it can be determined independently and eliminated.

Alternatively, the same information can be extracted from bidirectional reflectance measurements, preferably from a bidirectional scan where the source is normal to the target plane ( $\theta_i = 0$ ). In this case one works only with the cross-polarized components ( $\rho'_{\perp,||}$  and  $\rho'_{||,\perp}$ ) and integrates (or sums) over all receiver angles to get return.

As will be shown later in this section, the two methods yield the same results to within about 10%. The agreement is important because it tends to verify the reliability of the method, which means that one has a way to predict bidirectional reflectance wavelength dependence as long as a directional reflectance spectral scan and a bidirectional scan with normal source is available. Details of procedures follow.

### 3.1 Extraction From Directional Reflectance Data

It has been stated earlier that the directional reflectance measurement includes a surface reflection component which must be eliminated. This can be done if independent data are available from which the surface component can be taken. In the case of this work, the information is included in the bidirectional reflectance measurement of the surface component, i.e. the like-polarized component ( $\rho'_{\perp\perp}$  or  $\rho'_{||\perp}$ ). However, there is a non-surface contribution present in the like-polarized components which must first be subtracted out [1]. Also, since an unpolarized directional reflectance can be regarded as a sum of perpendicular and parallel polarized reflectances, we average over both of these cases in the bidirectional reflectance data and obtain:

$$\rho'_{\text{surface}} = \frac{\rho'_{\perp\perp} + \rho'_{||\perp}}{2} - \frac{\rho'_{\perp||} + \rho'_{||\perp}}{2}$$

where  $\rho'_{\text{surface}}$  is the surface contribution of the bidirectional reflectance. To obtain the surface contribution to the directional reflectance,  $\rho'_{\text{surface}}$  must be integrated or summed over the entire hemisphere so that, [3]:

$$\rho_{\text{surface}} = \int \rho'_{\text{surface}}(\theta_1, \phi_1, \theta_r, \phi_r) \sin\theta_r \cos\theta_r d\phi_r d\theta_r$$

If we now make the reasonable assumption that there is no  $\phi$  - dependence in  $\rho_D$ , then:

$$\rho_{\text{surface}} = 2\pi \int \rho'(\theta_1, \phi_1, \theta_r, \phi_r) \sin\theta_r \cos\theta_r d\theta_r$$

Since there is no easily expressible analytical form for  $\rho'$  it is necessary to resort to numerical or graphical methods. The method actually used was graphical and is described in [3]. Using a bidirectional reflectance scan with  $\theta_1 = 0$ , the functions

$$\frac{\rho'_{\perp\perp}(\theta_r) + \rho'_{||}(\theta_r) - \rho'_{||\perp}(\theta_r) - \rho'_{\perp||}(\theta_r)}{2} \sin\theta_r \cos\theta_r$$

was plotted on linear graph paper every 5° for each wavelength of interest. A planimeter was then used to obtain a relative area (or integration) for each plot.

Let  $\rho_d(\lambda_1)$  = area of volume component (cross-polarized) plot for wavelength  $\lambda_1$ .

$\rho_s(\lambda_1)$  = area of surface component (like-polarized minus cross-polarized) plot for wavelength  $\lambda_1$ .

Then:

$$\rho_D(\lambda_1) = \left[ \frac{\rho_d(\lambda_1)}{\rho_s(\lambda_1) + \rho_d(\lambda_1)} \right] \rho_{DB}(\lambda_1)$$

where

$\rho_D(\lambda_1)$  is the true directional reflectance for  $\lambda_1$ , and

$\rho_{DB}(\lambda_1)$  is the directional reflectance including the surface component as measured in the spectrometer.

Therefore:

$$\begin{aligned} \rho'(\theta_1, \phi_1, \theta_r, \phi_r; \lambda_1) &= \frac{\rho_D(\lambda_1)}{\rho_D(\lambda_2)} \rho'_V(\theta_1, \phi_1, \theta_r, \phi_r; \lambda_2) \\ &= \frac{\left[ \frac{\rho_d(\lambda_1)}{\rho_d(\lambda_1) + \rho_s(\lambda_1)} \right] \rho_{DB}(\lambda_1)}{\left[ \frac{\rho_d(\lambda_2)}{\rho_d(\lambda_2) + \rho_s(\lambda_2)} \right] \rho_{DB}(\lambda_2)} \rho'_V(\theta_1, \phi_1, \theta_r, \phi_r; \lambda_2) \end{aligned}$$

Note that to find  $\rho'_V$  at some  $\lambda_j$  between  $\lambda_1$  and  $\lambda_2$ , we would first find  $\rho_s(\lambda_j)$  by linear interpolation between  $\rho_s(\lambda_1)$  and  $\rho_s(\lambda_2)$ . Then assuming that  $\rho_D(\lambda_1)$ ,  $\rho_D(\lambda_j)$  and  $\rho'_V(\lambda_1)$  are known, we can find  $\rho_D(\lambda_1)$  and can calculate:

$$\rho'_V(\lambda_j) = \frac{\rho_D(\lambda_1)}{\rho_D(\lambda_j)} \rho'_V(\lambda_1).$$

### 3.2 Extraction From Bidirectional Reflectance Data

In this case we use only the bidirectional reflectance scan where the source is normal to the target plane ( $\theta_i = 0$ ).

The function to be integrated is:

$$\rho_D = (\rho_{\perp} + \rho_{\parallel}) \sin\theta_r \cos\theta_r$$

Once again the integration is performed graphically after plotting values for the above expression every 5° using the  $\theta_i = 0$  bidirectional data. After repeating the procedure for a second wavelength, the expression can be written:

$$\rho'_V(\theta_i, \phi_i, \theta_r, \phi_r; \lambda_1) = \frac{\rho_D(\lambda_1)}{\rho_D(\lambda_2)} \rho'_V(\theta_i, \phi_i, \theta_r, \phi_r; \lambda_2)$$

In both this procedure and the previous one in which directional data were used the wavelength factor is actually applied to the RHOPRIME program input,  $\rho_V$  or  $\rho_X$  [see Volume I], so that

$$\rho_V(\lambda_1) = \frac{\rho_D(\lambda_1)}{\rho_D(\lambda_2)} \rho_V(\lambda_2)$$

and similarly for  $\rho_X$ .

### 4.0 MODEL VALIDATION

In Figures 8, 9, and 10, the justification for assuming a linear relation between wavelength and surface directional reflectance is shown. Figure 8 shows directional surface reflectance as a function of wavelength for sample AO 1610. (By directional surface reflectance we mean the surface component of the bidirectional reflectance integrated over the hemisphere.) Figures 9 and 10 represent samples AO 2022 and AO 2023 respectively. In all cases the reflectances are normalized so that the value at 0.63  $\mu\text{m}$  is 1. A straight line is drawn between reflectance values at 0.63  $\mu\text{m}$  and 10.6  $\mu\text{m}$ . For sample AO 1610, the largest deviation from linearity is about 40%. For sample AO 2022 the fit to linearity is never worse than 17%, and for AO 2023, never worse than 16%.

As pointed out earlier, validation was done only at 0.63 and 1.06  $\mu\text{m}$  since there was no measurable cross-polarized reflectance for any of the



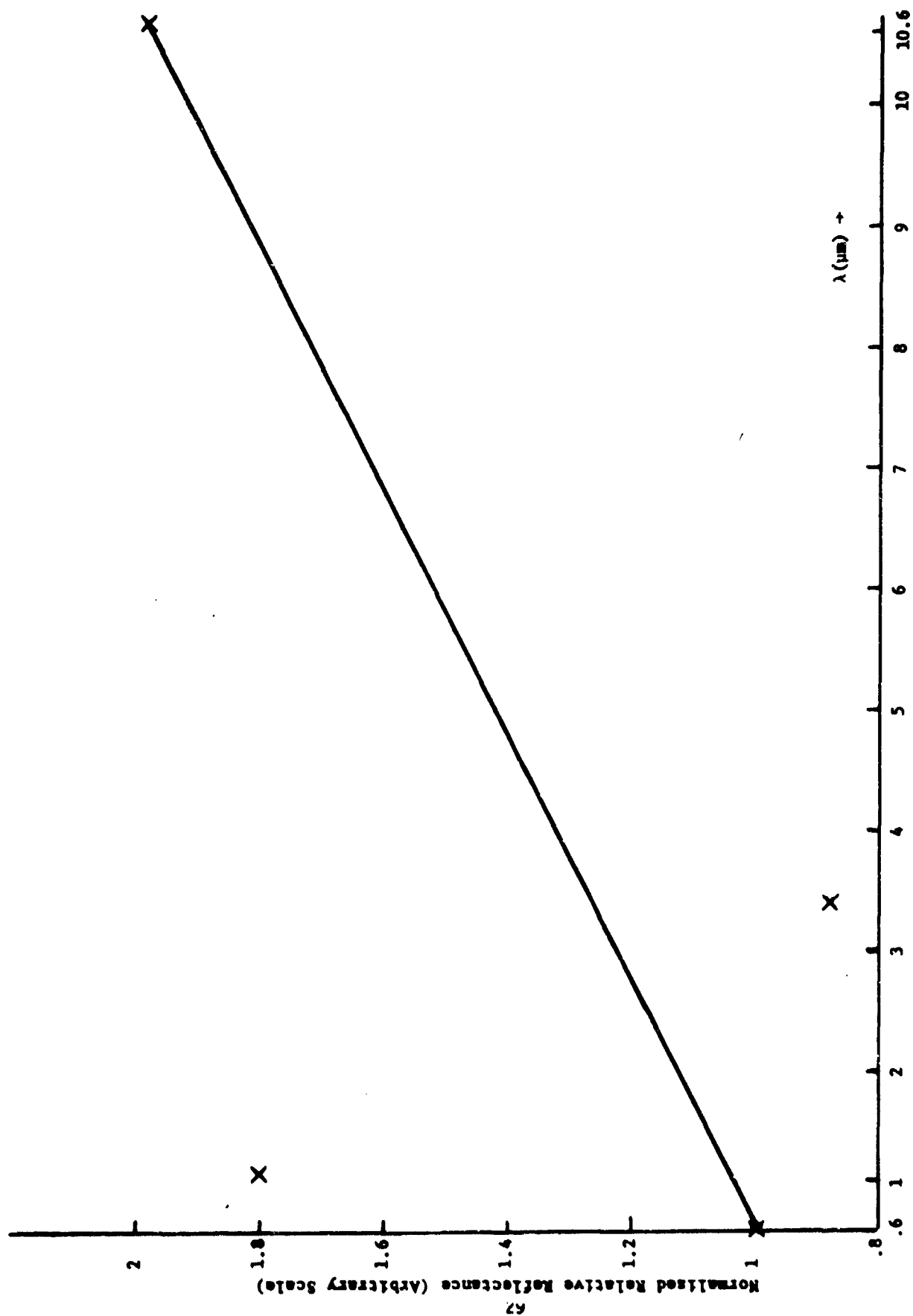


FIGURE 8. Surface Component Of Spectral Directional Reflectance For A01610.

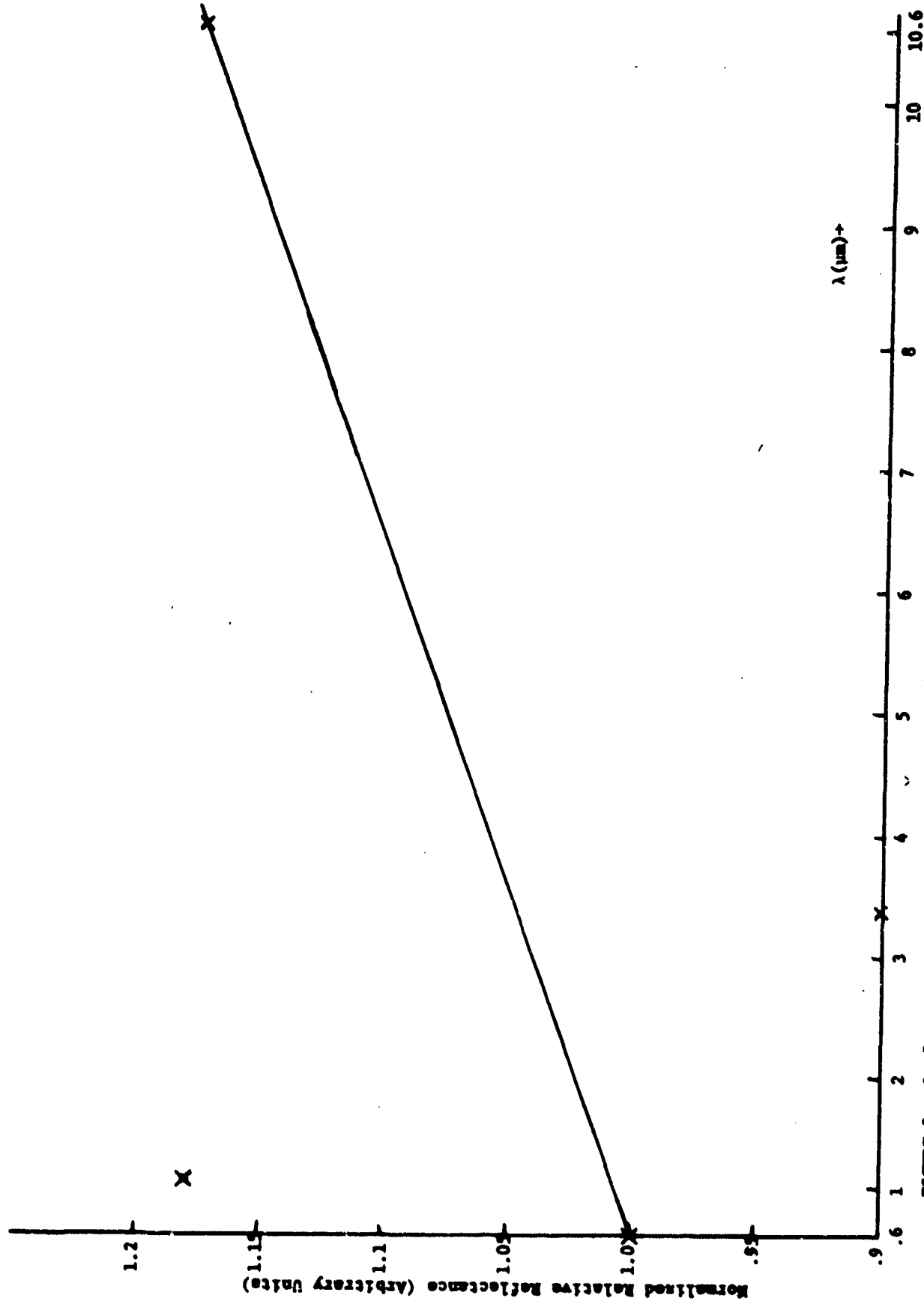


FIGURE 9. Surface Component Of Spectral Directional Reflectance For A02022

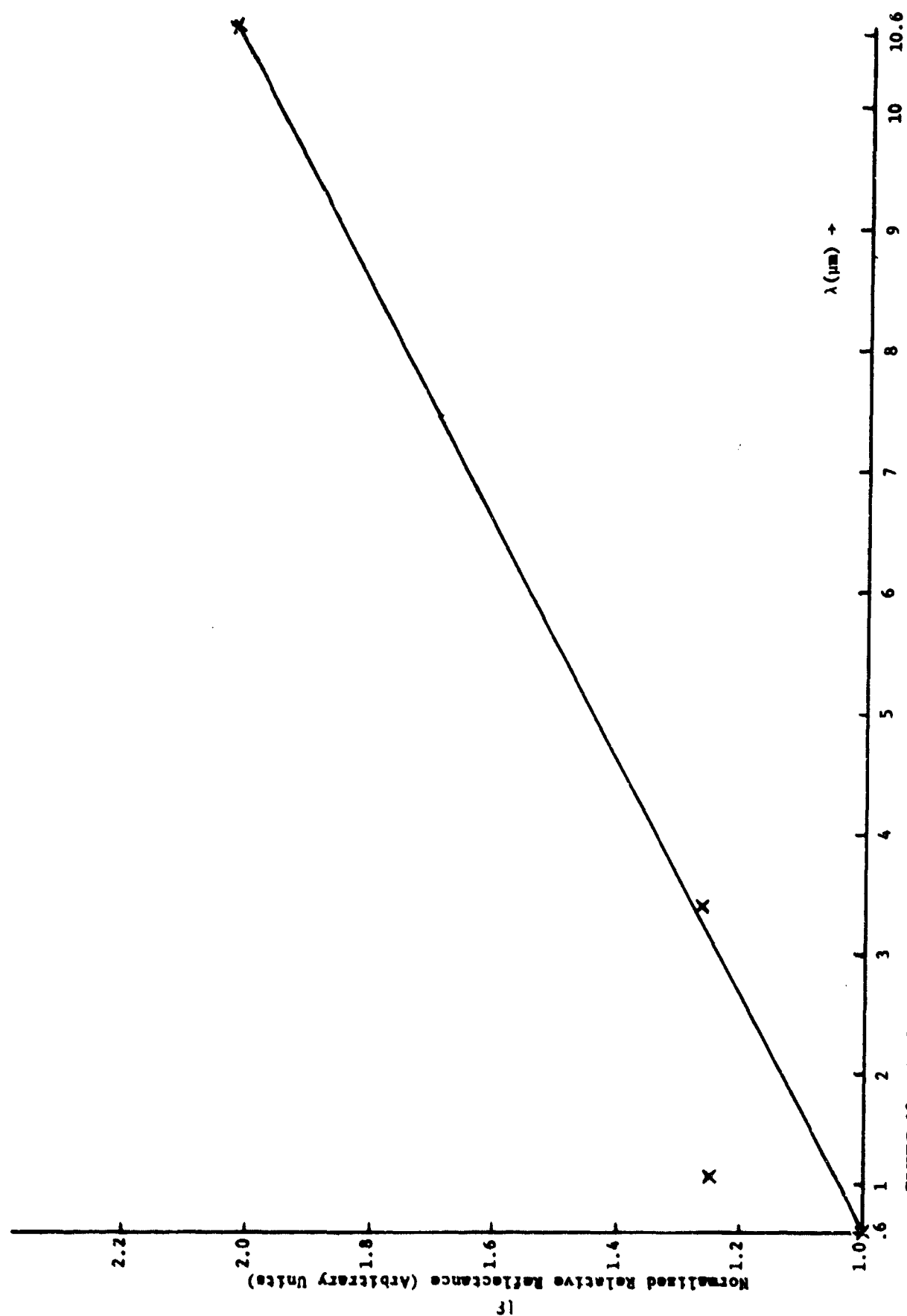


FIGURE 10. Surface Component Of Spectral Directional Reflectance For A02023

samples at 3.39 or 10.6  $\mu\text{m}$ . Therefore validation in this case is a confirmation that the relationship,

$$\rho_V(\lambda_1) = \frac{\rho_D(\lambda_1)}{\rho_D(\lambda_2)} \rho_V(\lambda_2)$$

is valid based on comparison with measurements. If it had turned out that there was a measureable volume component at 3.39  $\mu\text{m}$  the interpolation scheme described in Section 3 could have been more thoroughly validated. Also only samples A01610 and A02022 were used because A02023 had no measurable cross-polarized reflectance at 0.63  $\mu\text{m}$ .

Fixed bistatic bidirectional reflectance scans at both wavelengths (Figures 11, 12, 13 and 14) indicate that both samples follow a non-Lambertian volume reflectance at 0.63  $\mu\text{m}$ . At 1.06  $\mu\text{m}$  the volume component appears to be quite flat for both samples and so in the validation it was assumed that the volume component was Lambertian. Therefore in running the model we use  $\rho_V$  for 0.63  $\mu\text{m}$  and  $\rho_X$  for 1.06  $\mu\text{m}$  as discussed in Volume 1. In Section 3 it was pointed out the  $\rho_D$ , the directional reflectance can be extracted from a combination of bidirectional and directional reflectance measurements where the bidirectional measurement was used to determine and eliminate the effect of the surface reflectance component.

In running the RHOPRIME program, only the cross-polarized contribution was calculated since as stated earlier, only the cross-polarized component has significant wavelength dependence in the spectral region between 0.63  $\mu\text{m}$  and 3.39  $\mu\text{m}$ .

The validation was performed two ways for each sample. In one case,  $\rho_X$  was determined from the fixed bistatic data at 1.06  $\mu\text{m}$  and  $\rho_V$  for 0.63  $\mu\text{m}$  was then calculated from:

$$\rho_V(0.63) = \frac{\rho_D(0.63)}{\rho_D(1.06)} \rho_X(1.06)$$

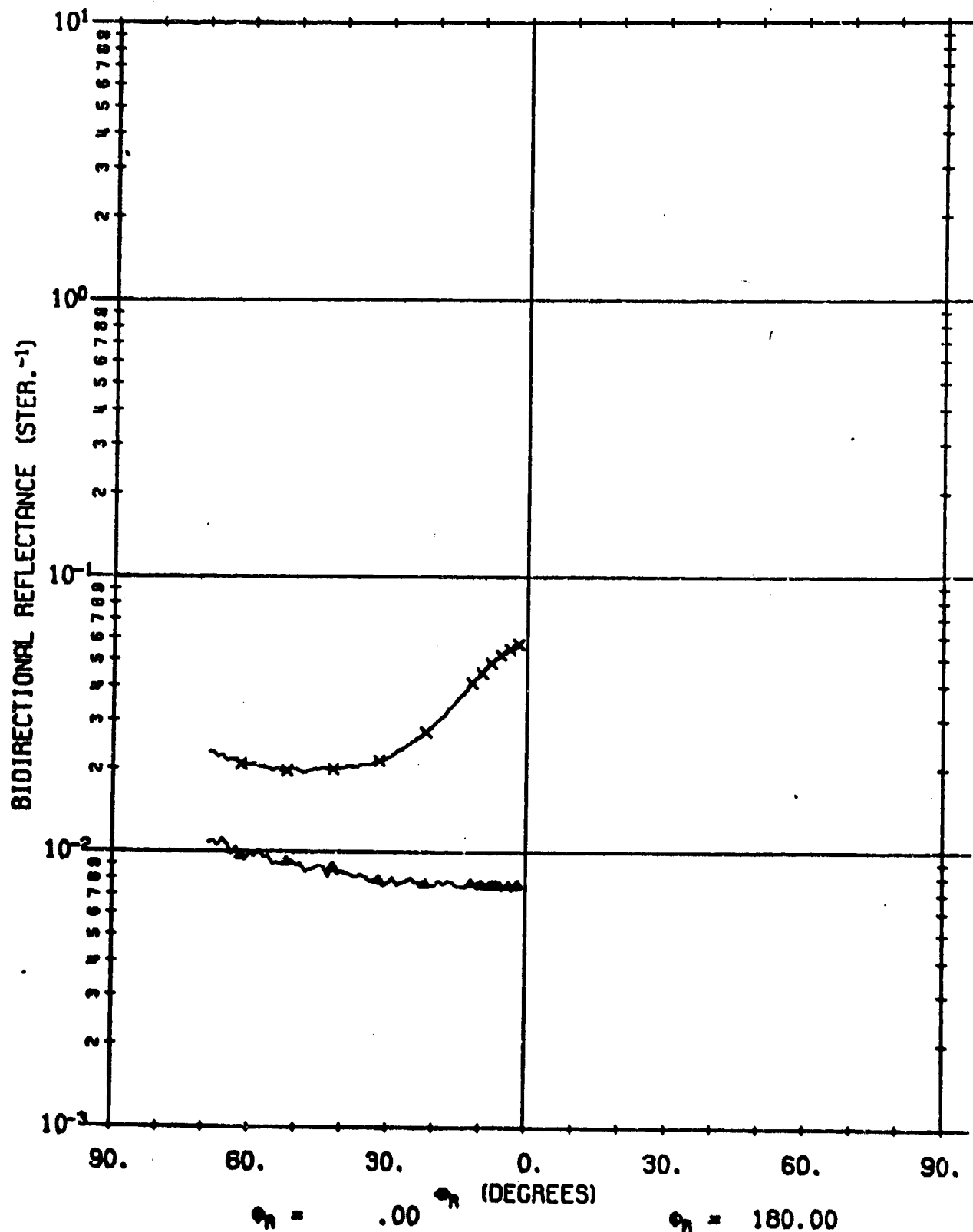
In the other case  $\rho_V$  was determined from the fixed bistatic data at 0.63  $\mu\text{m}$  and  $\rho_X$  for 1.06  $\mu\text{m}$  was then calculated from:

$$\lambda = .63$$

$$\phi_j = \phi_n + -1.7$$

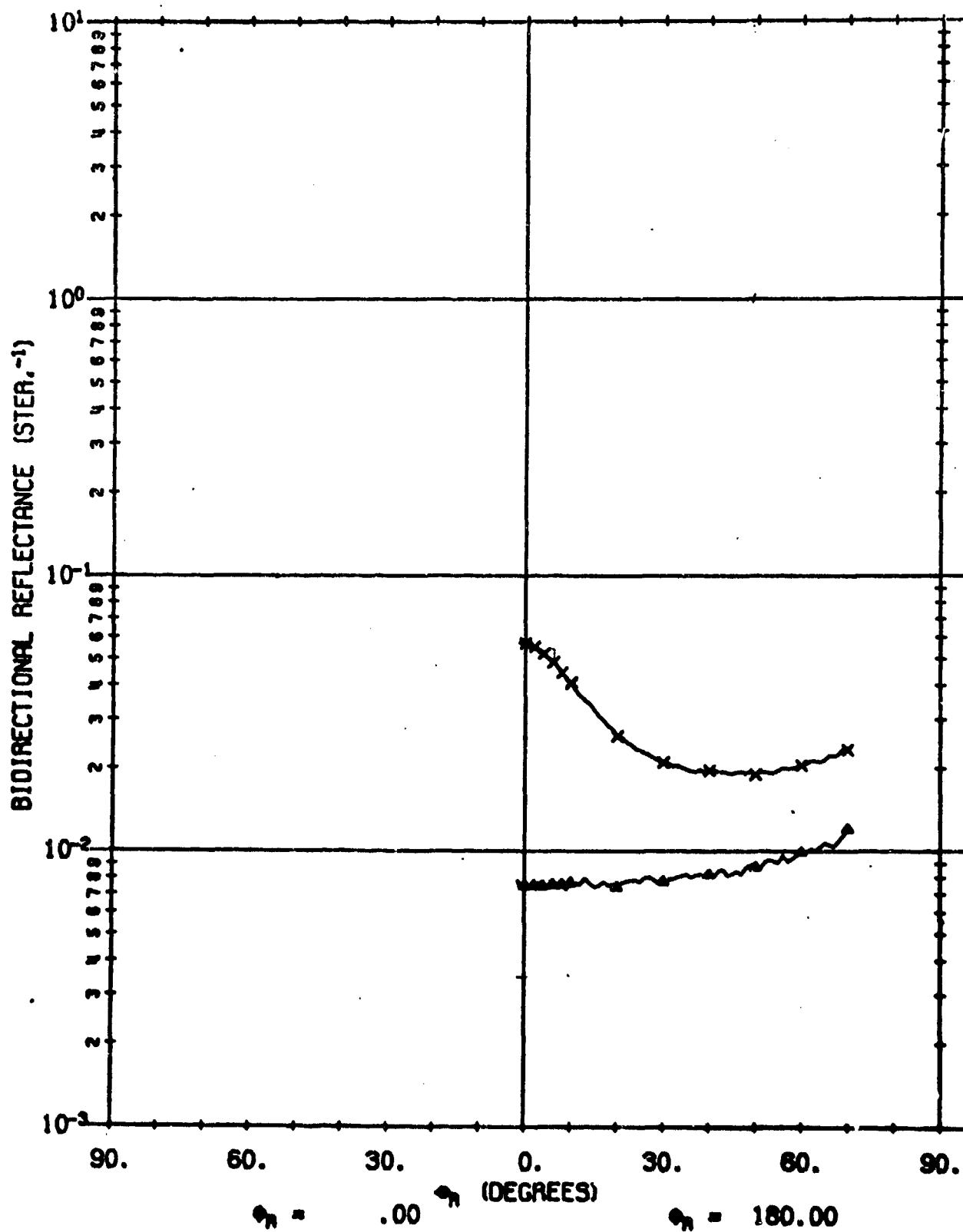
$$\phi_j = .0$$

FIGURE 11a  
AO 1610



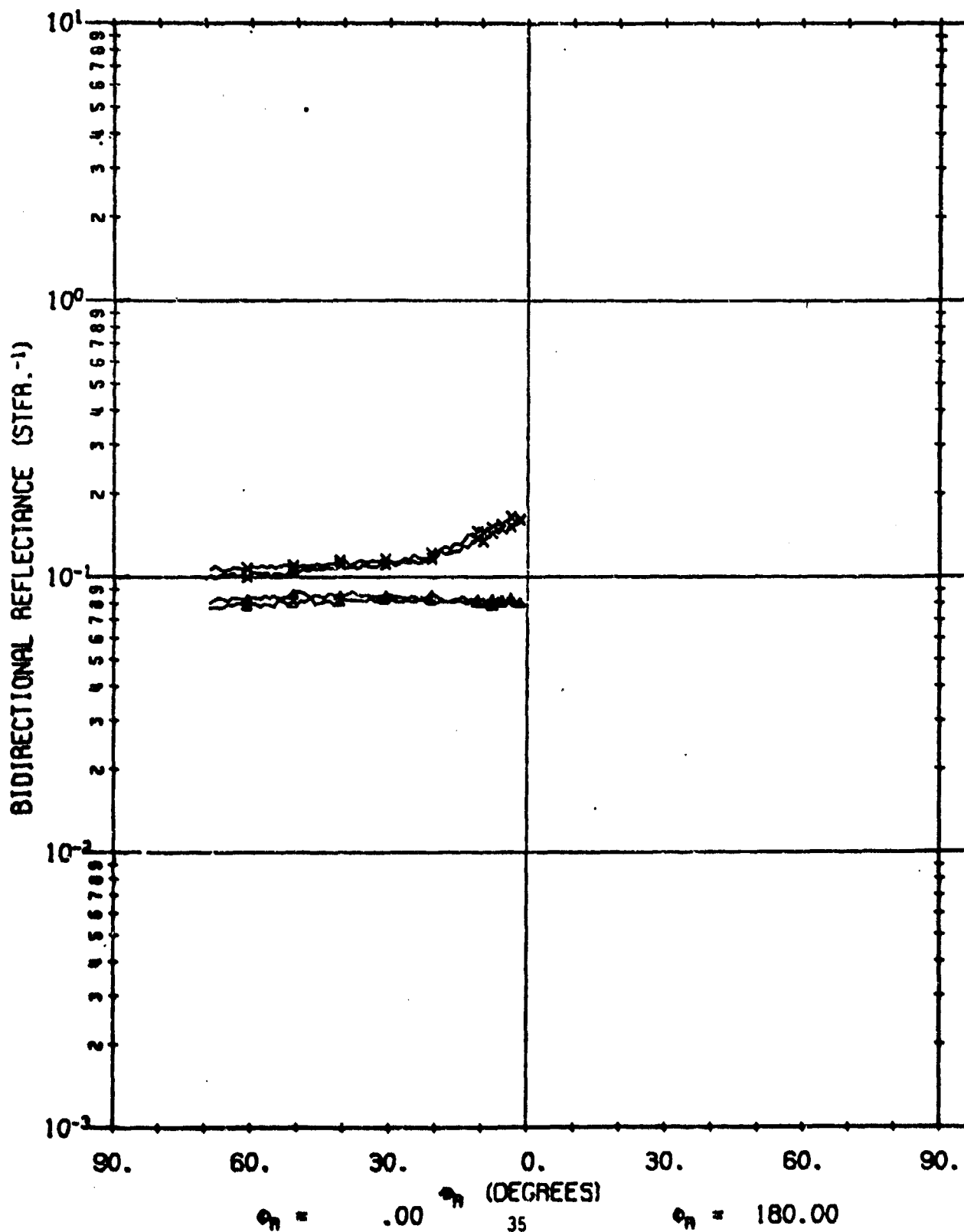
$\lambda = .63$   
 $\phi_1 = \phi_2 = 1.7$   
 $\phi_1 = 180.0$

FIGURE 11b  
 -AO 1610-



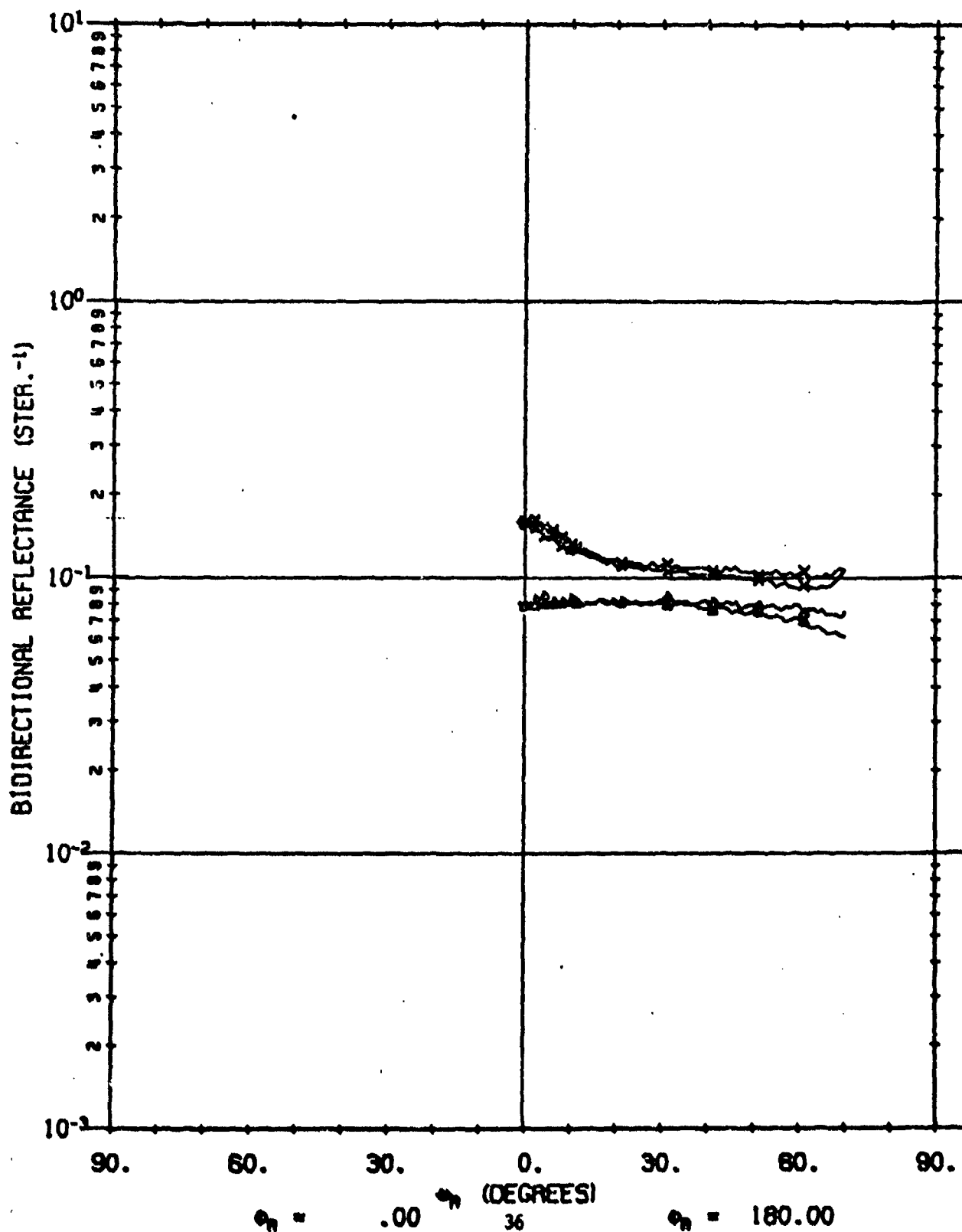
$\lambda = 1.06$   
 $\phi_i = \phi_n + -1.7$   
 $\phi_i = .0$

FIGURE 12a  
A0 1610



$\lambda = 1.06$   
 $\phi_i = \phi_r = 1.7$   
 $\phi_i = 180.0$

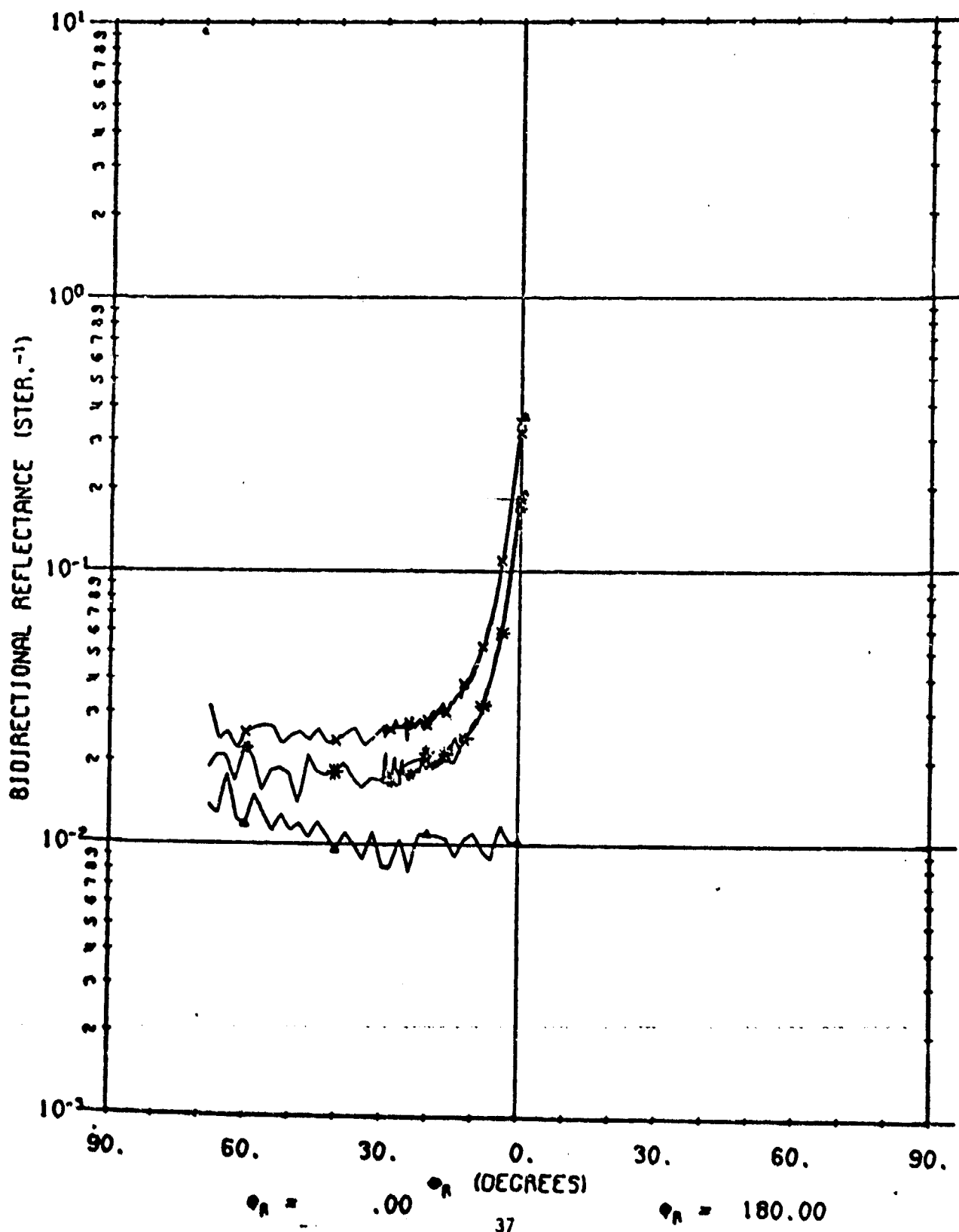
FIGURE 12b  
AO 1610





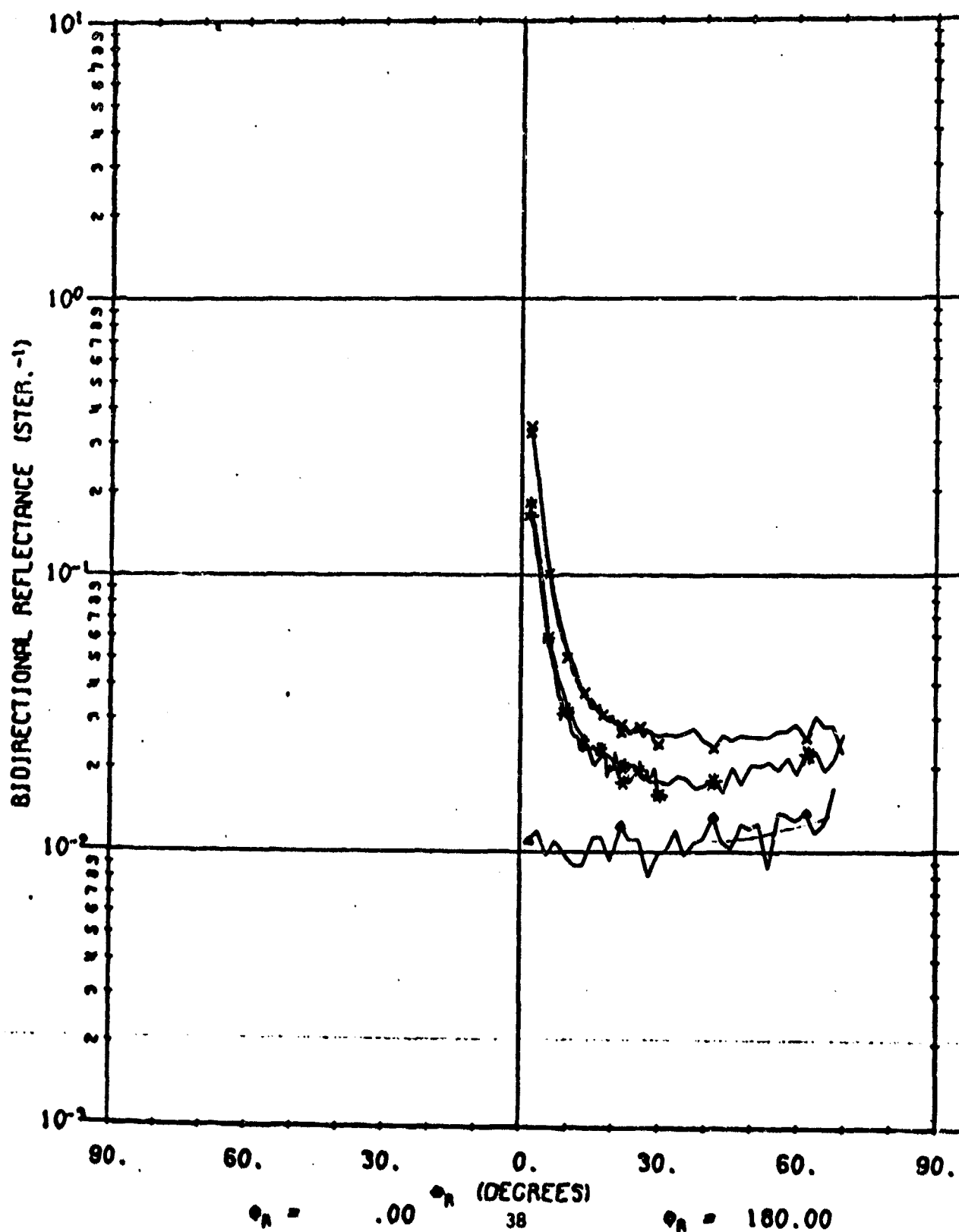
$\lambda = .63$   
 $\phi_i = \phi_R = 1.7$   
 $\phi_j = .0$

FIGURE 13a  
AO 2022



$\lambda = .63$   
 $\phi_i = \phi_r = -1.7$   
 $\phi_i = 180.0$

FIGURE 13b  
AO 2022



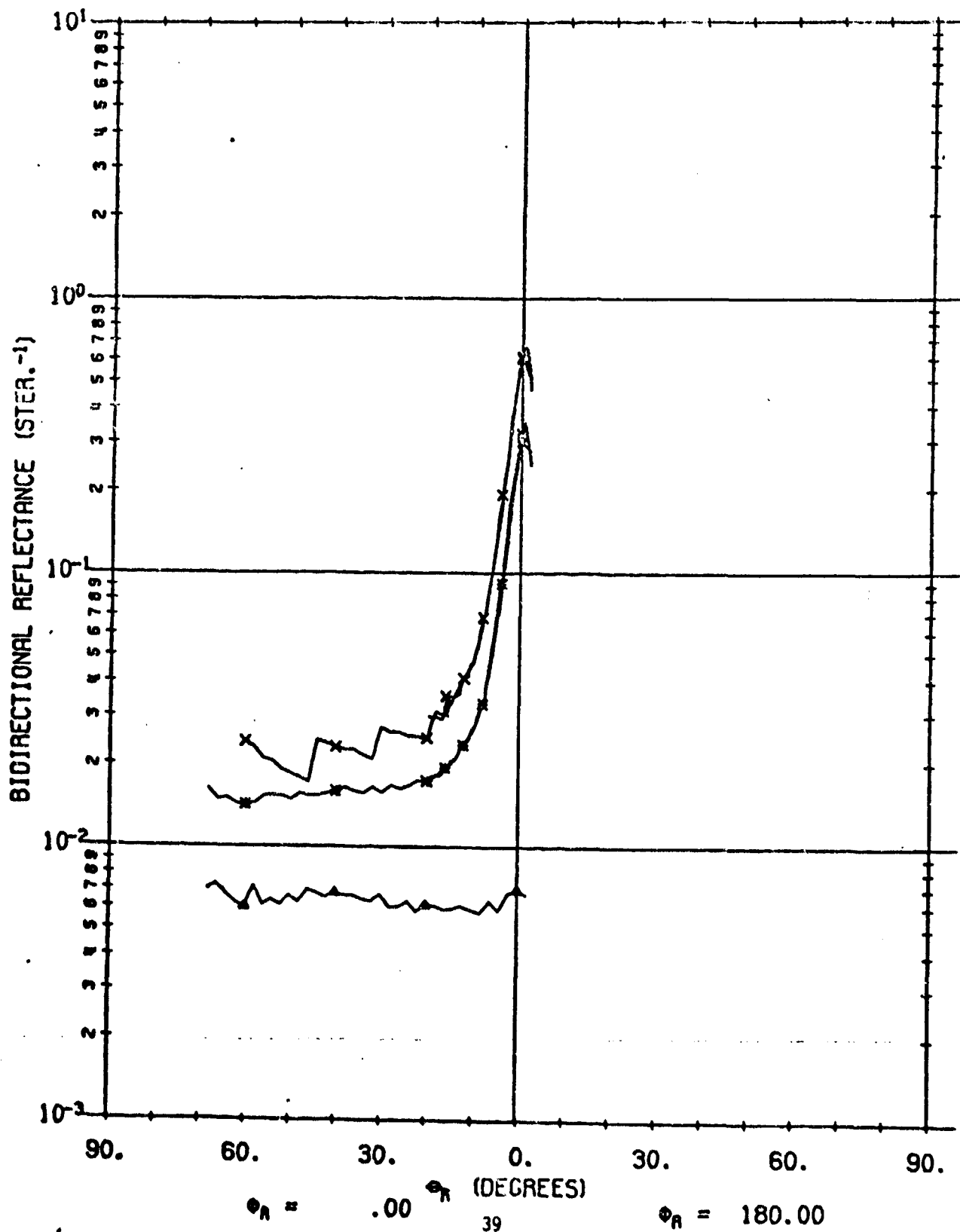
O

$$\lambda = 1.06$$

$$\phi_1 = \phi_n + 1.7$$

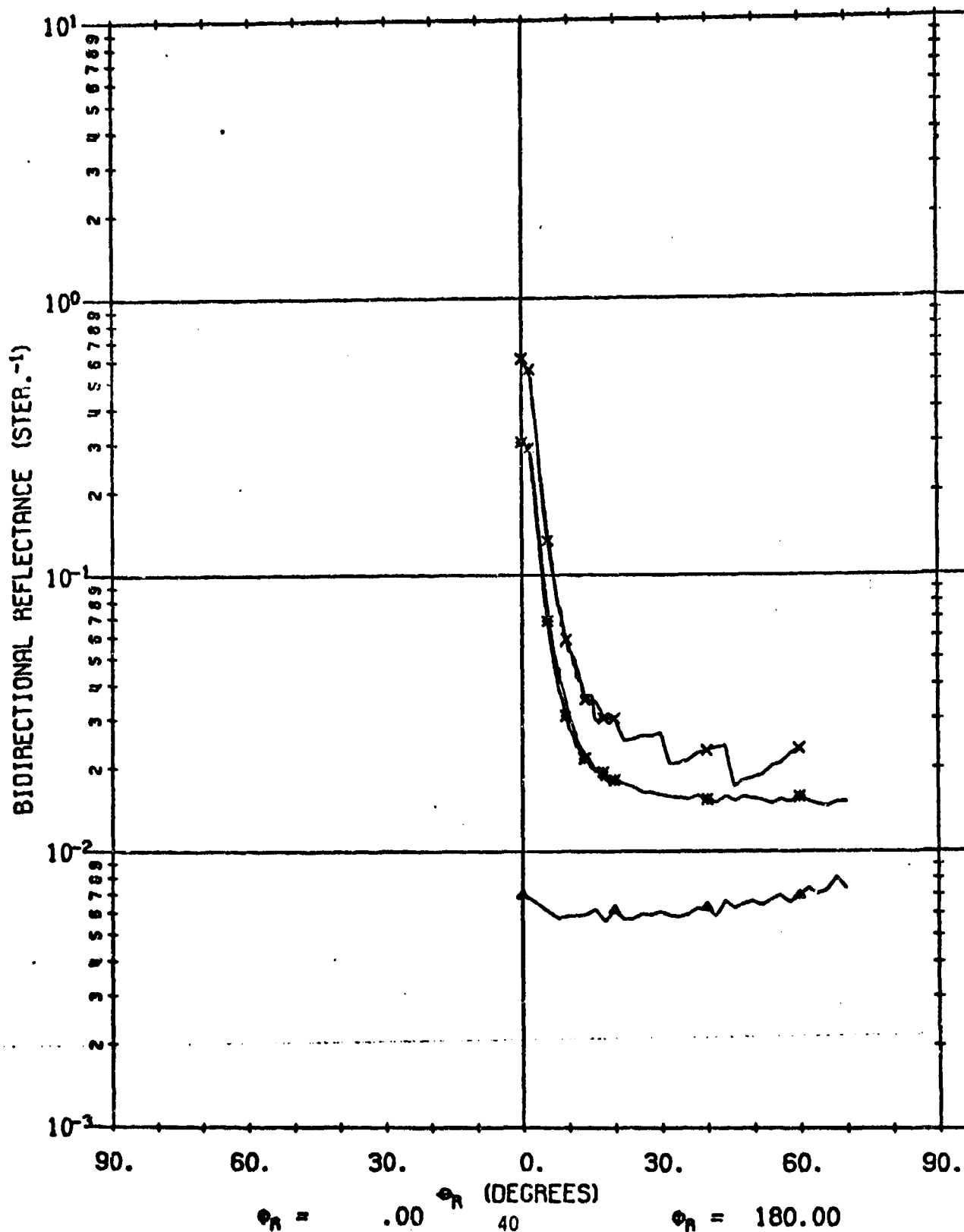
$$\phi_1 = .0$$

FIGURE 14a  
AO 2022



$\lambda = 1.06$   
 $\phi_1 = \phi_2 = -1.0$   
 $\phi_1 = 180.0$

FIGURE 14b  
AO 2022



$$\rho_x(1.06) = \frac{\rho_D(1.06)}{\rho_D(0.63)} \rho_V(0.63)$$

Results were then compared to the measured data for two different source angles,  $\theta_i = 0^\circ$  and  $\theta_i = 40^\circ$ . For both samples it was decided that behavior was most nearly non-Lambertian at 0.63  $\mu\text{m}$  and most nearly Lambertian at 1.06  $\mu\text{m}$ .

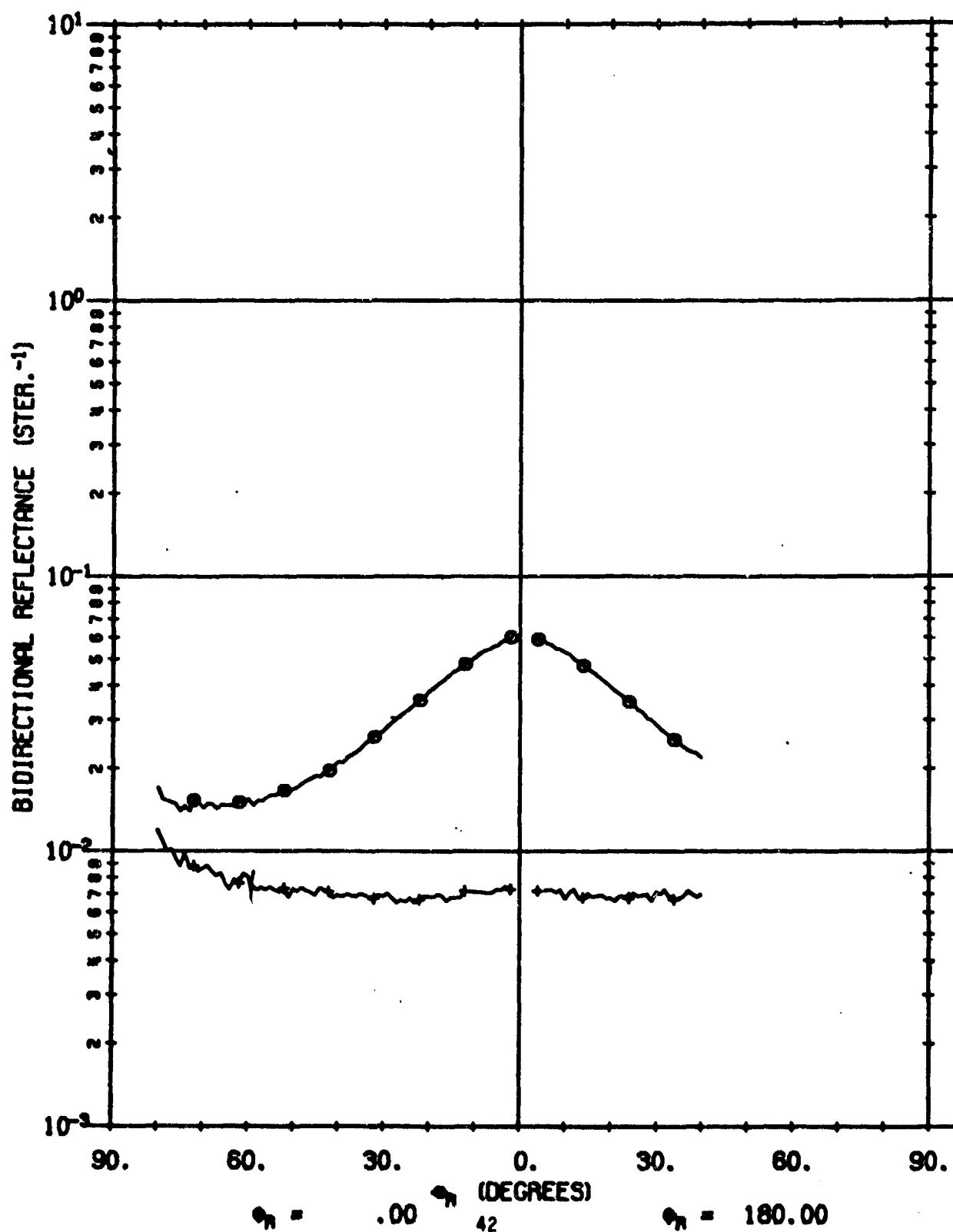
Figure 15 shows the measured data for sample A01610 with "parallel" - polarized source\* at  $\theta_i = 0$  and at 0.63  $\mu\text{m}$ . Figure 16 shows the calculation for the volume component for 0.63  $\mu\text{m}$  with the  $\rho_V$  value extrapolated from 1.06  $\mu\text{m}$  data. The agreement is very close. Figures 17 and 18 provide a similar comparison for  $\theta_i = 40^\circ$ . Figures 19 - 22 again provide similar comparisons for sample A02022. It should be noted that between 0.63  $\mu\text{m}$  and 1.06  $\mu\text{m}$  the wavelength correction is small. As wavelength increases beyond 1.06  $\mu\text{m}$ , however, the cross-polarized component decreases rapidly. (At 3.39  $\mu\text{m}$  it is effectively zero.) Therefore the wavelength correction will be more important as  $\lambda$  increases beyond 1.06  $\mu\text{m}$ .

---

\*The cross-polarized component for the "parallel"-polarized source is the same as that for the "perpendicular"-polarized source.

$\lambda = .63$   
 $\phi_i = .0$   
 $\phi_f = 180.0$

FIGURE 15  
AO 1610

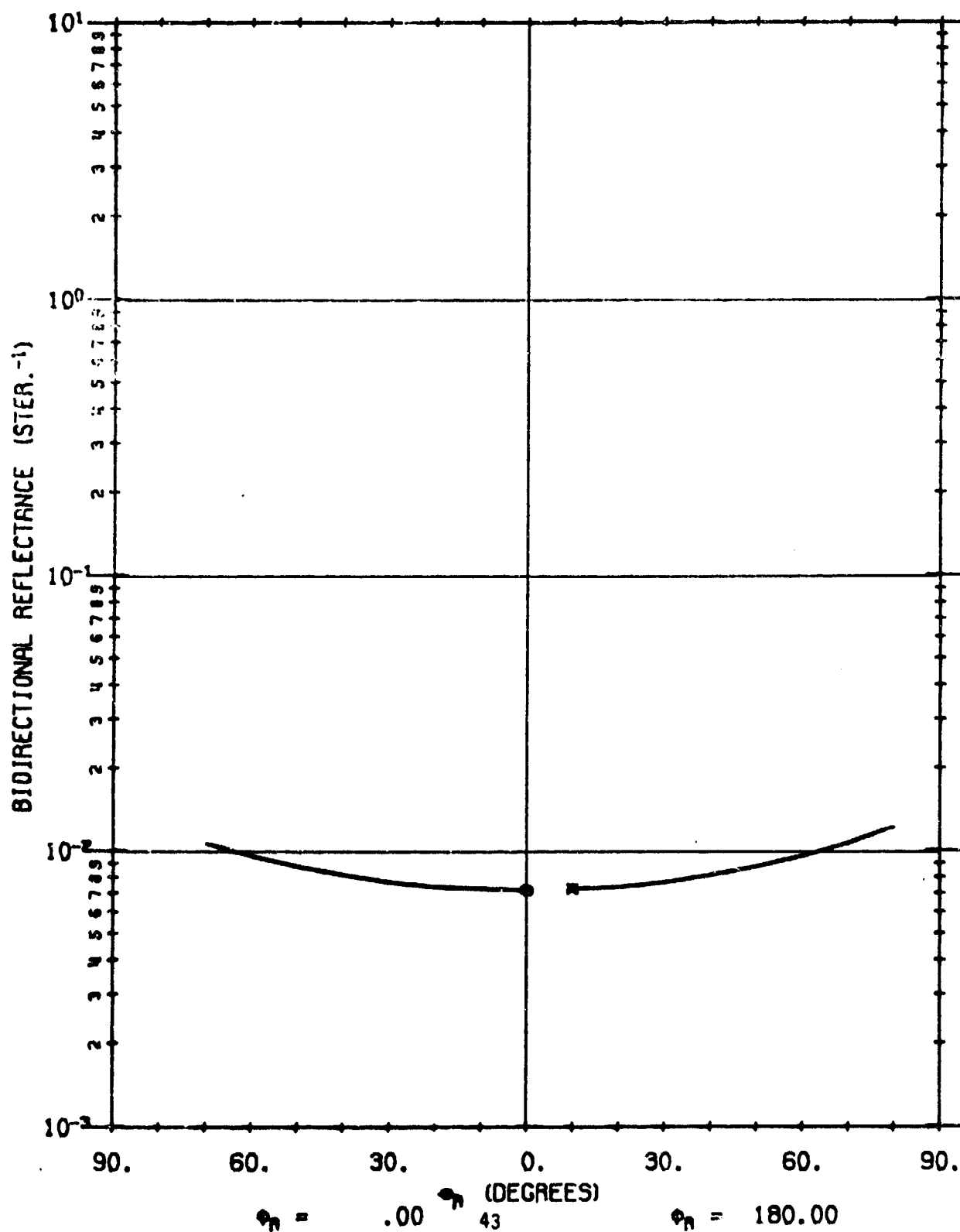


$\phi_n = .00$

42

$\phi_n = 180.00$

$\text{X} + \text{X} \rightarrow \text{X} + \text{X}$



$\lambda = .63$   
 $\phi_1 = 40.0$   
 $\phi_2 = 180.0$

FIGURE 17  
AO 1610

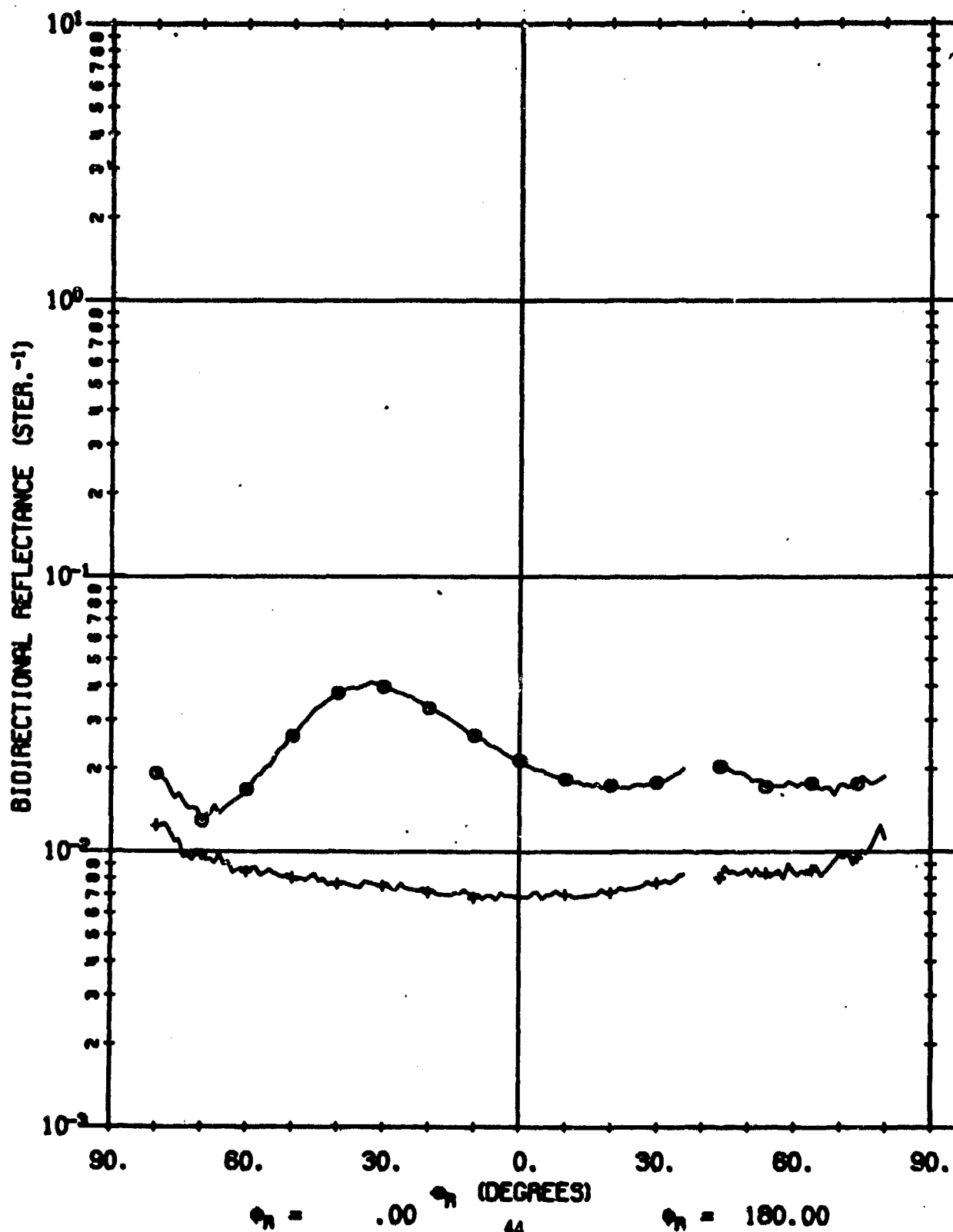
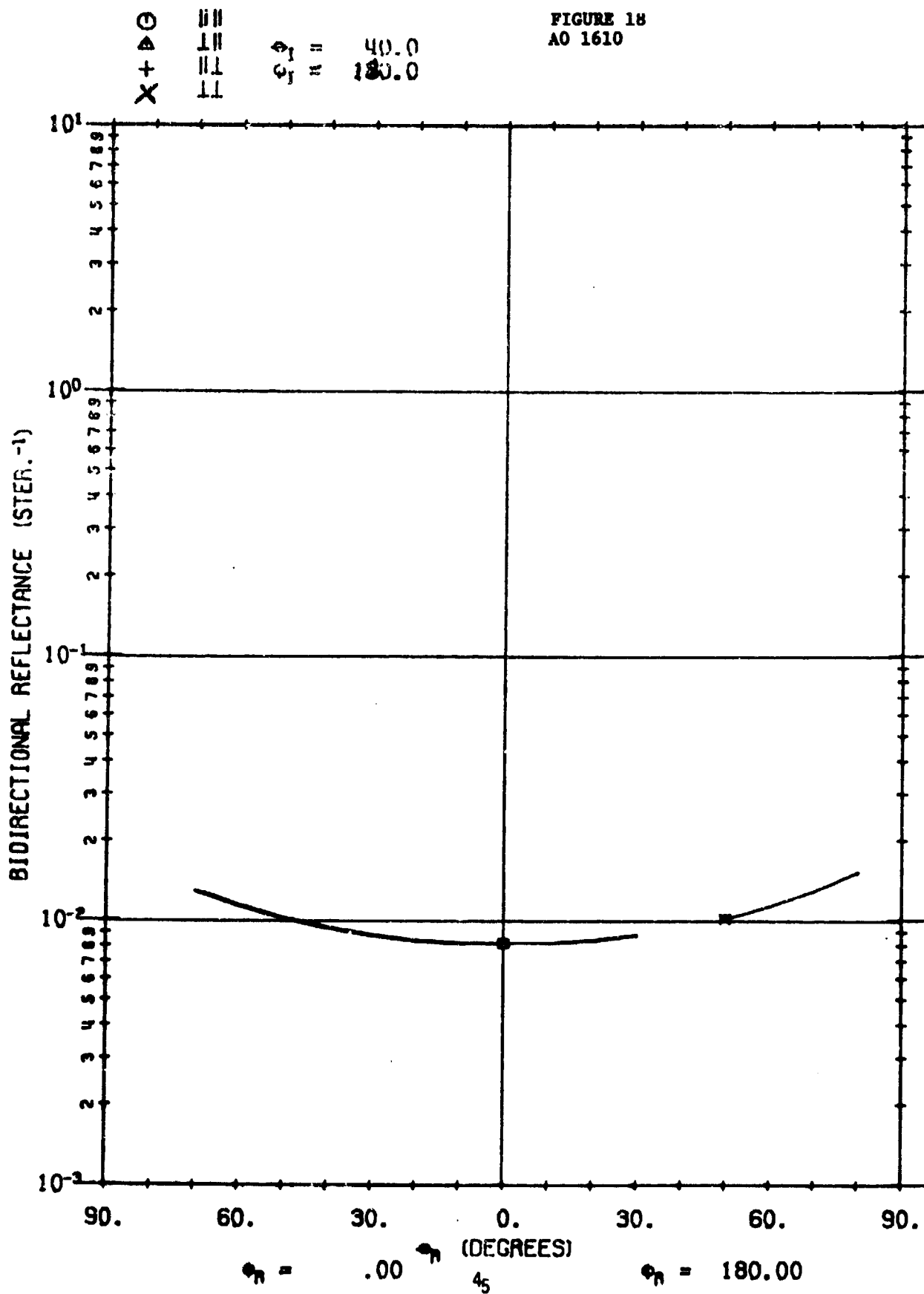




FIGURE 18  
AO 1610



$\lambda = .63$   
 $\phi_i = .0$   
 $\phi_f = 180.0$

FIGURE 19  
AO 2022

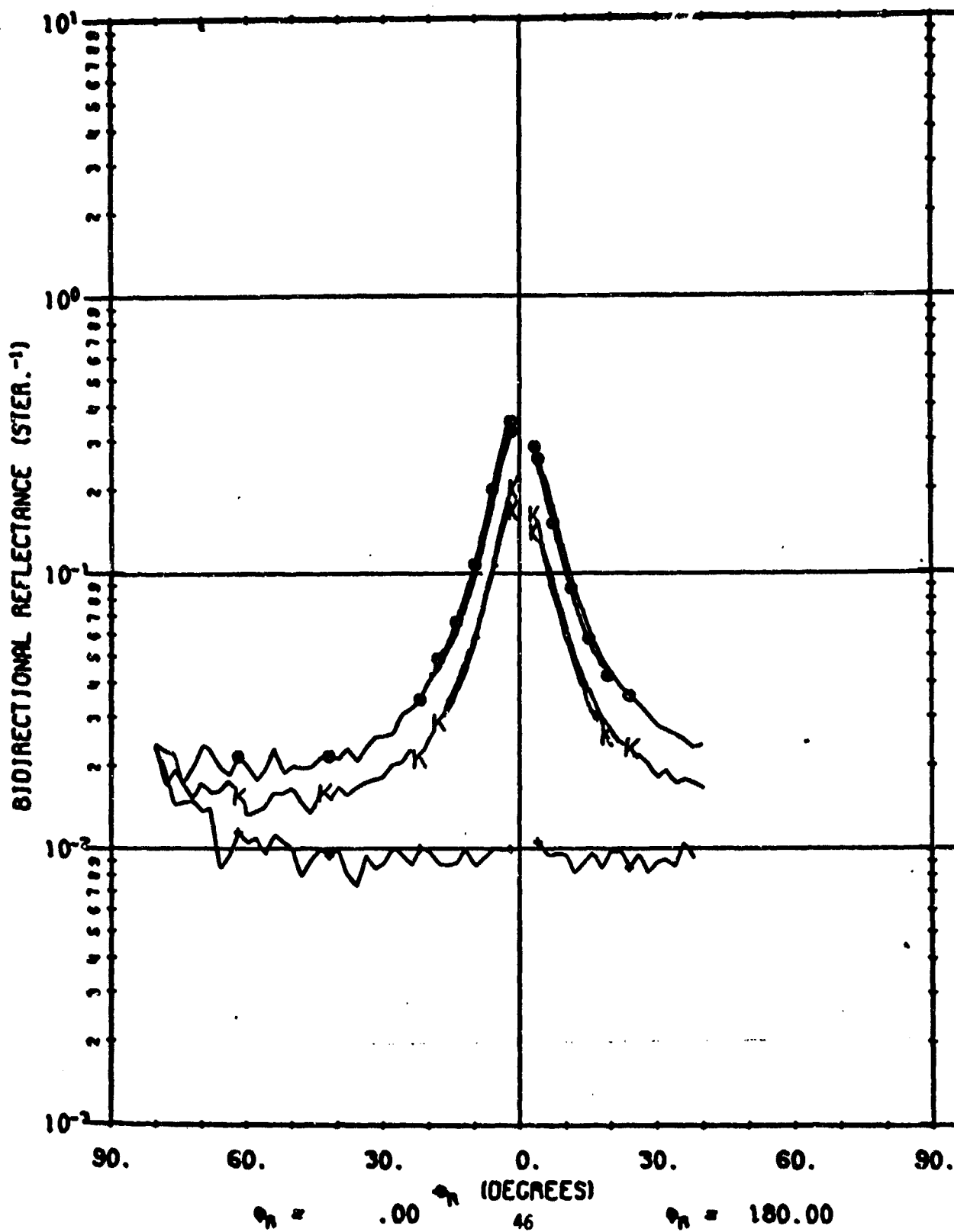
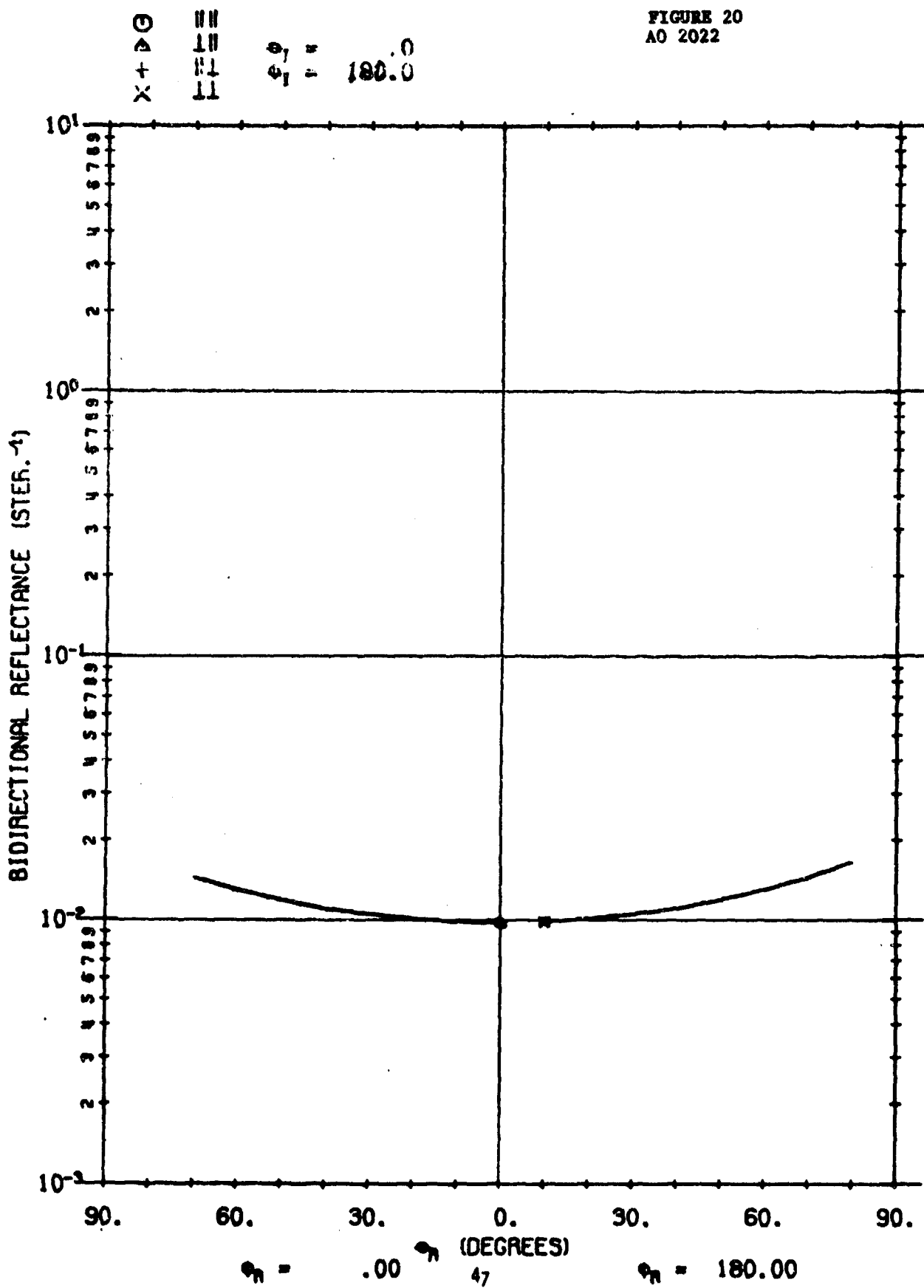


FIGURE 20  
AO 2022



$\lambda = .63$   
 $\phi_i = 40.0$   
 $\phi_f = 180.0$

FIGURE 21  
AO 2022

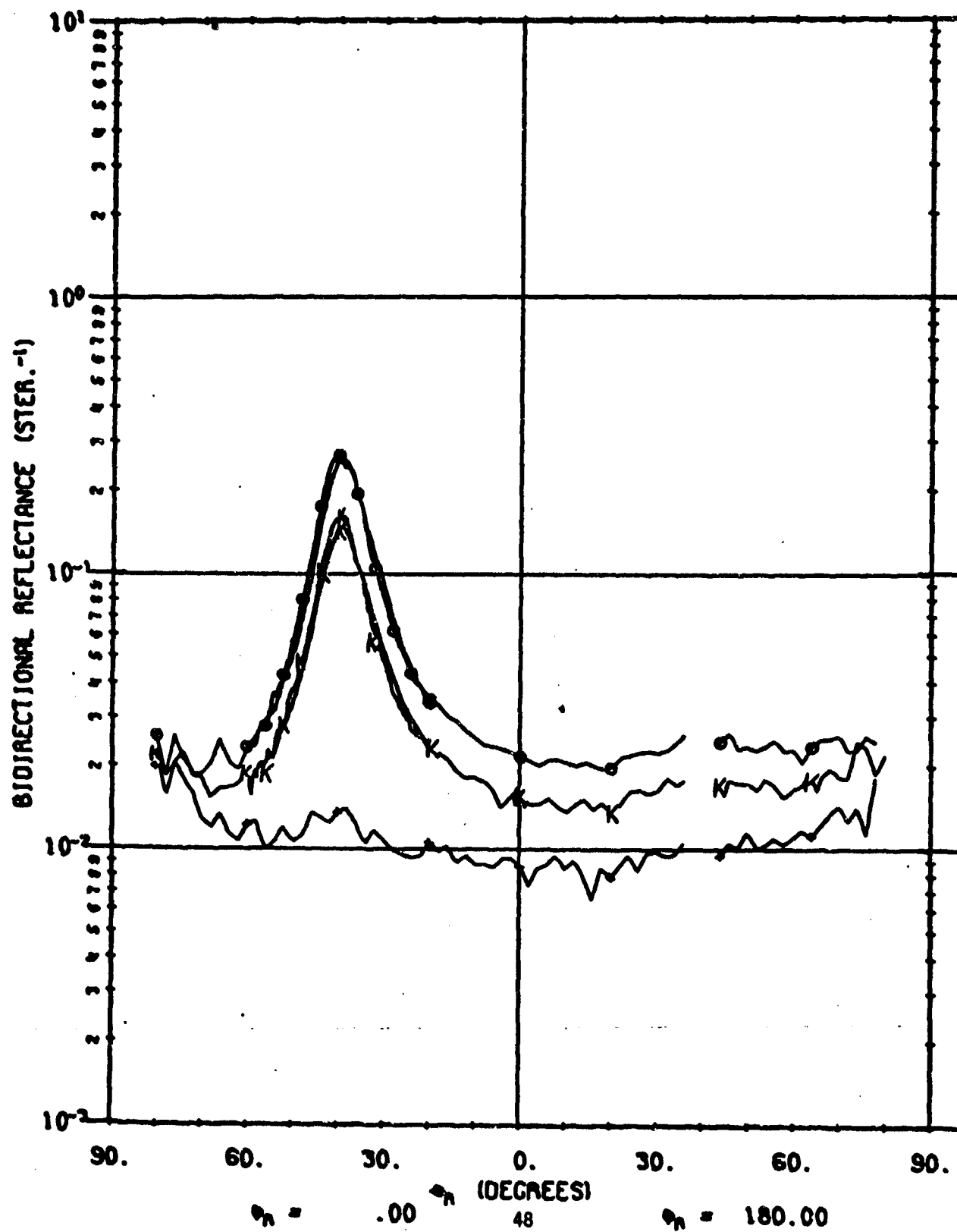
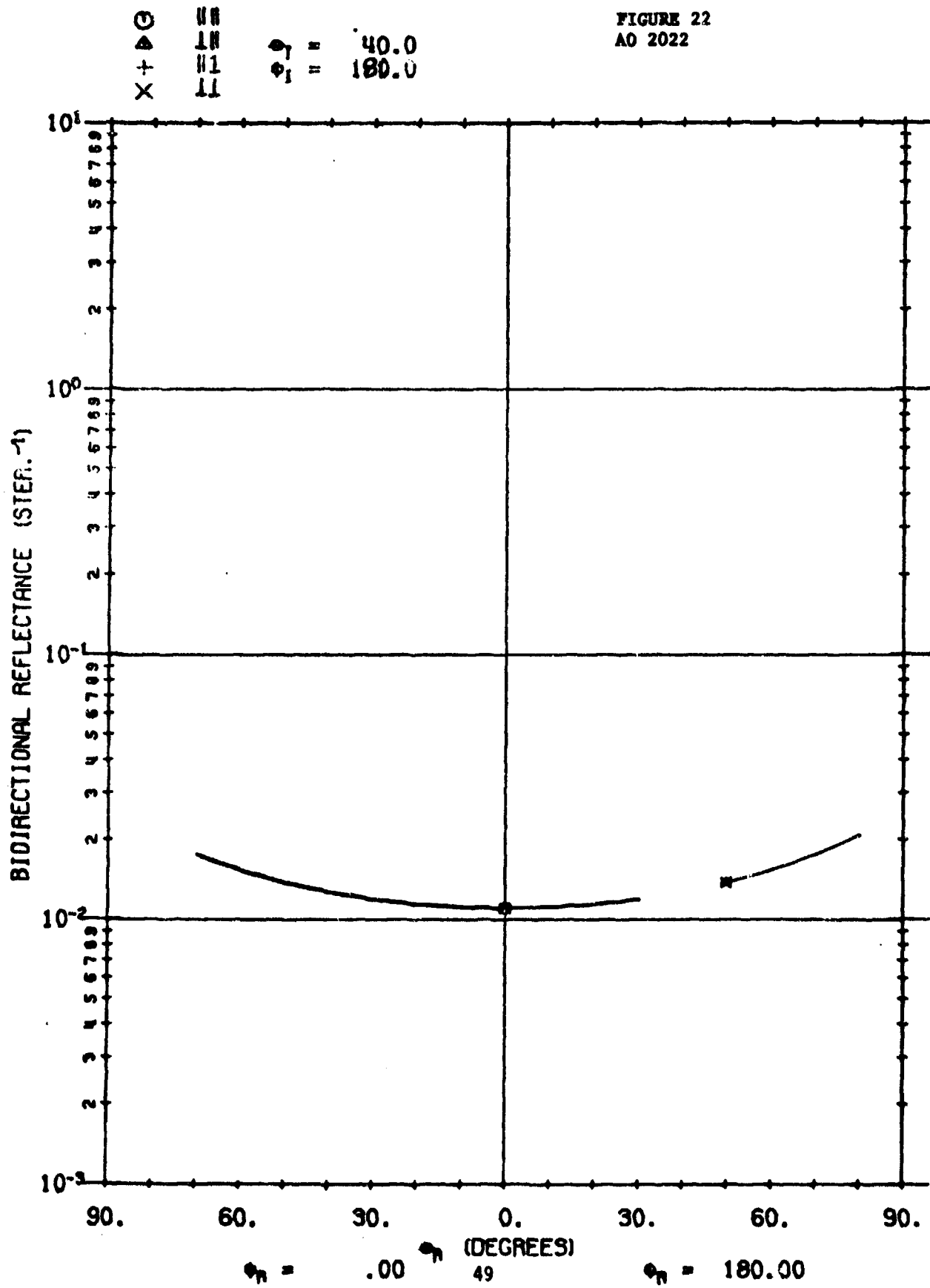


FIGURE 22  
AO 2022



(DEGREES)

49

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2. Target Signature Program: Measurements and Analyses, Report No. AFAL-TR-70-213, Willow Run Laboratories of The University of Michigan, Ann Arbor, March 1971.
3. A Gonireflectometer Facility Using Coherent and Incoherent Sources, Report No. AFAL-TR-70-161, Willow Run Laboratories of The University of Michigan, Ann Arbor, August 1970.
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APPENDIX A

BIDIRECTIONAL REFLECTANCE DATA FOR SAMPLES  
A01610, A02022, A02023 AT 0.63, 1.06, 3.39 AND 10.6  $\mu\text{m}$ .

For convenience in using this Appendix, the data are preceeded by an index which outlines the organization and provides page numbers of specific data sets.

# Bidirectional Reflectance Data With Fixed Bistatic Angle

<u>Sample</u>	<u>Source Polarization</u>	<u><math>\lambda</math> (<math>\mu\text{m}</math>)</u>	<u><math>\phi</math>-Plane</u>	<u>Page</u>
A02023	$\perp$	.63, 1.06, 3.39, 10.6	0, 180	57
	45	3.39, 10.6	0, 180	65
		.63, 1.06, 3.39, 10.6	0, 180	69
		10.6	90, 270	77
A01610	$\perp$	.63, 1.06, 3.39, 10.6	0, 180	79
	45	3.39	0, 180	87
		.63, 1.06, 3.30	0, 180	89
		10.6	90, 270	95
A02022	$\perp$	.63, 1.06, 3.39, 10.6	0, 180	97
	45	3.39, 10.6	0, 180	105
		.63, 1.06, 3.39, 10.6	0, 180	109
		10.6	90, 270	117



# Bidirectional Reflectance Data With Variable Bistatic Angle

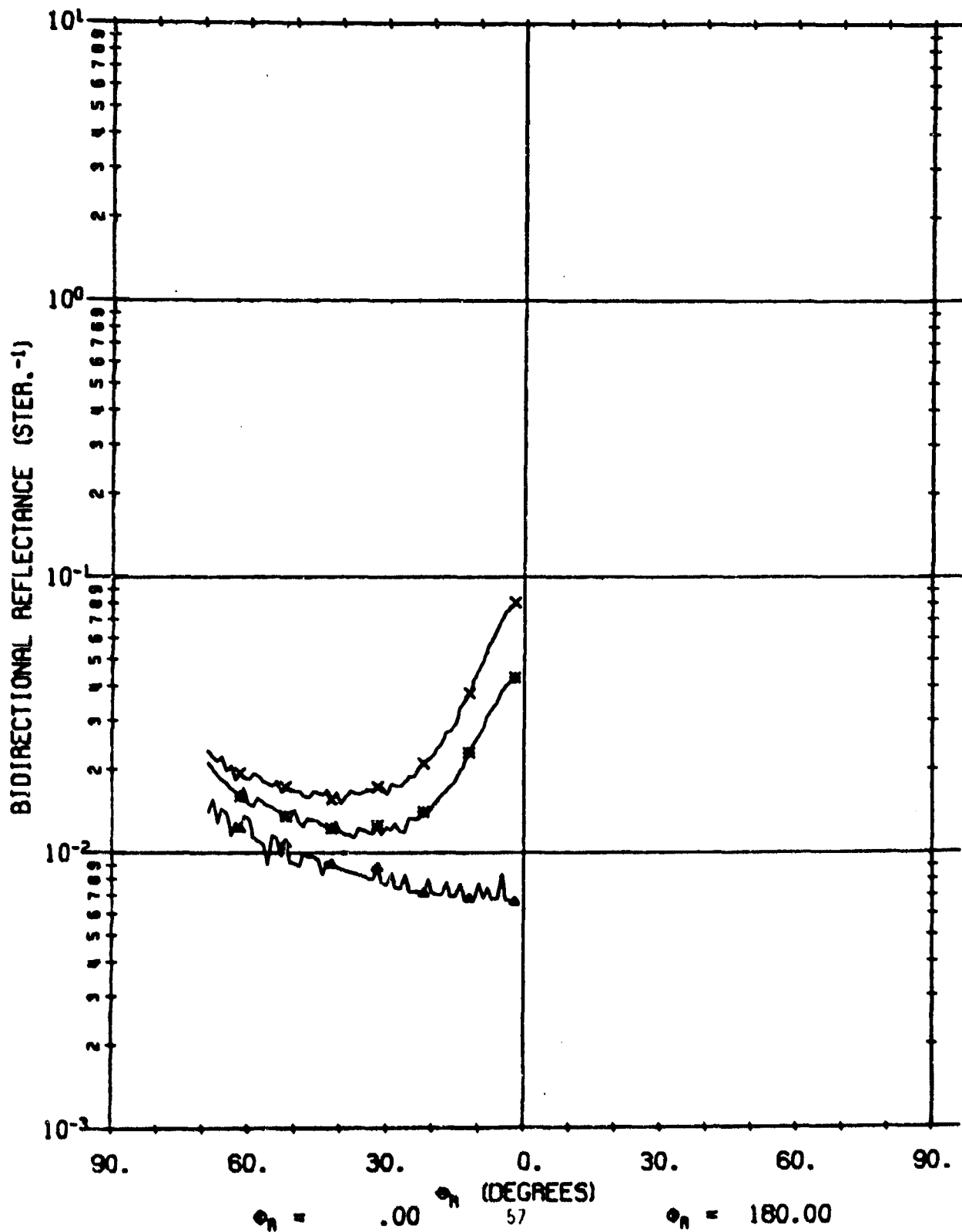
<u>Sample</u>	<u>Source Polarisation</u>	<u><math>\theta_i</math></u>	<u><math>\lambda</math> (<math>\mu\text{m}</math>)</u>	<u><math>\phi</math>-Plane</u>	<u>Page</u>
A01610	⊥	0	.63, 1.06, 3.39, 10.6	0, 180	119
		20	.63, 1.06, 3.39, 10.6	0, 180	123
		20	.63, 1.06, 3.39, 10.6	90, 270	127
		40	.63, 1.06, 3.39, 10.6	0, 180	131
		40	.63, 1.06, 3.39, 10.6	90, 270	135
		60	.63, 1.06, 3.39, 10.6	0, 180	139
		60	.63, 1.06, 3.39, 10.6	90, 270	143
A01610	45°	0	3.39, 10.6	0, 100	147
		20	3.39, 10.6	0, 100	149
		20	3.39, 10.6	90, 270	151
		40	3.39, 10.6	0, 180	153
		40	3.39	90, 270	155
		60	3.30, 10.6	0, 180	156
		60	3.39	90, 270	158
A01610		0	.63, 1.06, 3.39, 10.6	0, 180	159
		20	.63, 1.06, 3.39, 10.6	0, 180	163
		20	.63, 1.06, 3.39	90, 270	167
		40	.63, 1.06, 3.39, 10.6	0, 180	170
		40	.63, 1.06, 3.39	90, 270	174
		60	.63, 1.06, 3.39, 10.6	0, 180	177
		60	.63, 1.06, 3.39	90, 270	181

<u>Sample</u>	<u>Source Polarization</u>	<u><math>\theta_i</math></u>	<u><math>\lambda</math> (<math>\mu\text{m}</math>)</u>	<u><math>\phi</math>-Plane</u>	<u>Page</u>
A02022	┴	0	.63, 1.06, 3.39, 10.6	0, 180	184
		0	.63, 1.06	90, 270	188
		20	.63, 1.06, 3.39, 10.6	0, 180	190
		20	.63, 1.06, 3.39, 10.6	90, 270	194
		40	.63, 1.06, 3.39, 10.6	0, 180	198
		40	.63, 1.06, 3.39, 10.6	90, 270	202
		60	.63, 1.06, 3.39, 10.6	0, 180	206
		60	.63, 1.06, 3.39, 10.6	90, 270	210
A02022	45°	0	3.39, 10.6	0, 180	214
		20	3.39, 10.6	0, 180	216
		20	3.39, 10.6	90, 270	218
		40	3.39, 10.6	0, 180	220
		40	3.39, 10.6	90, 270	222
		60	3.39, 10.6	0, 180	224
		60	3.39, 10.6	90, 270	226
A02022		0	.63, 1.06, 3.39, 10.6	0, 180	228
		0	.63, 1.06	90, 270	232
		20	.63, 1.06, 3.39, 10.6	0, 180	234
		20	.63, 1.06, 3.39, 10.6	90, 270	238
		40	.63, 1.06, 3.39, 10.6	0, 180	242
		40	.63, 1.06, 3.39, 10.6	90, 270	246
		60	.63, 1.06, 3.39, 10.6	0, 180	250
		60	.63, 1.06, 3.39	90, 270	254

<u>Sample</u>	<u>Source Polarization</u>	<u><math>\theta_i</math></u>	<u><math>\lambda</math> (<math>\mu\text{m}</math>)</u>	<u><math>\phi</math>-Plane</u>	<u>Page</u>
A02023	⊥	0	1.06, 3.39, 10.6	0, 180	257
		0	1.06	90, 270	260
		20	1.06, 3.30, 10.6	0, 180	261
		20	.63, 1.06, 3.39, 10.6	90, 270	264
		40	1.06, 3.39, 10.6	0, 180	268
		40	.63, 1.06, 3.39, 10.6	90, 270	271
		60	1.06, 3.39, 10.6	0, 180	275
		60	.63, 1.06, 3.39, 10.6	90, 270	278
A02023	45°	0	3.39, 10.6	0, 180	282
		20	3.39, 10.6	0, 180	284
		20	3.39, 10.6	90, 270	286
		40	3.39, 10.6	0, 180	288
		40	3.39, 10.6	90, 270	290
		60	3.39, 10.6	0, 180	292
		60	3.39, 10.6	90, 270	294
A02023		0	.63, 1.06, 3.39, 10.6	0, 180	296
		0	1.06	90, 270	300
		20	.63, 1.06, 3.39, 10.6	0, 180	301
		20	.63, 1.06, 3.39, 10.6	90, 270	305
		40	.63, 1.06, 3.39, 10.6	0, 180	309
		40	.63, 1.06, 3.39, 10.6	90, 270	313
		60	.63, 1.06, 3.39, 10.6	0, 180	317
		60	.63, 1.06, 3.39, 10.6	90, 270	321

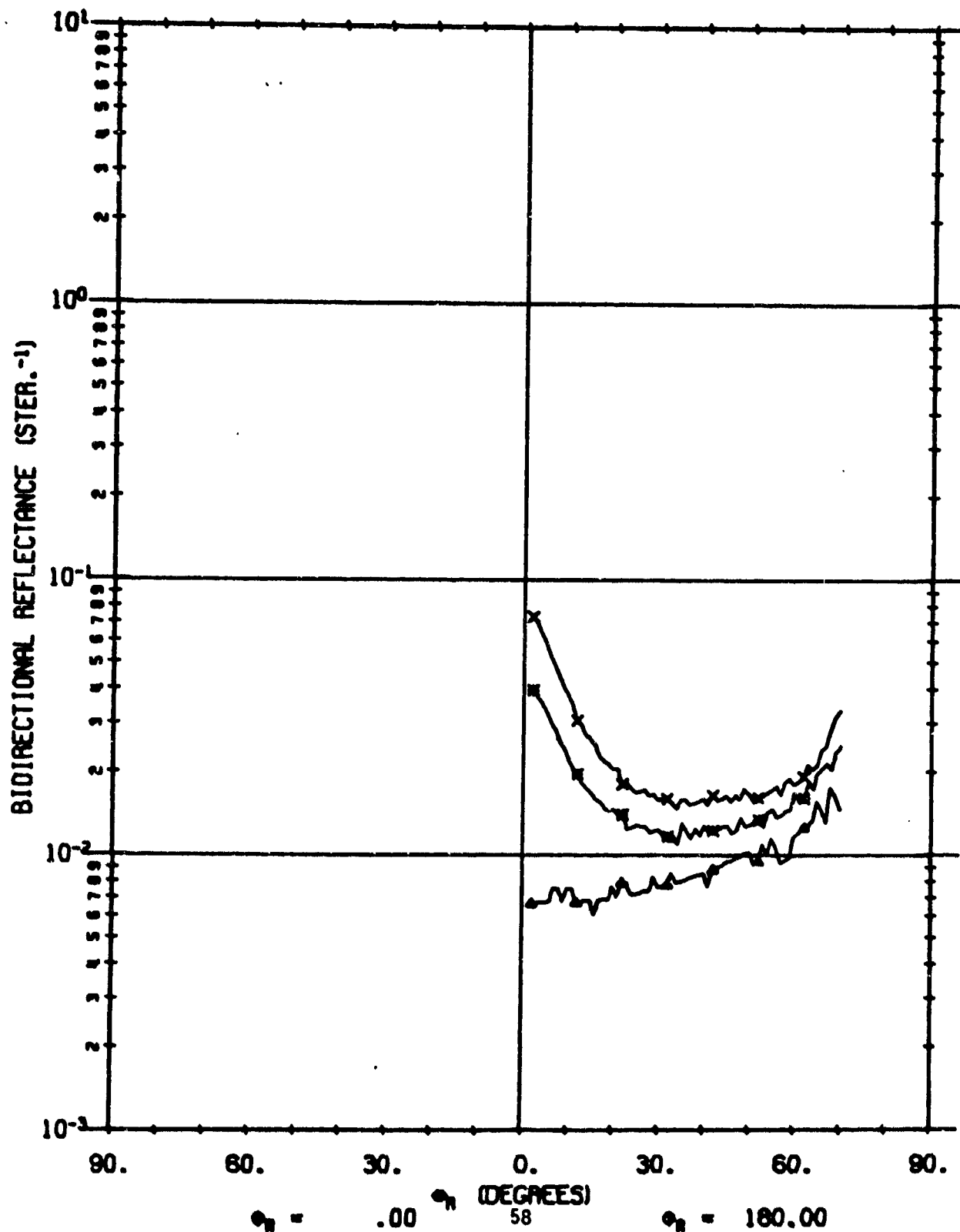
A02023 501

$$\begin{aligned} \lambda &= .63 \\ \phi_i &= \phi_n + -1.7 \\ \phi_i &= .0 \end{aligned}$$



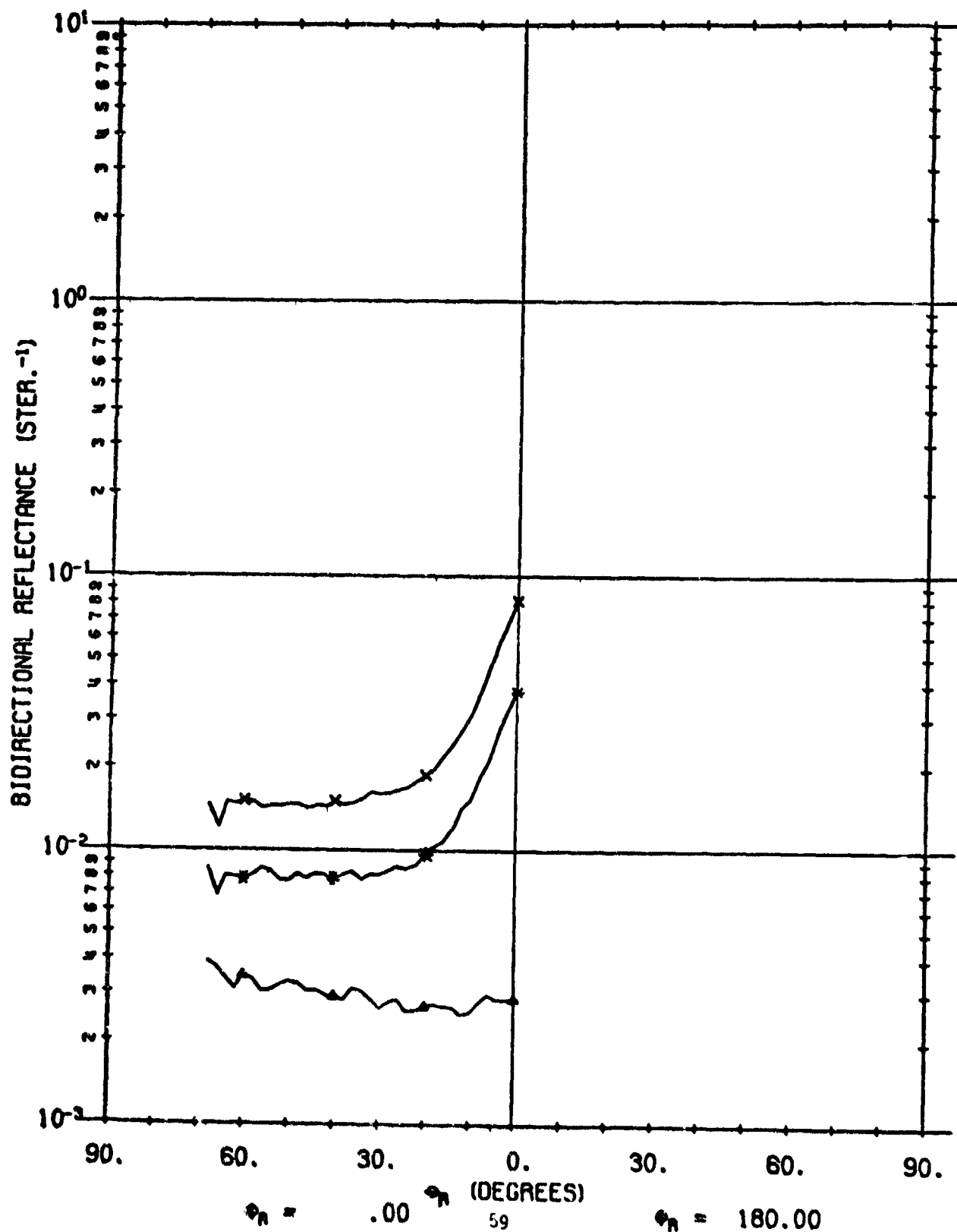
A02023 501

$\lambda = .63$   
 $\phi_i = 1.7$   
 $\phi_i = 180.0$



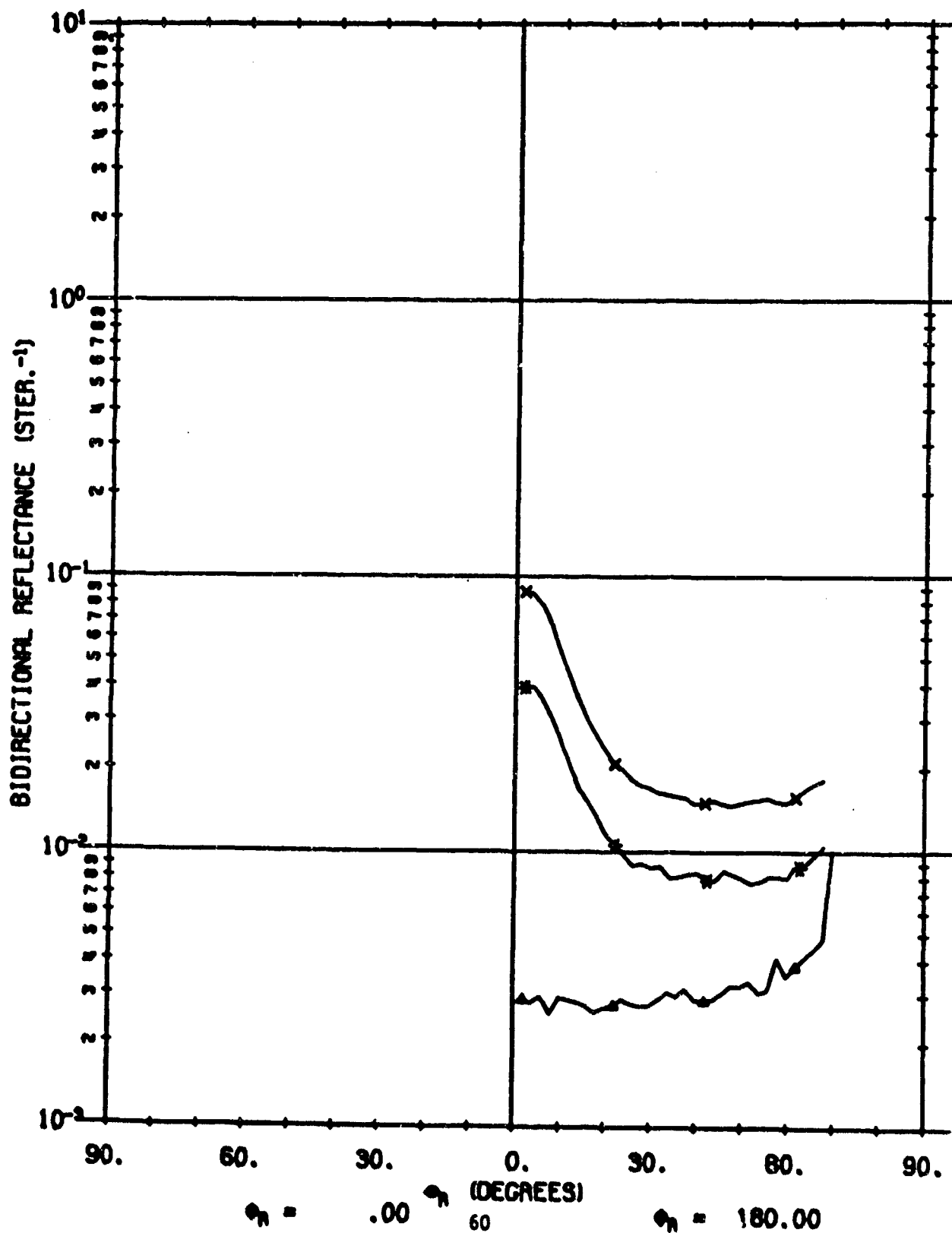
A02023 101

$$\begin{aligned} \lambda &= 1.06 \\ \phi_1 &= \phi_n^+ 1.7 \\ \phi_1 &= .0 \end{aligned}$$



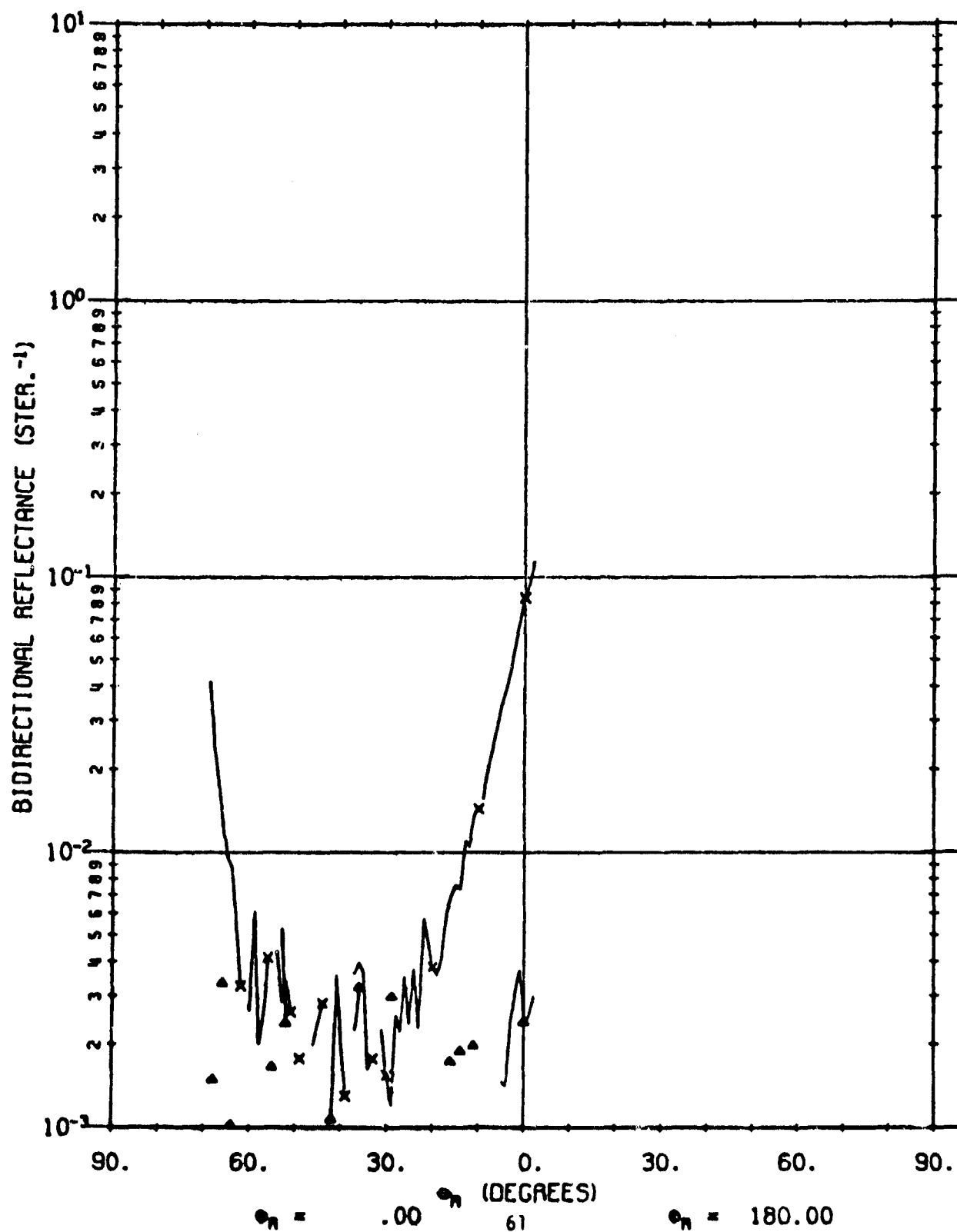
A02023 101

$\lambda = 1.06$   
 $\phi_1 = \phi_1^+ - 1.0$   
 $\phi_1 = 180.0$



A02023 701

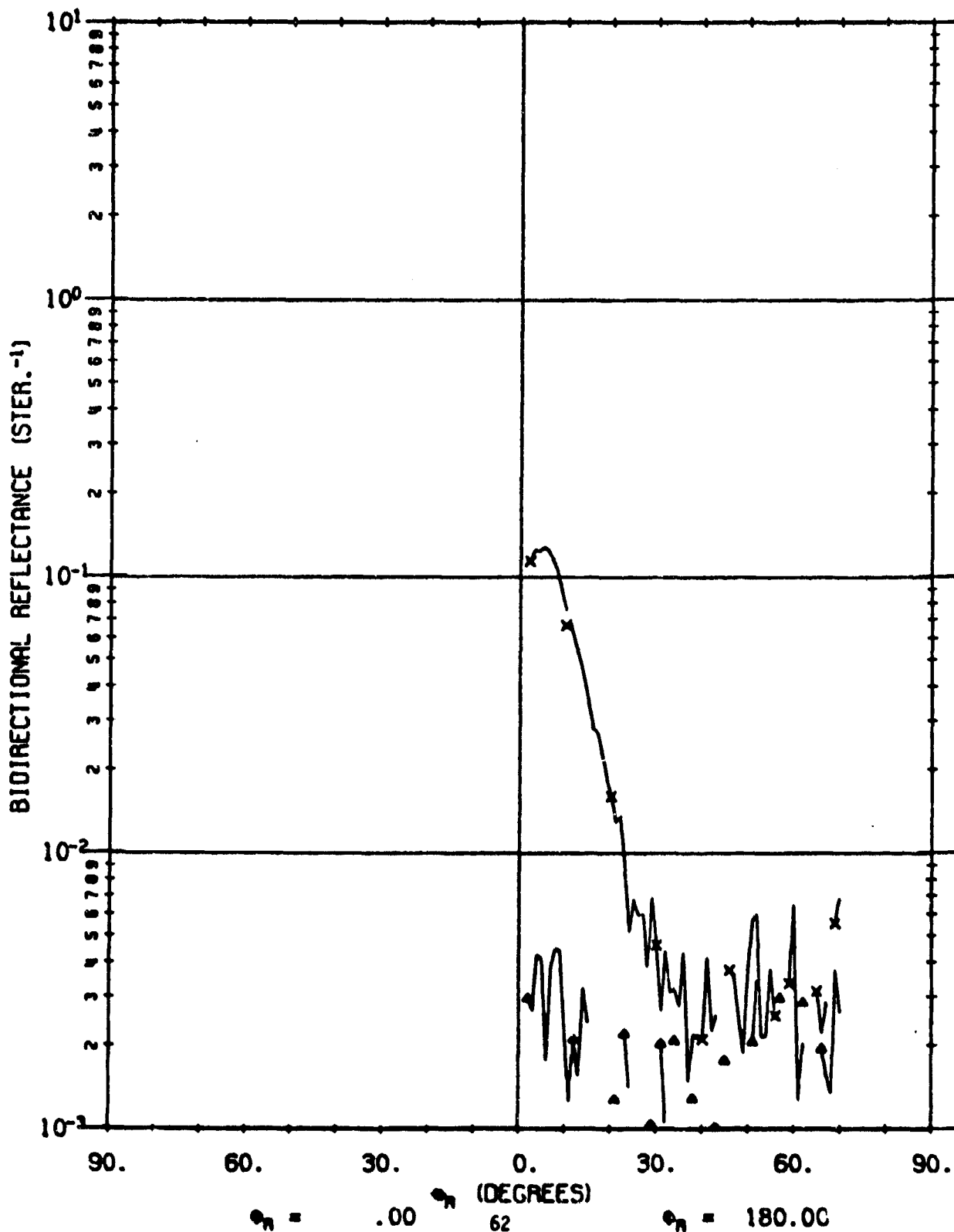
$\lambda = 3.39$   
 $\phi_i = \phi_n^+ 2.0$   
 $\phi_i = .0$





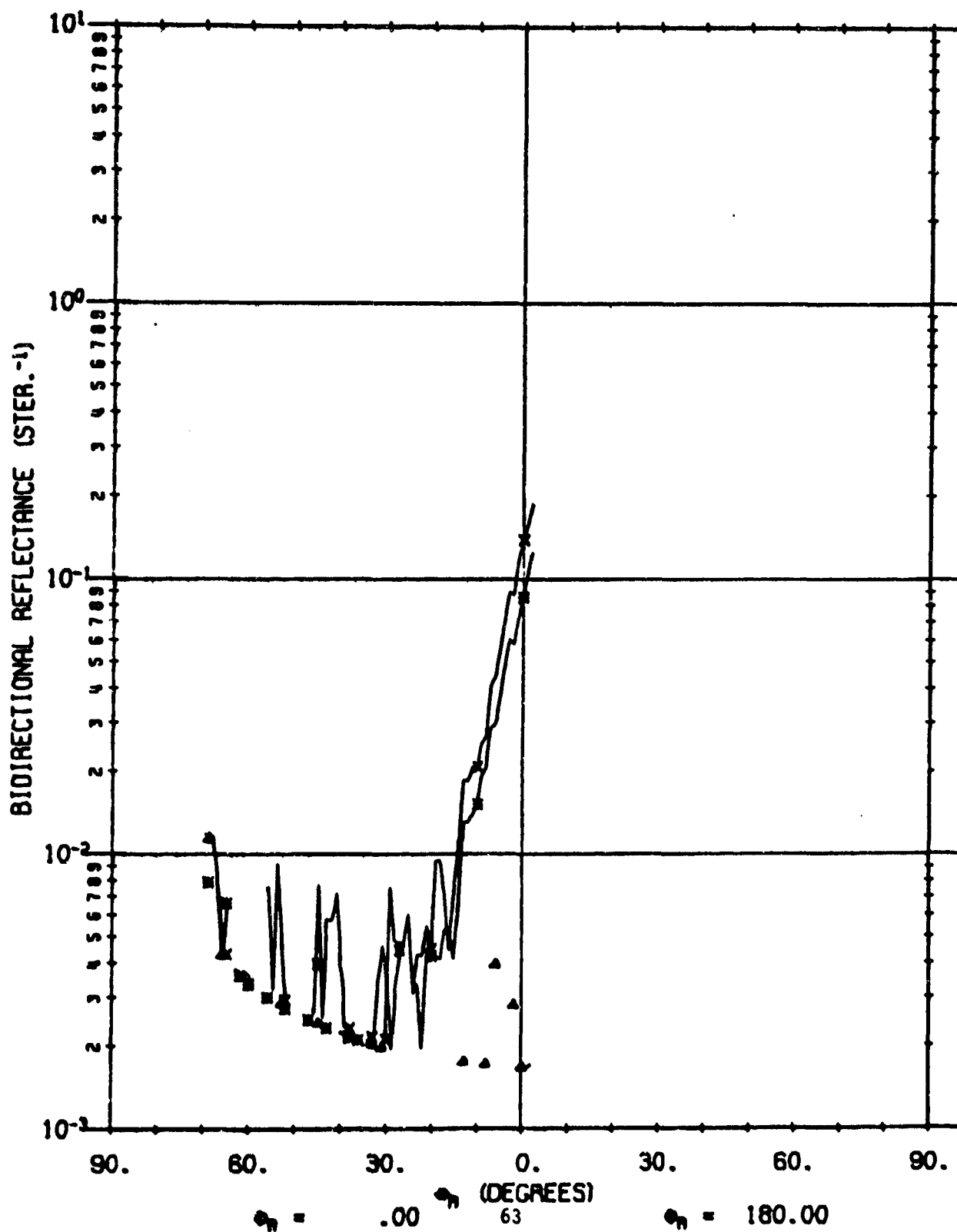
A02023 701

$\lambda = 3.39$   
 $\theta_i = -2.0$   
 $\phi_i = 180.0$



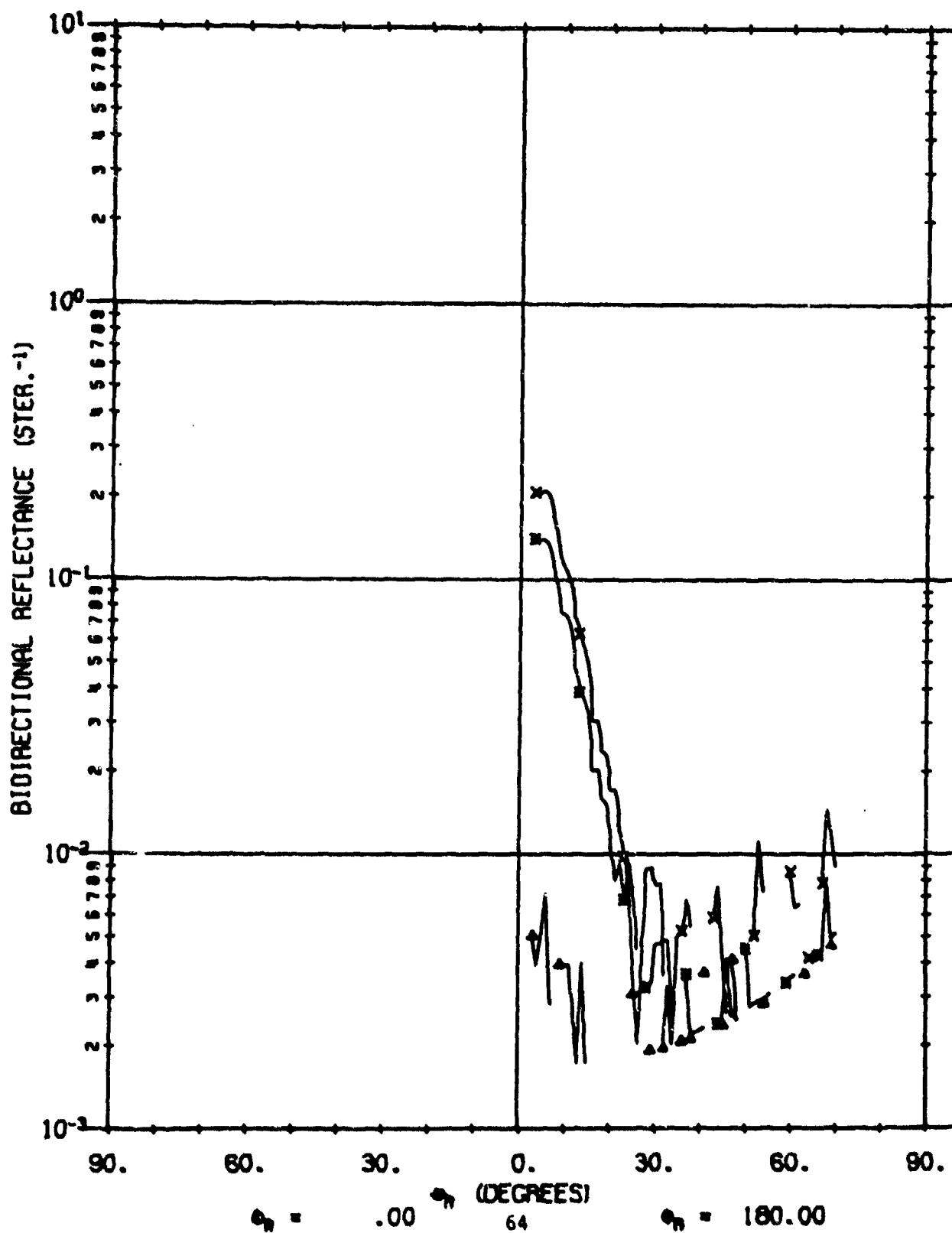
A02023 604

$\lambda = 10.60$   
 $\phi_1 = \phi_2 = 2.5$   
 $\phi_1 = .0$



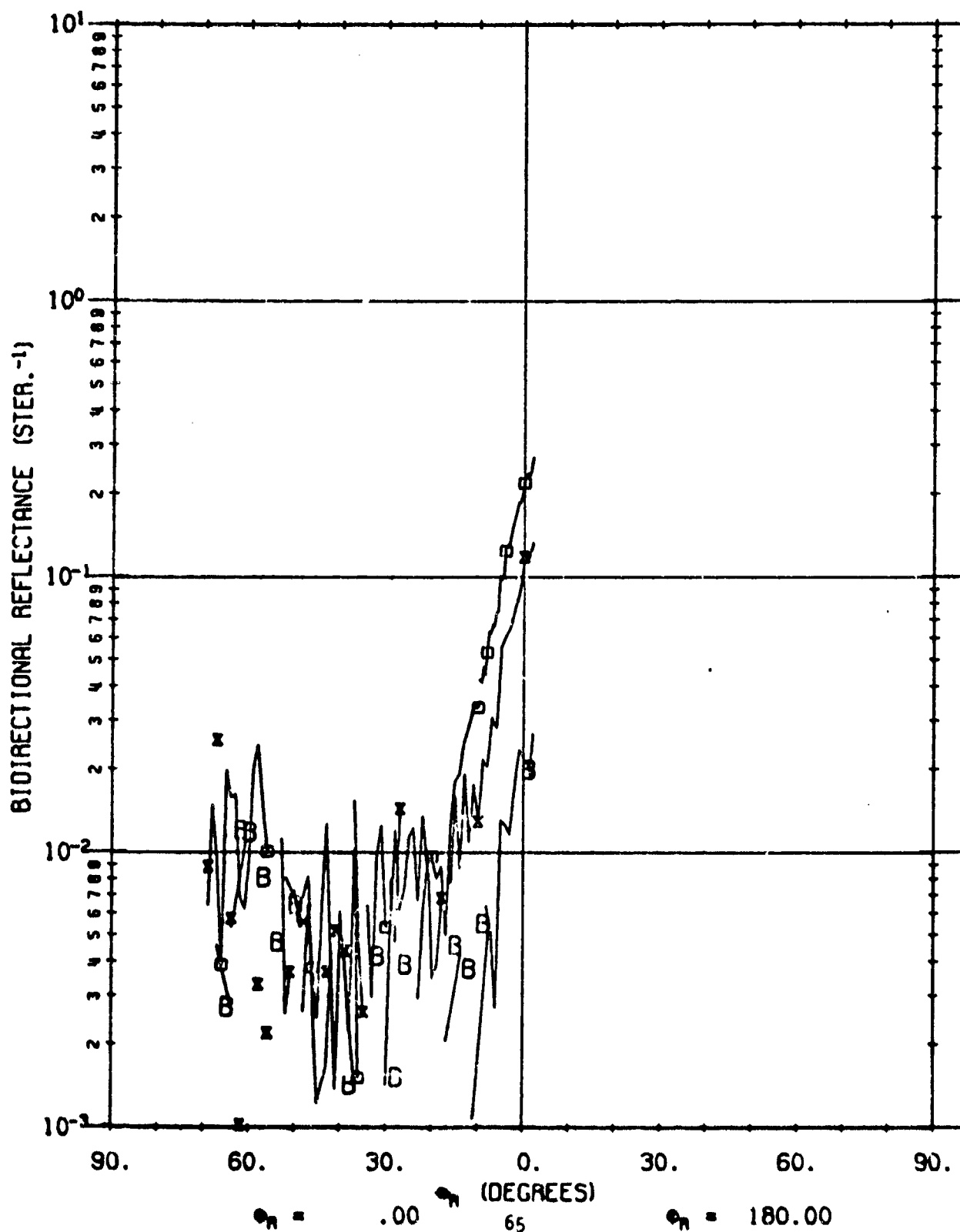
A02023 604

$\lambda = 10.60$   
 $\phi_i = -2.5$   
 $\phi_i = 180.0$



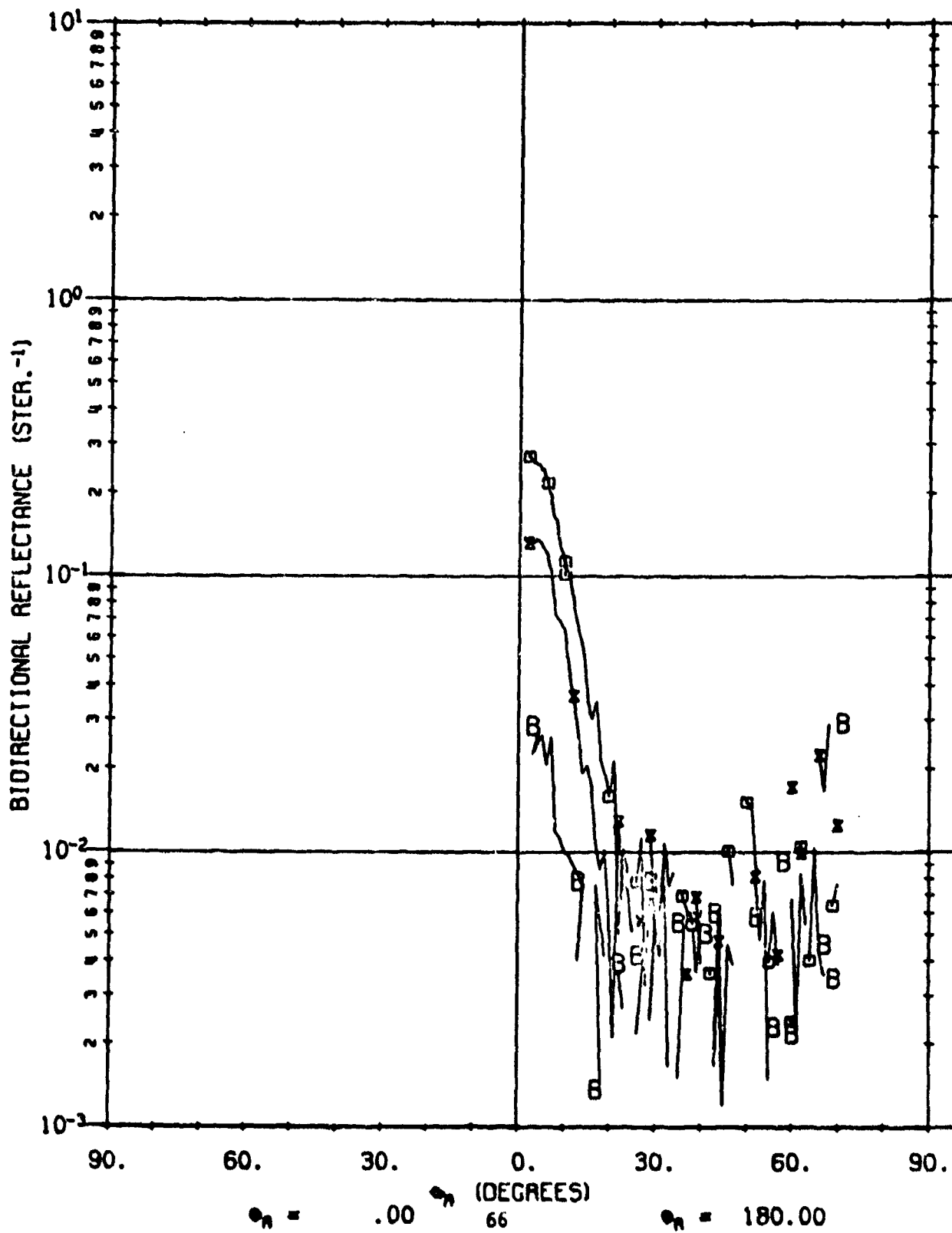
A02023 703

$\lambda = 3.39$   
 $\phi_i = \phi_n + 2.0$   
 $\phi_i = .0$



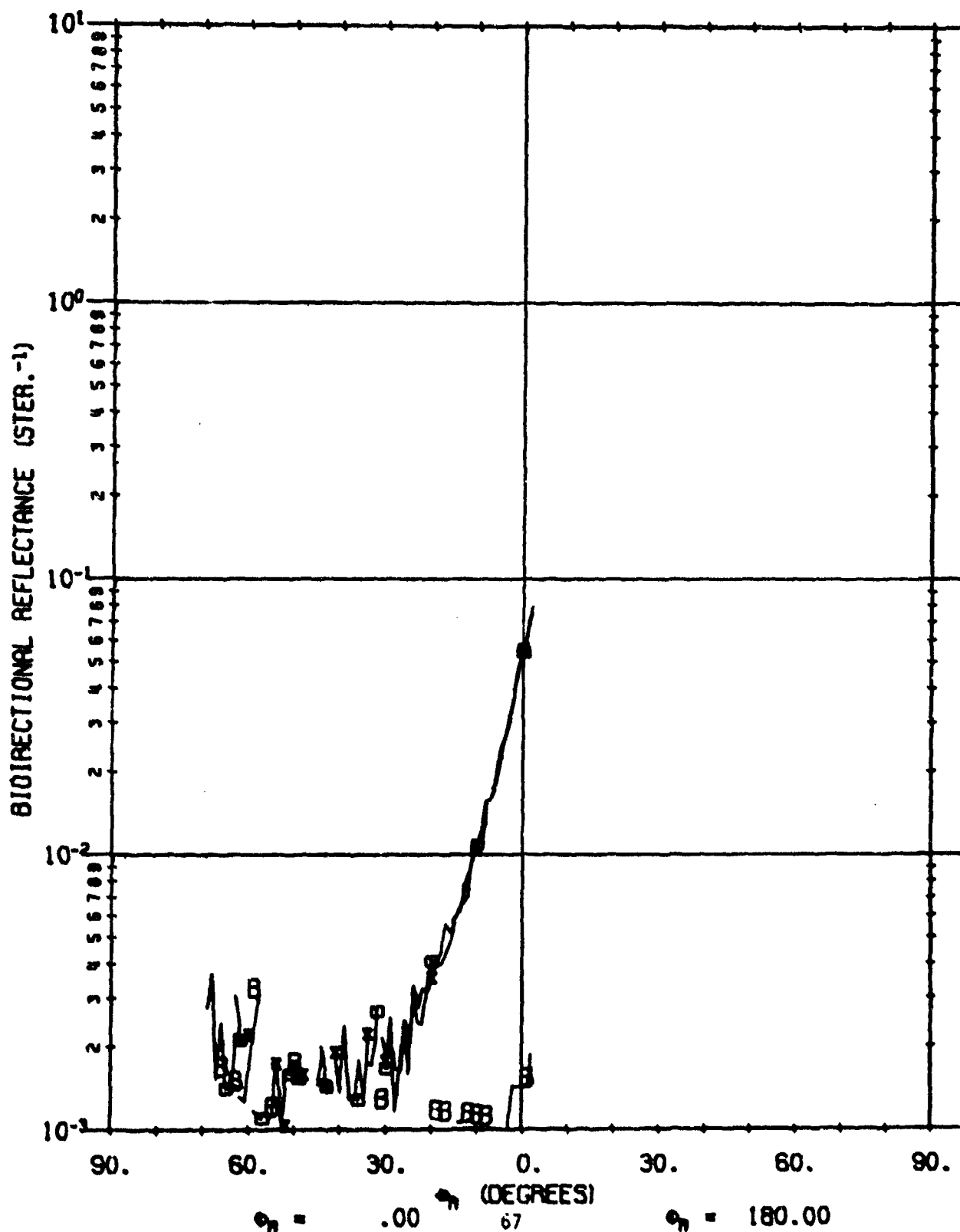
A02023 703

$\lambda = 3.39$   
 $\phi_1 = \phi_2 = -2.0$   
 $\phi_1 = 180.0$



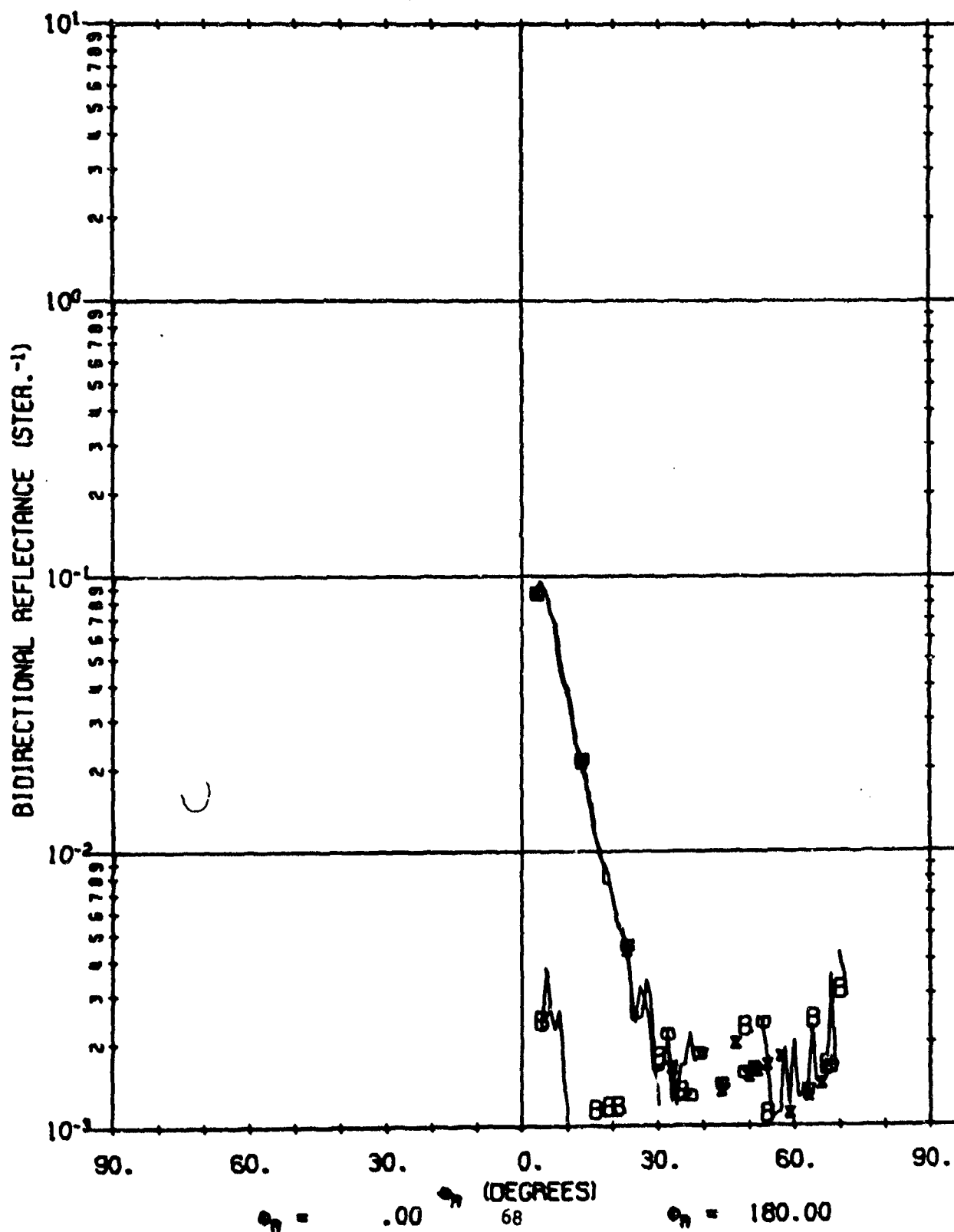
A02023 603

$\lambda = 10.60$   
 $\phi_i = \phi_n^+ 2.5$   
 $\phi_t = .0$



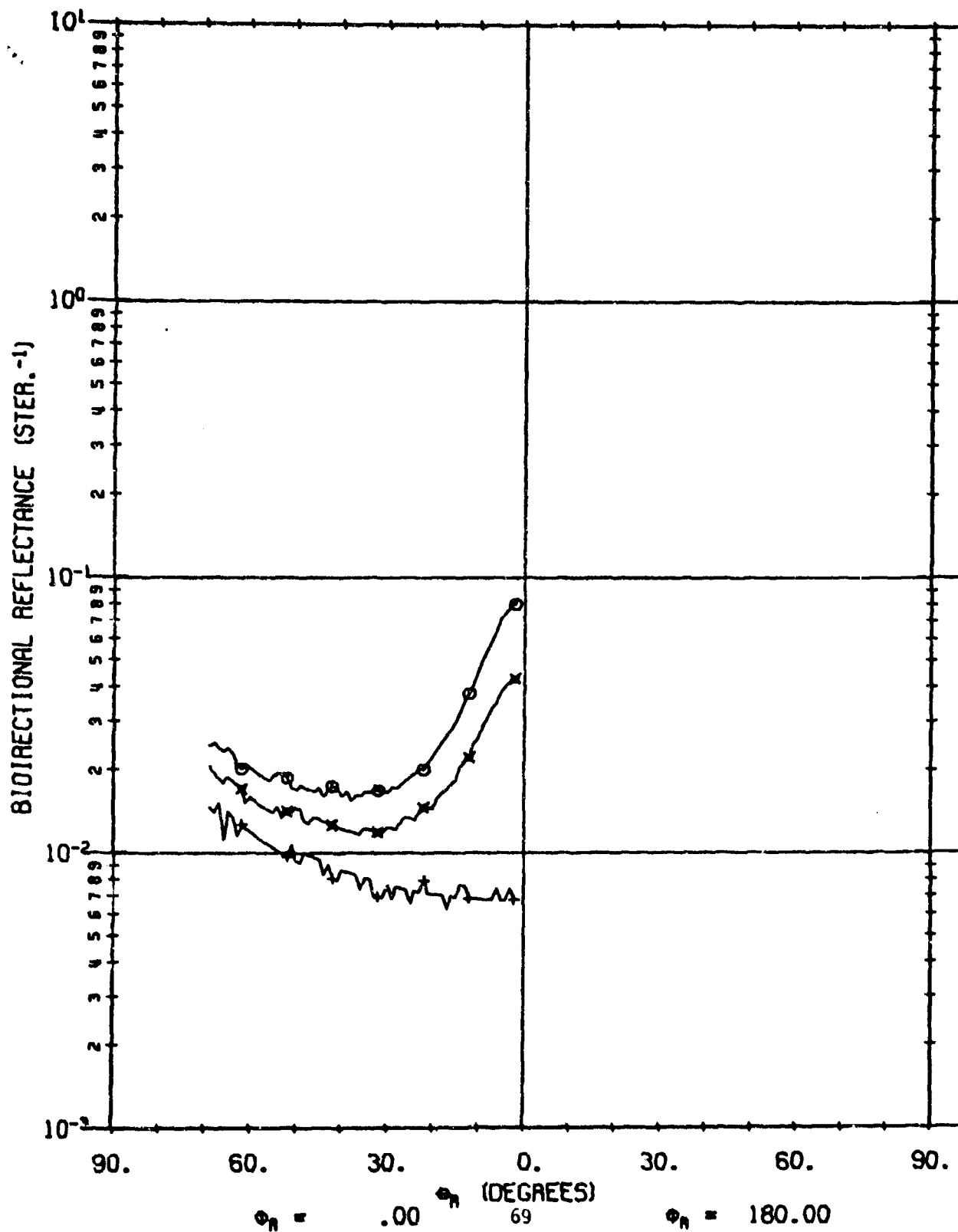
A02023 603

$\lambda = 10.60$   
 $\phi_i = \phi_r = -2.5$   
 $\phi_i = 180.0$



A02023 501

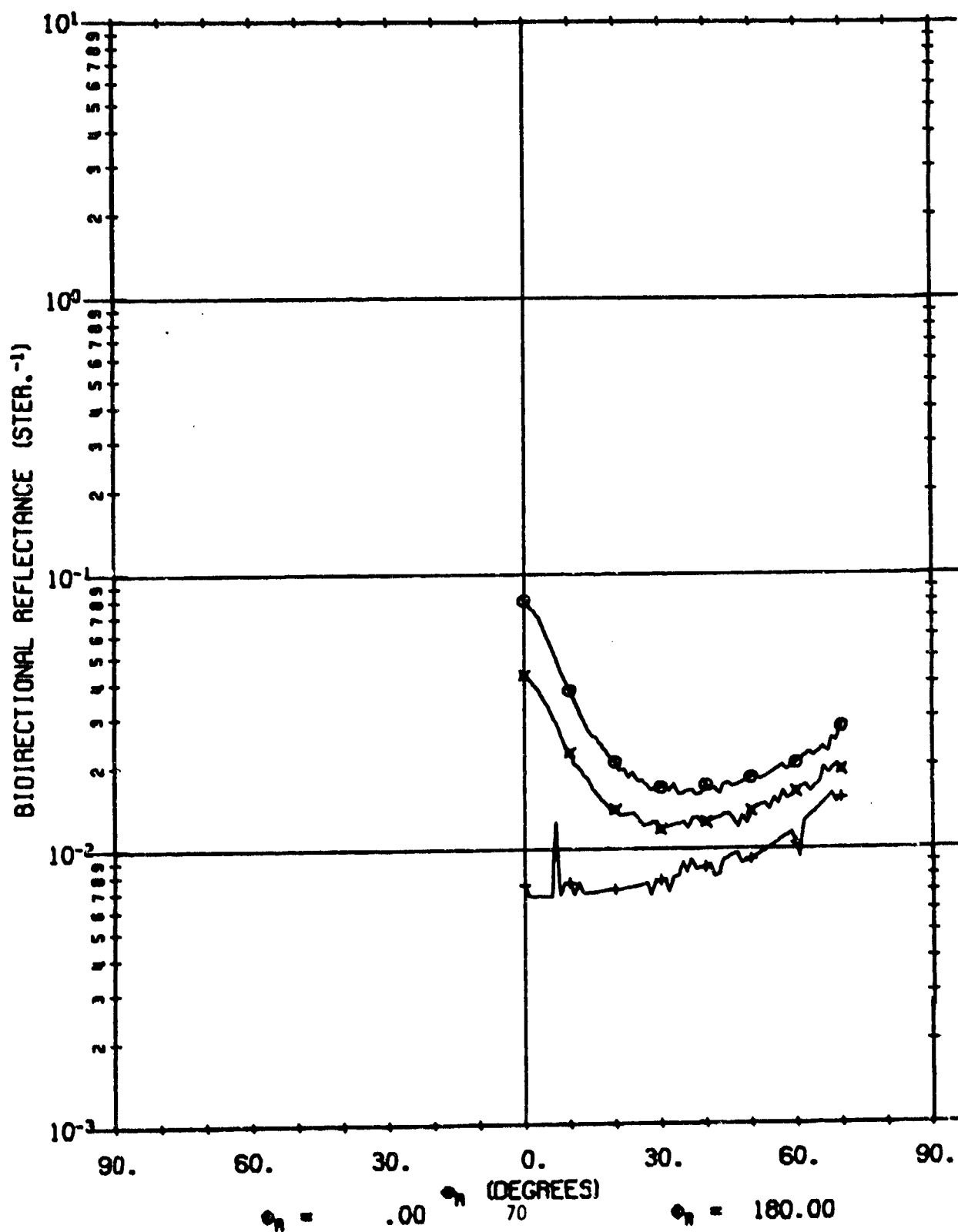
$$\begin{aligned}\lambda &= .63 \\ \phi_i &= \phi_n + -1.7 \\ \phi_i &= .0\end{aligned}$$





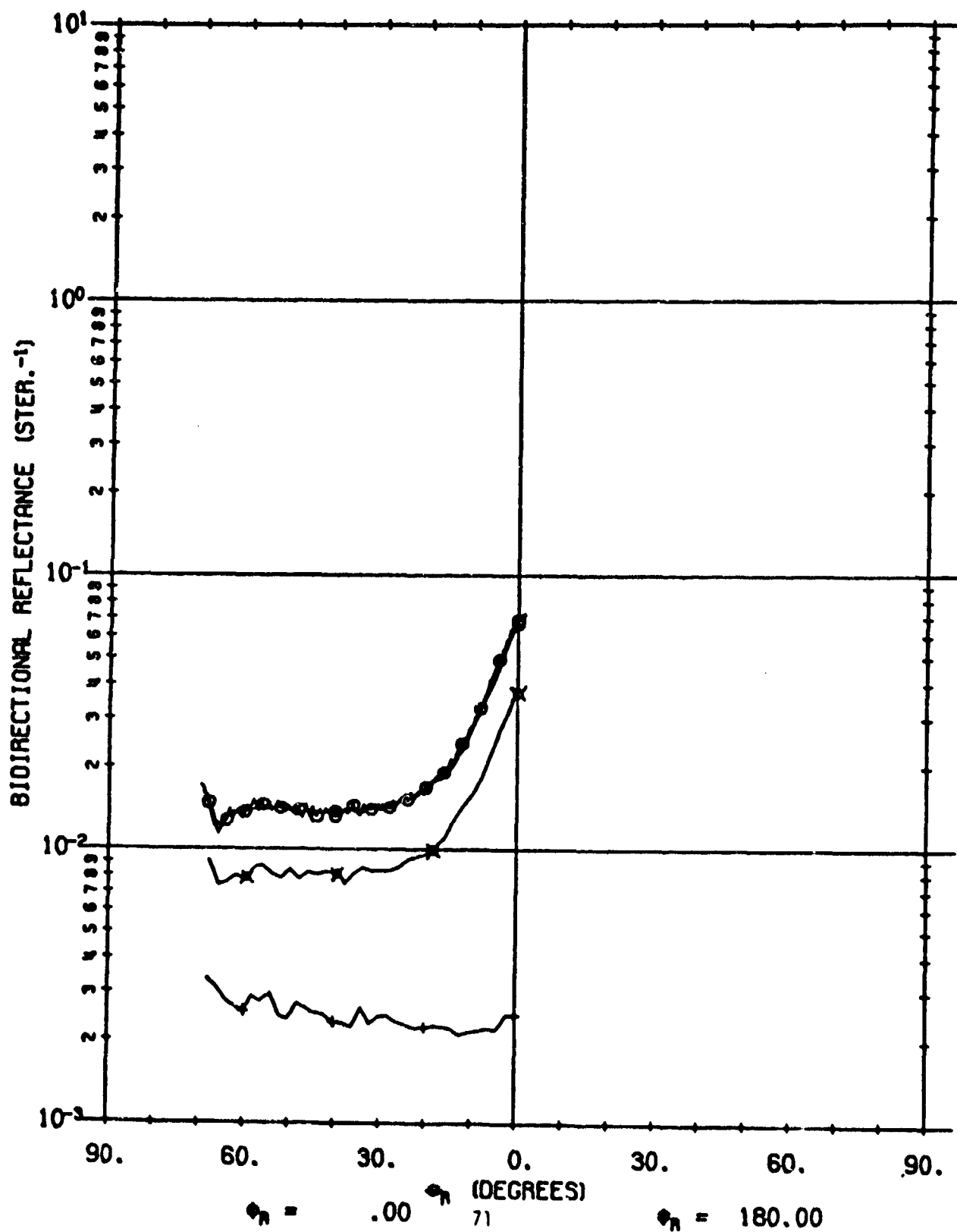
A02023 501

$\lambda = .63$   
 $\theta_i = 1.7$   
 $\theta_t = 180.0$



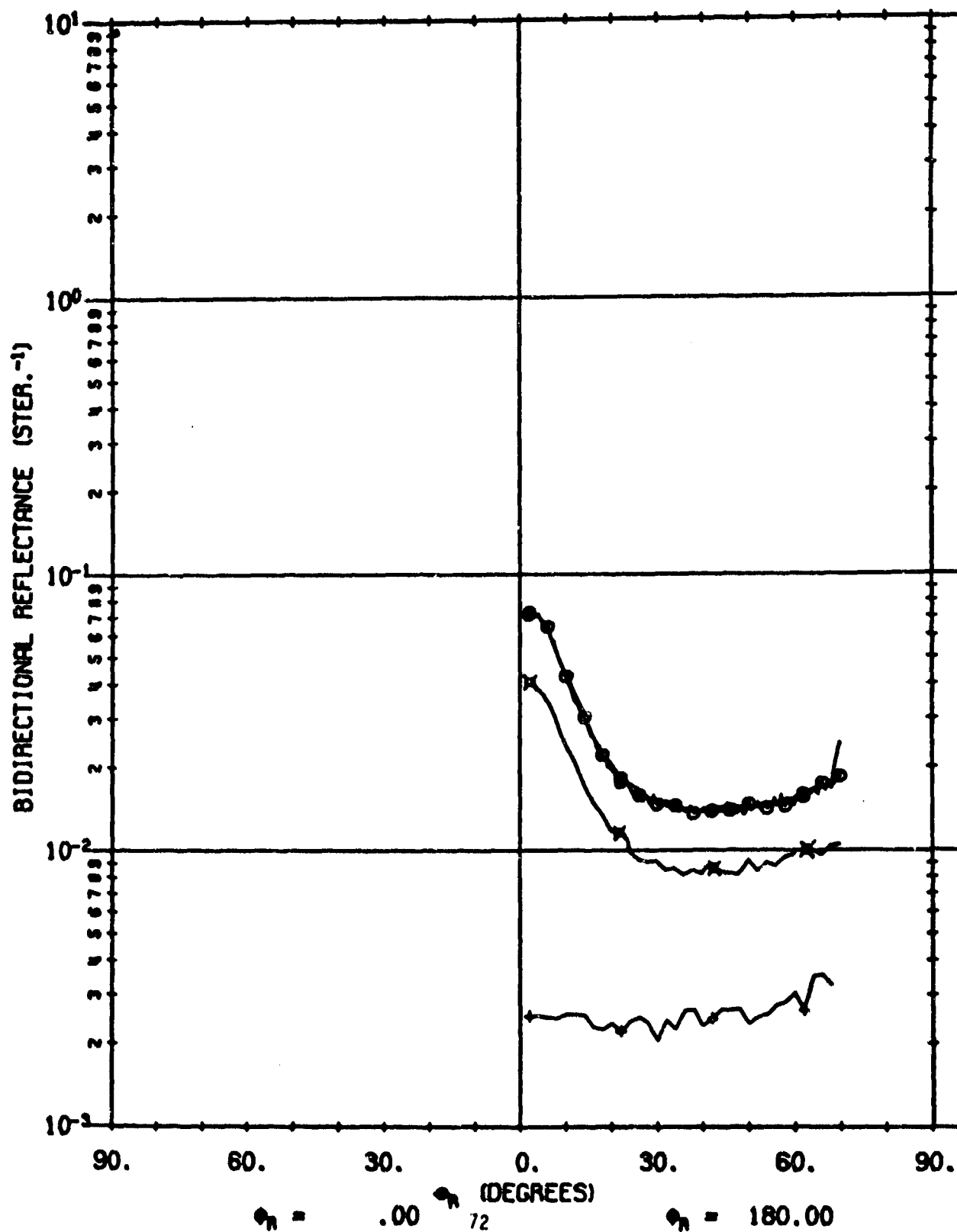
A02023 101

$\lambda = 1.06$   
 $\phi_1 = \phi_2 = 1.7$   
 $\phi_1 = \phi_2 = .0$



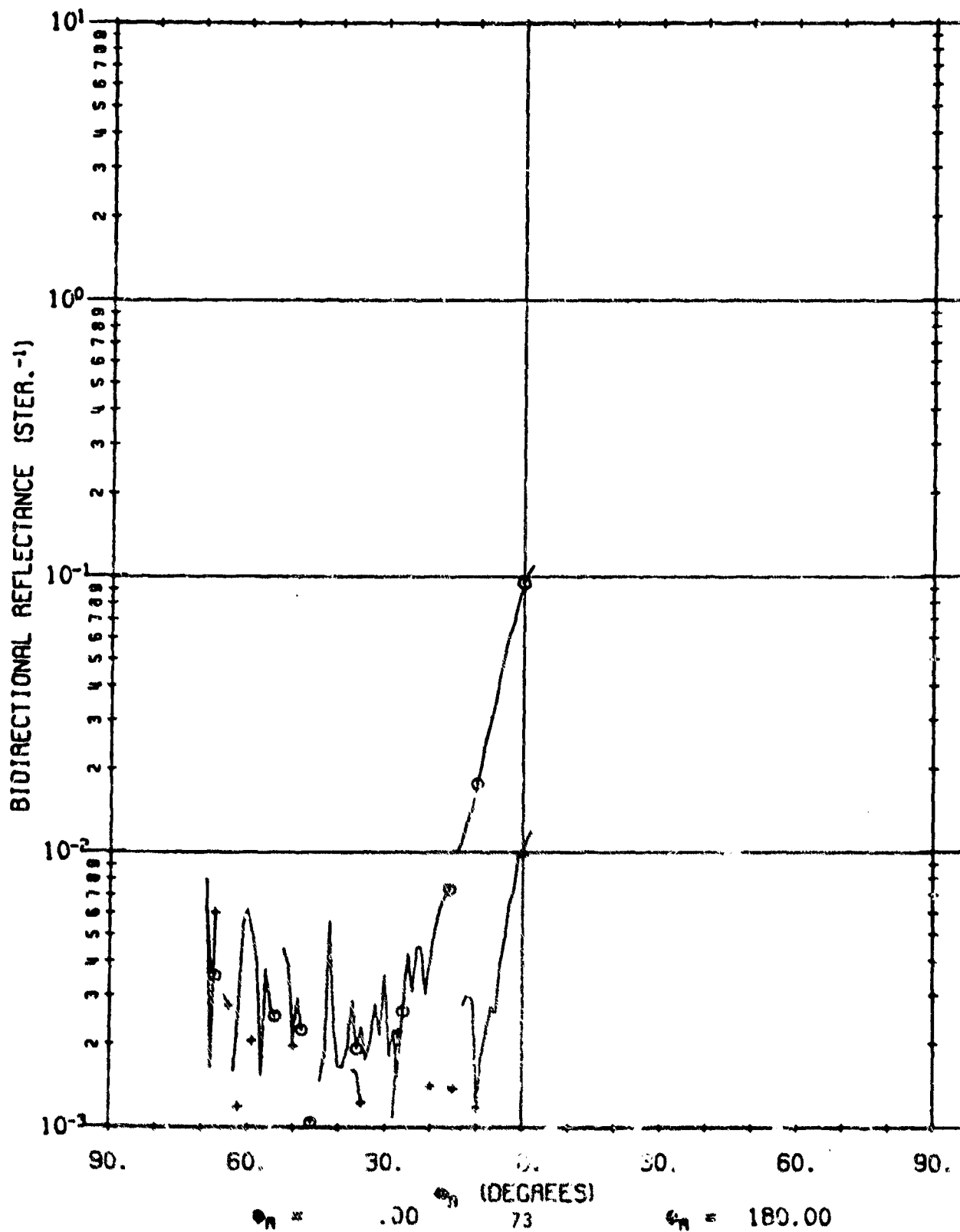
A02023 101

$\lambda = 1.06$   
 $\phi_1 = \phi_2^+ - 1.0$   
 $\phi_1 = 180.0$



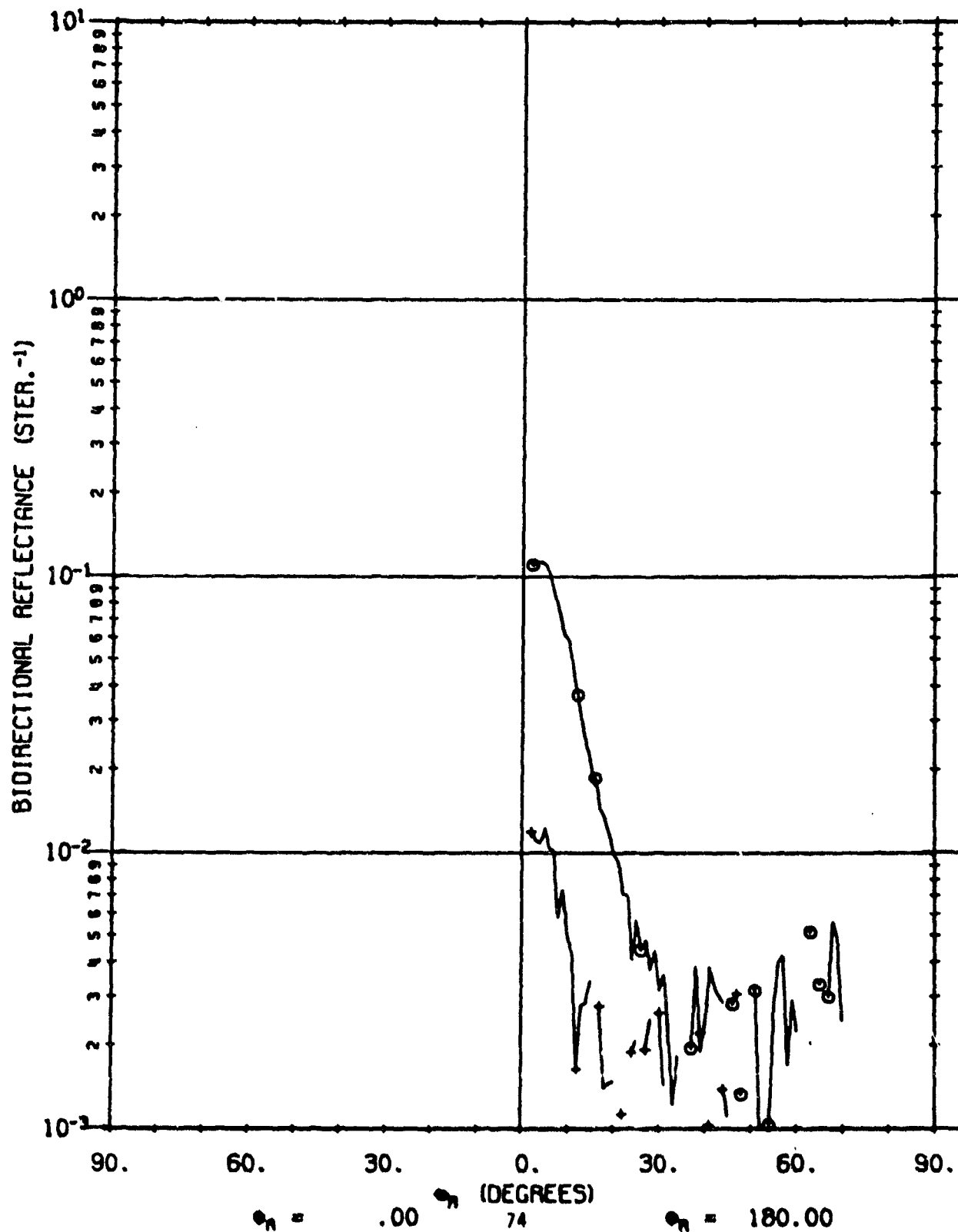
A02023 702

$\lambda = 3.39$   
 $\phi_1 = \phi_n^+ 2.0$   
 $\phi_1 = .0$



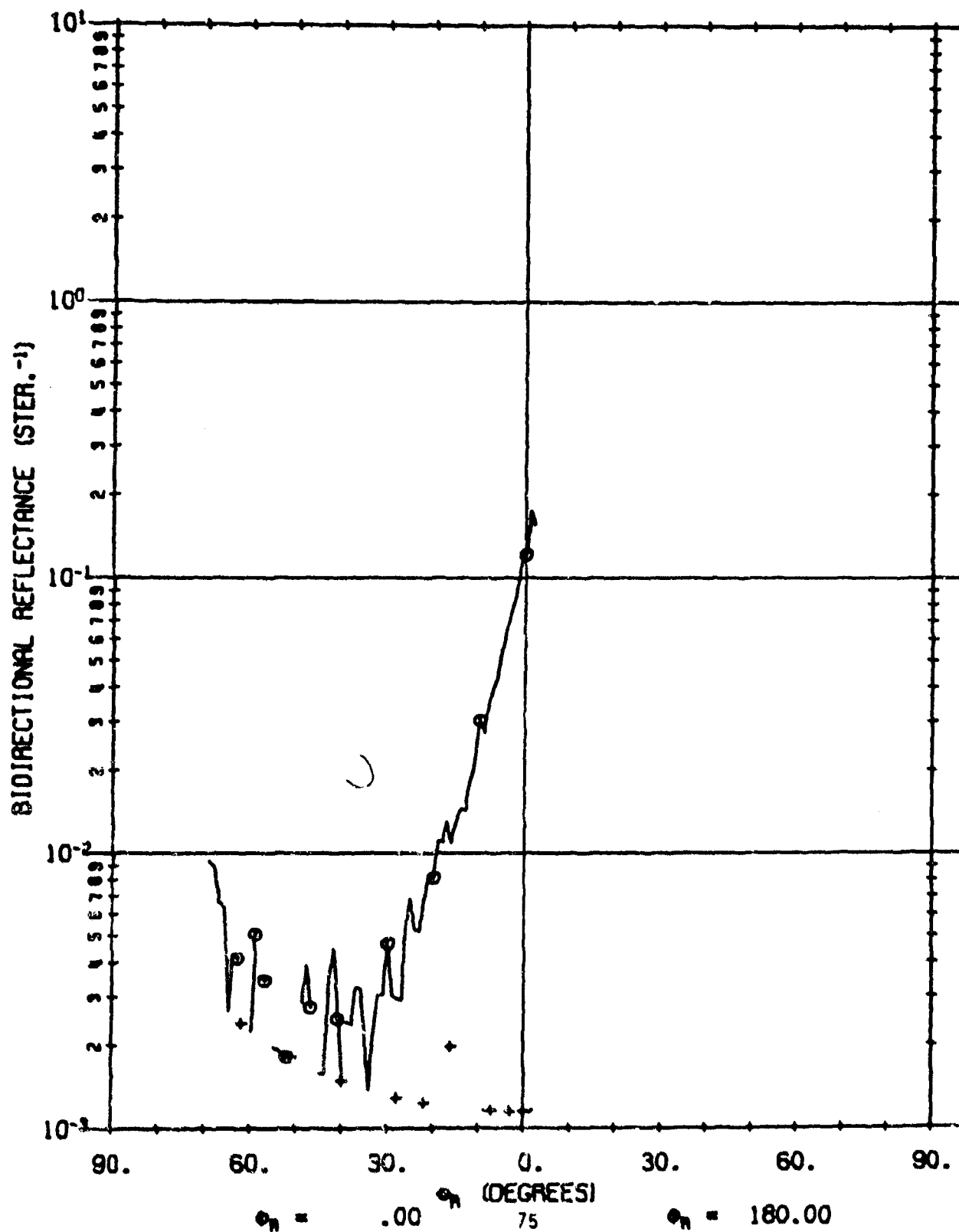
A02023 702

$\lambda = 3.39$   
 $\phi_1 = \phi_2 = -2.0$   
 $\phi_1 = 180.0$



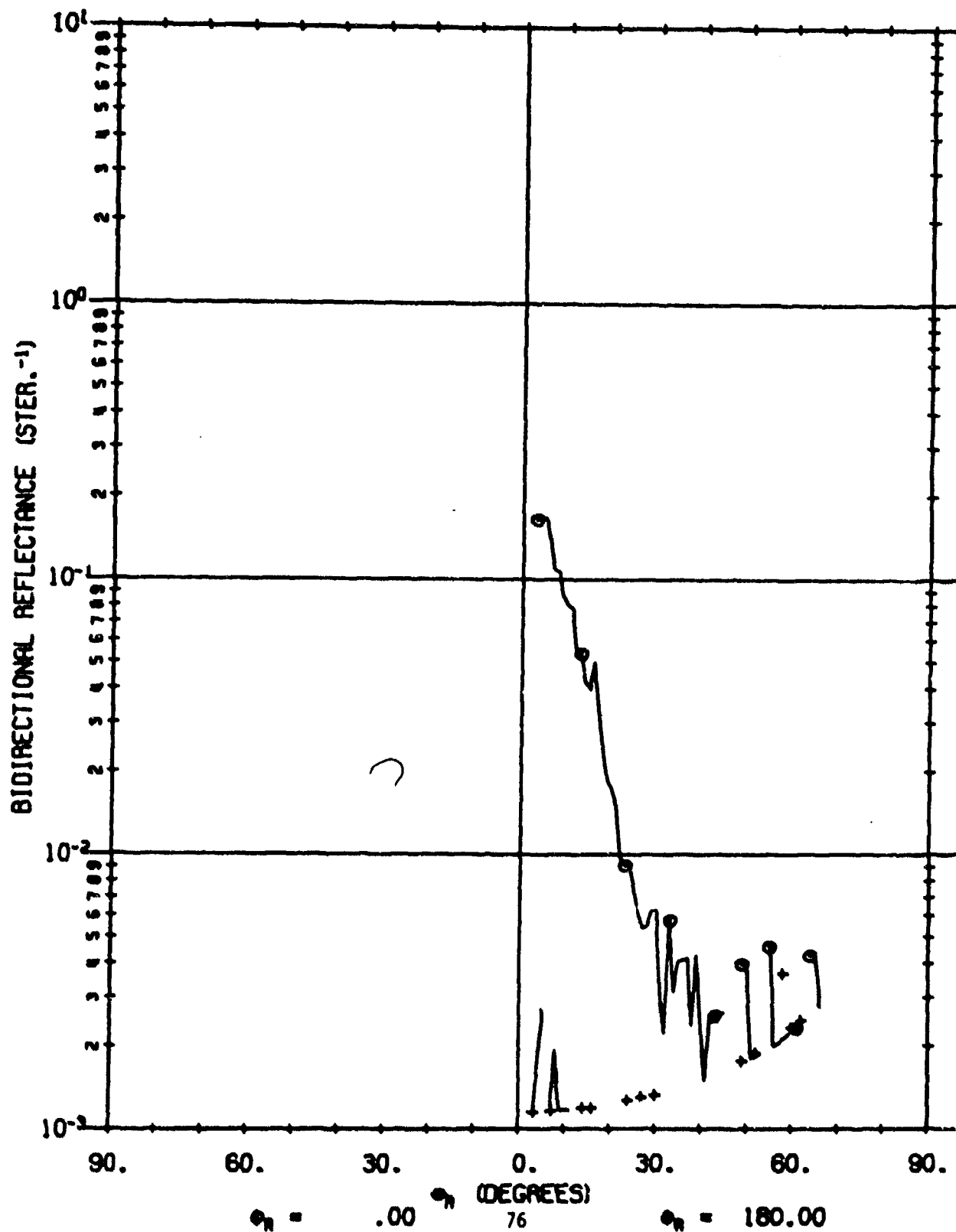
A02023 602

$\lambda = 10.60$   
 $\phi_i = \phi_n + 2.5$   
 $\phi_i = .0$



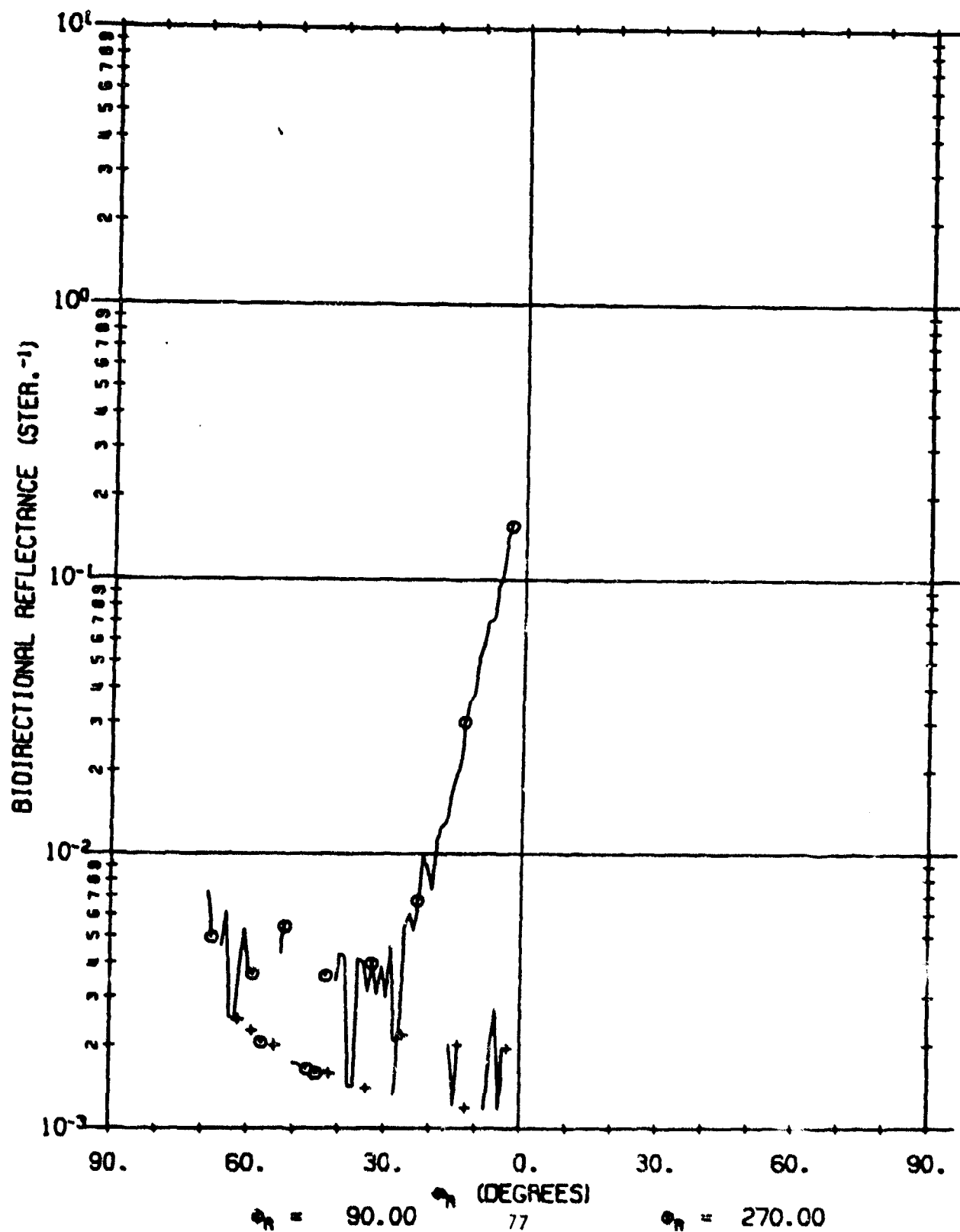
A02023 602

$\lambda = 10.60$   
 $\phi_i = \phi_r = -2.5$   
 $\phi_t = 180.0$



A02023 602

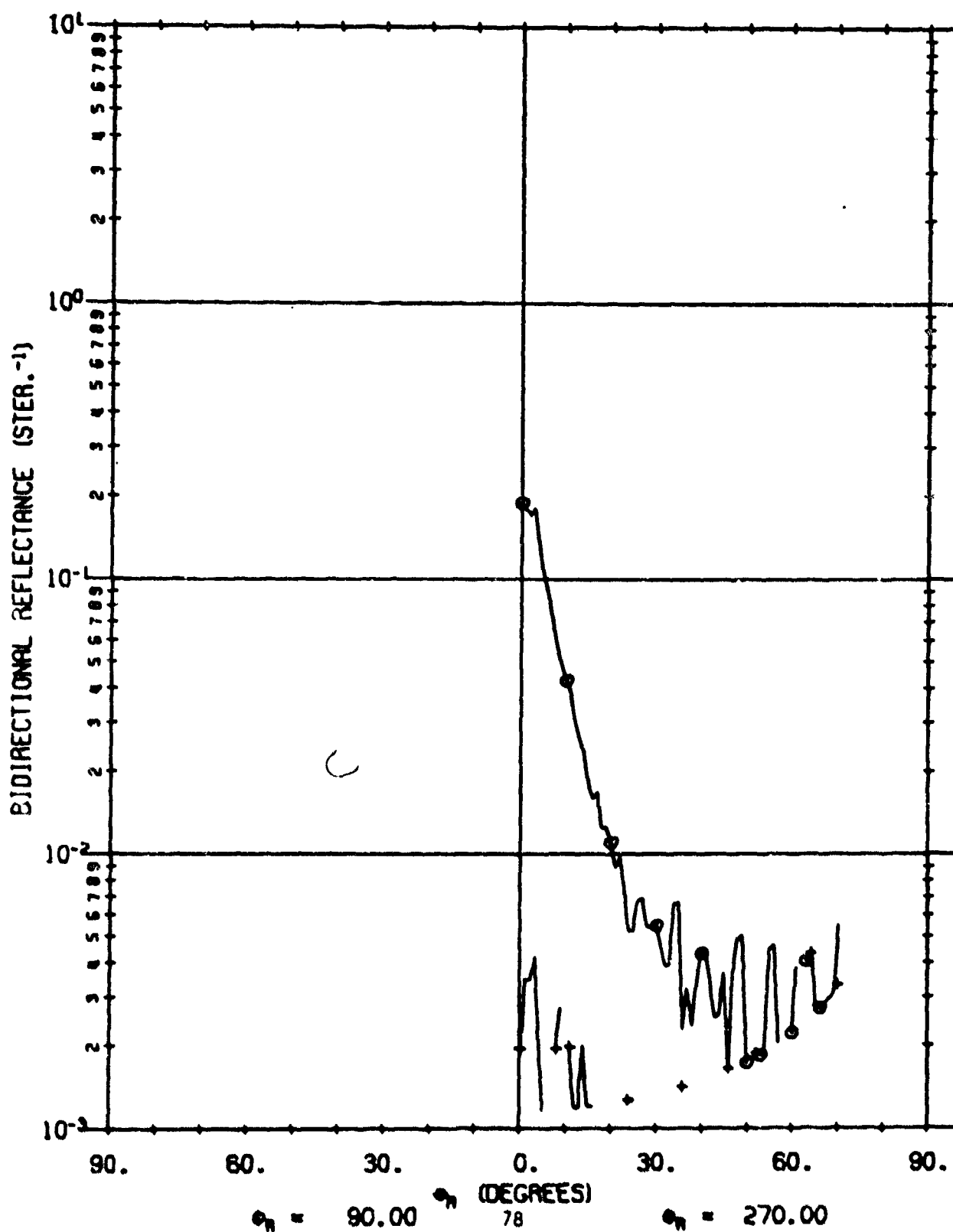
$\lambda = 10.60$   
 $\phi_i = \phi_r^+ - 2.5$   
 $\phi_i = 90.0$





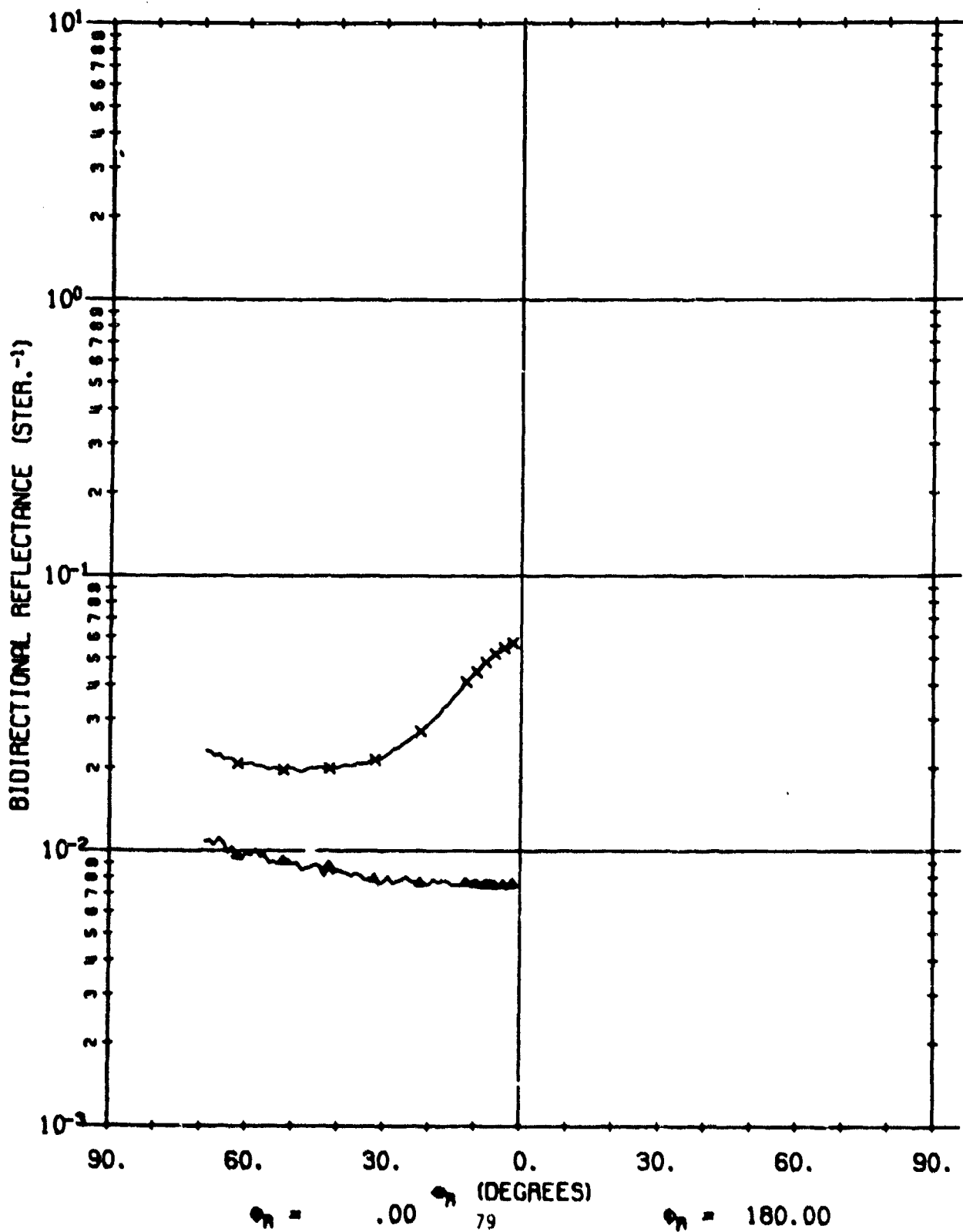
A02023 602

$\lambda = 10.60$   
 $\phi_i = 2.5$   
 $\phi_f = 270.0$



A01610 101

$$\begin{aligned}\lambda &= .63 \\ \phi_i &= \phi_n + -1.7 \\ \phi_i &= .0\end{aligned}$$

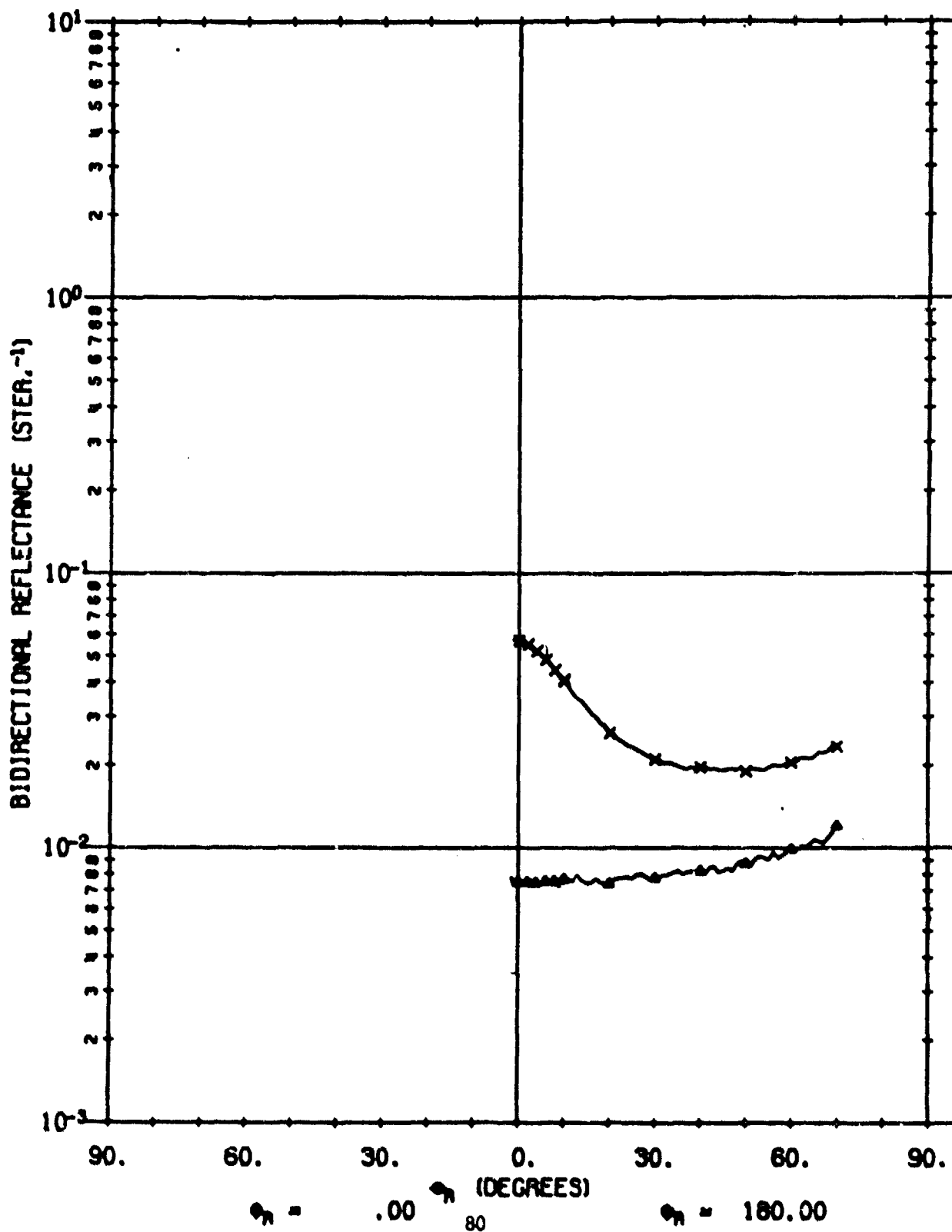


101010

101

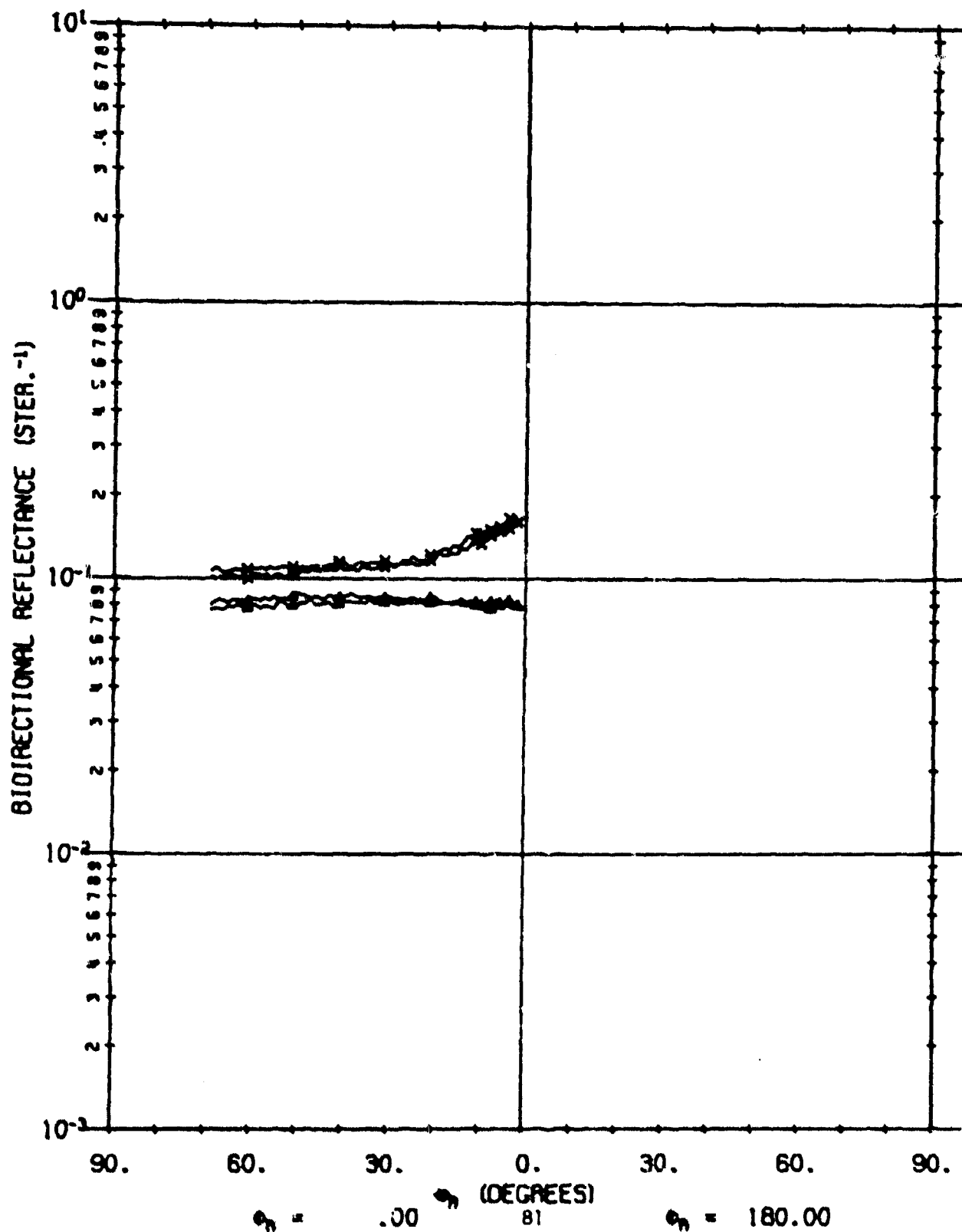
1

$\lambda = .63$   
 $\theta_1 = \theta_2 = 1.7$   
 $\phi_1 = 180.0$



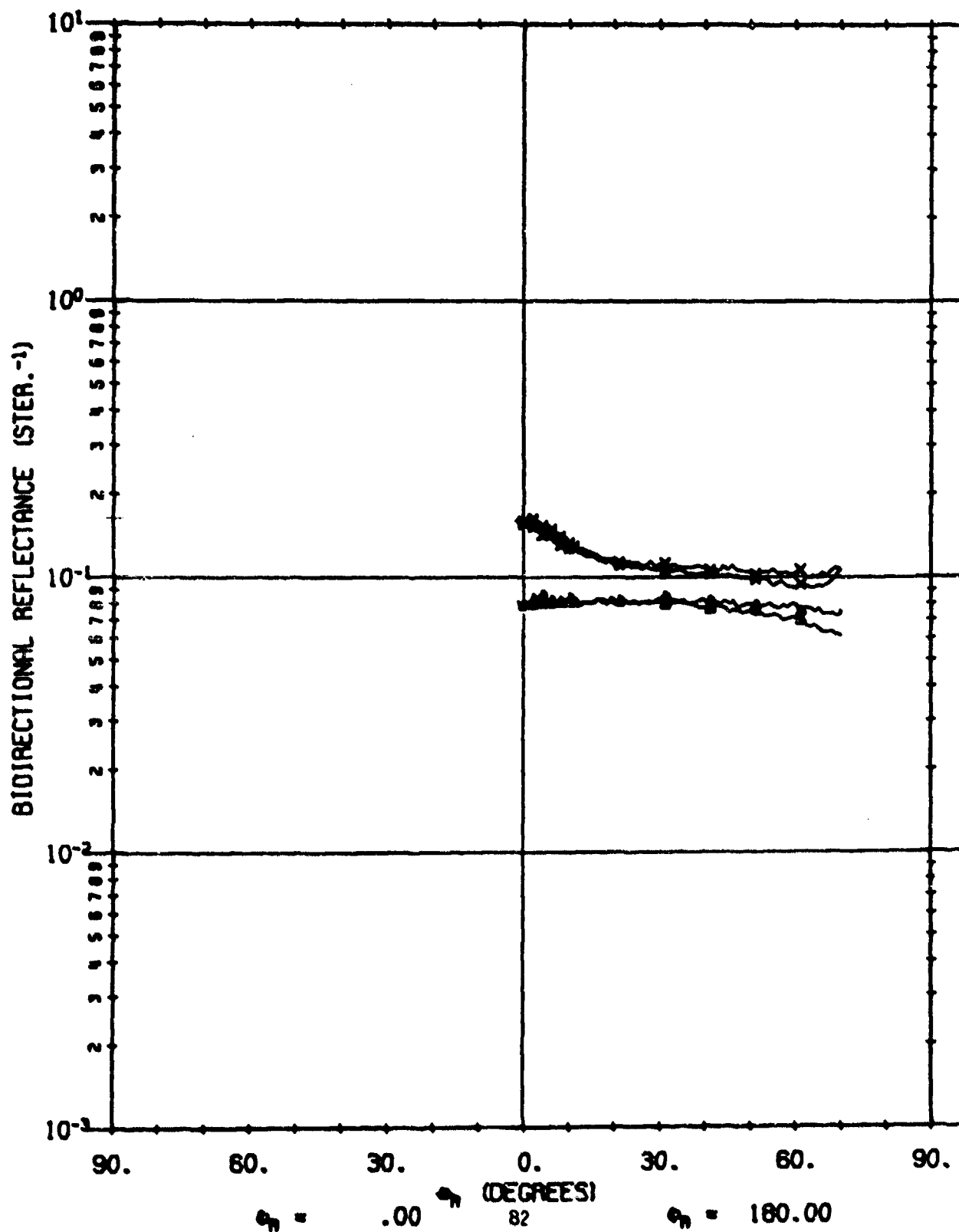
A01610 102

$\lambda = 1.06$   
 $\phi_i = \phi_t = -1.7$   
 $\phi_r = .0$



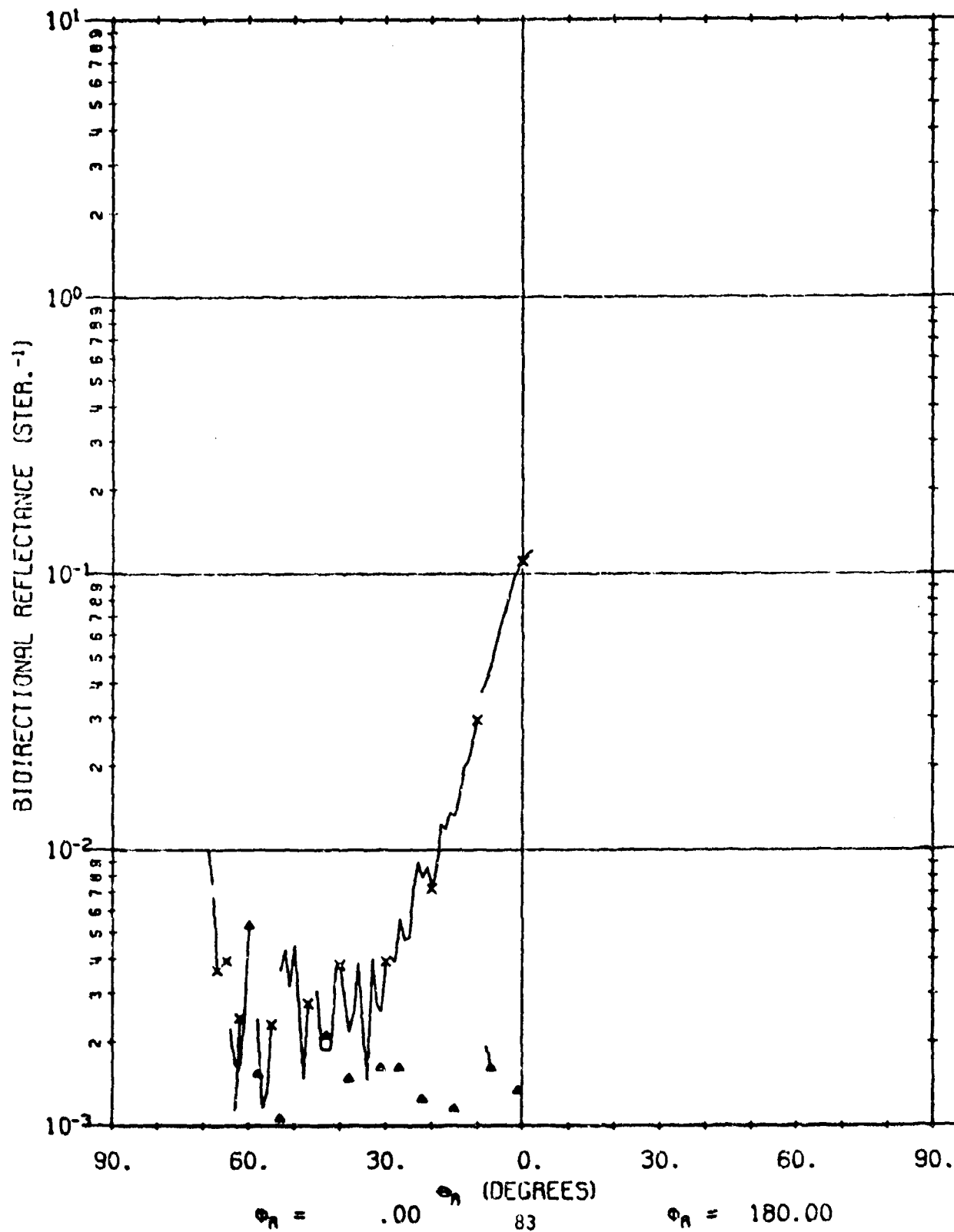
A01610 102

$\lambda = 1.06$   
 $\theta_1 = 1.7$   
 $\theta_i = 180.0$



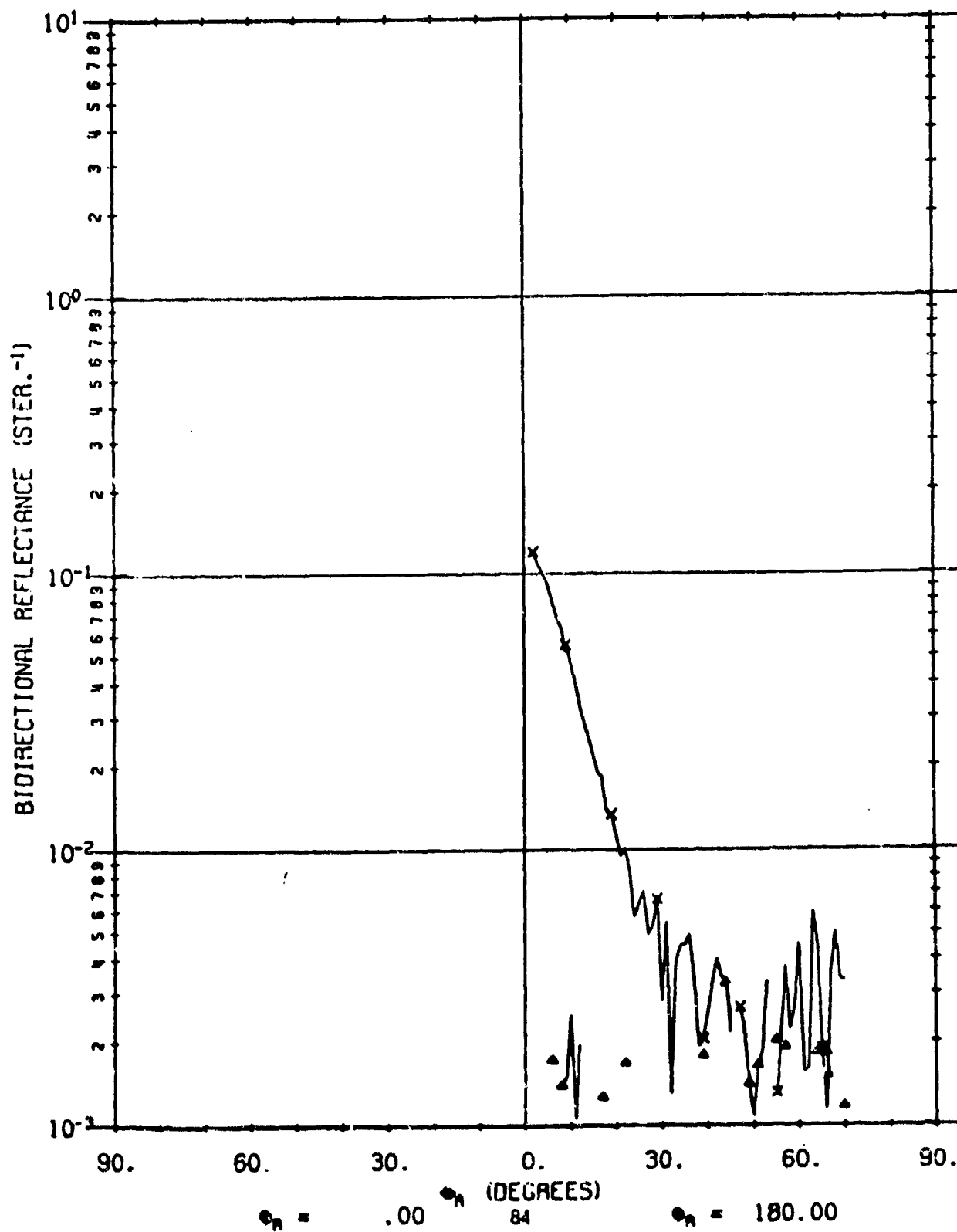
A01610 301

$\lambda = 3.39$   
 $\phi_1 = \phi_R + 2.0$   
 $\phi_1 = .0$



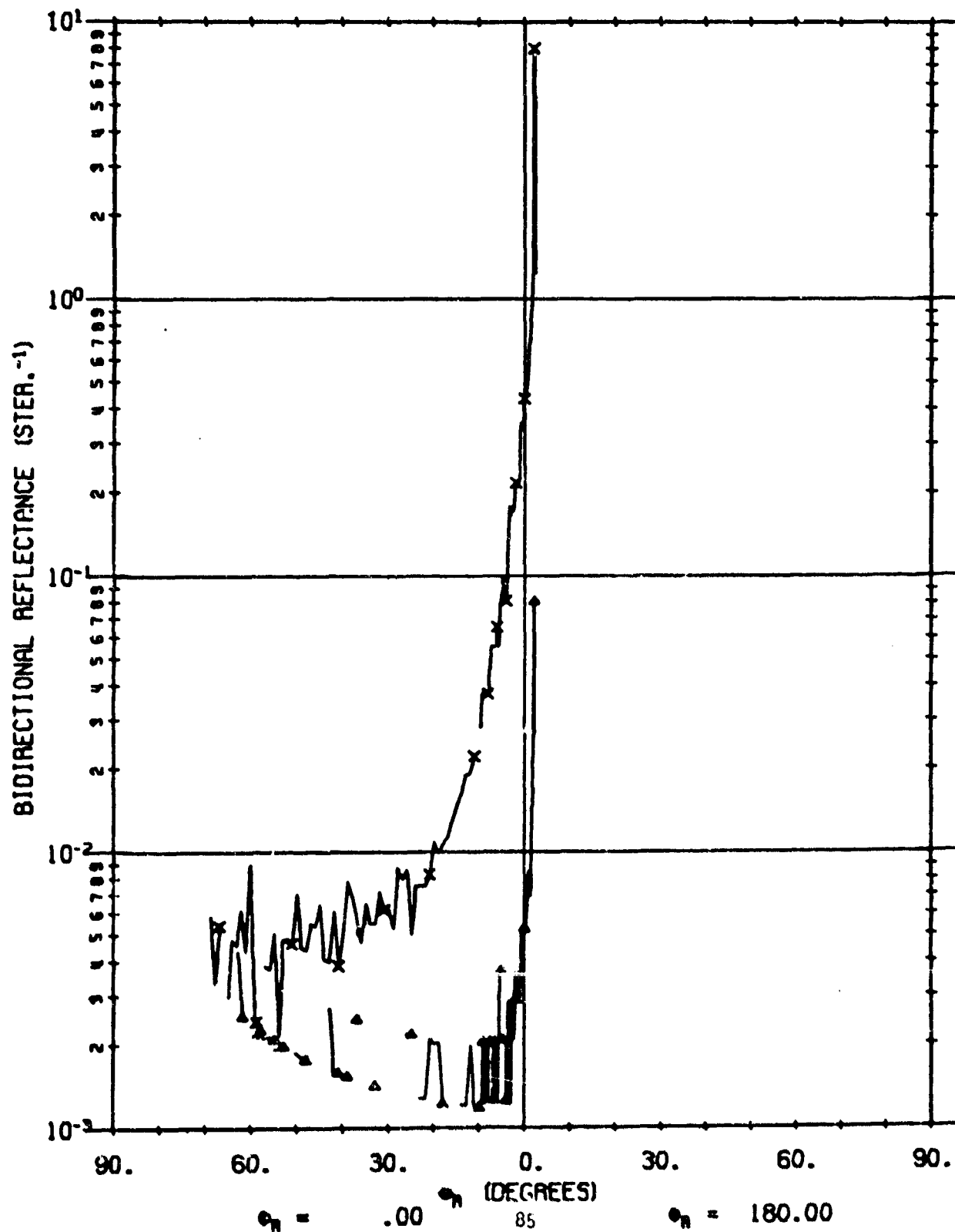
A01610 301

$\lambda = 3.39$   
 $\phi_1 = -2.0$   
 $\phi_2 = 180.0$



A01610 201

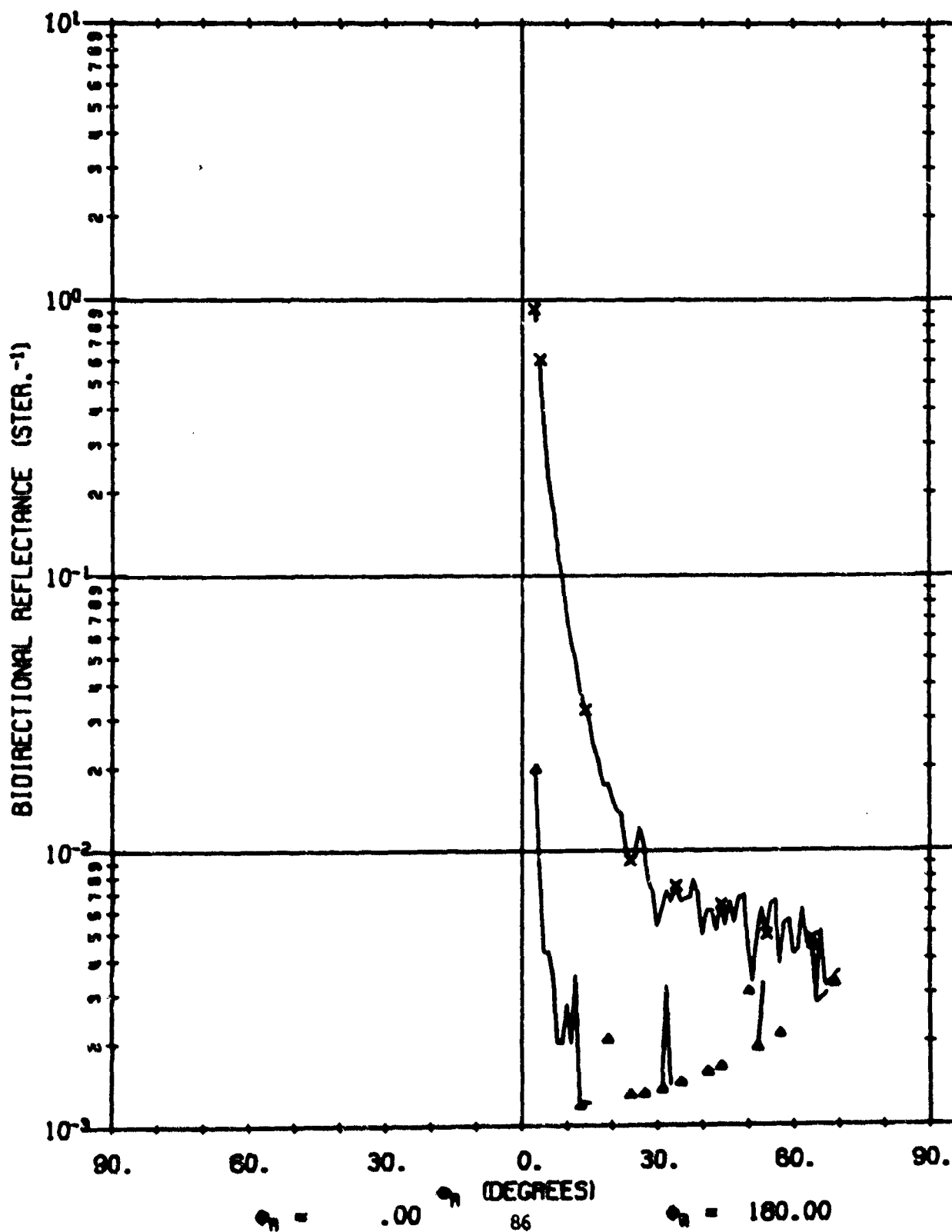
$\lambda = 10.60$   
 $\phi_i = \phi_n^+ 2.5$   
 $\phi_i = .0$





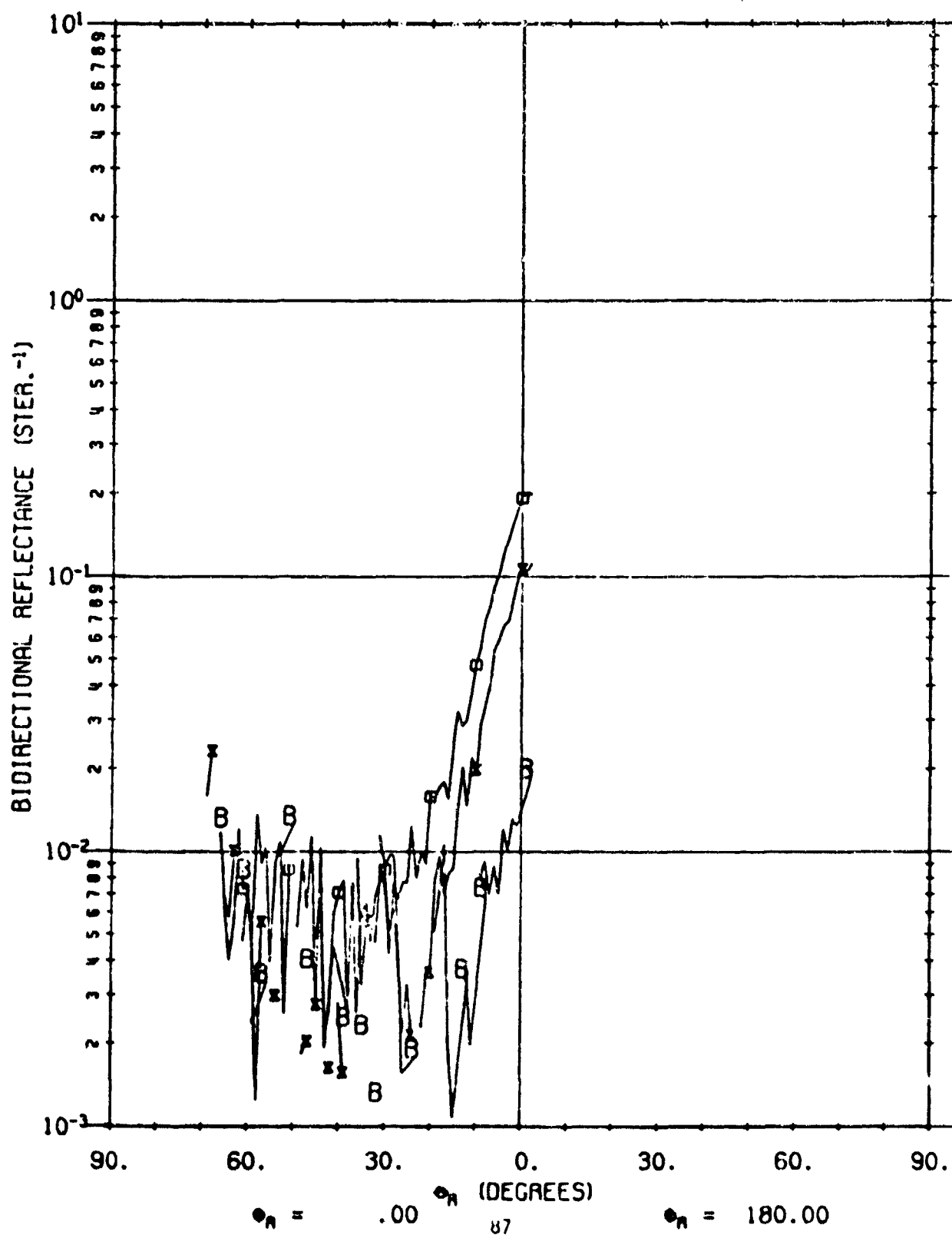
A01610 201

$\lambda = 10.60$   
 $\phi_1 = -2.5$   
 $\phi_2 = 180.0$



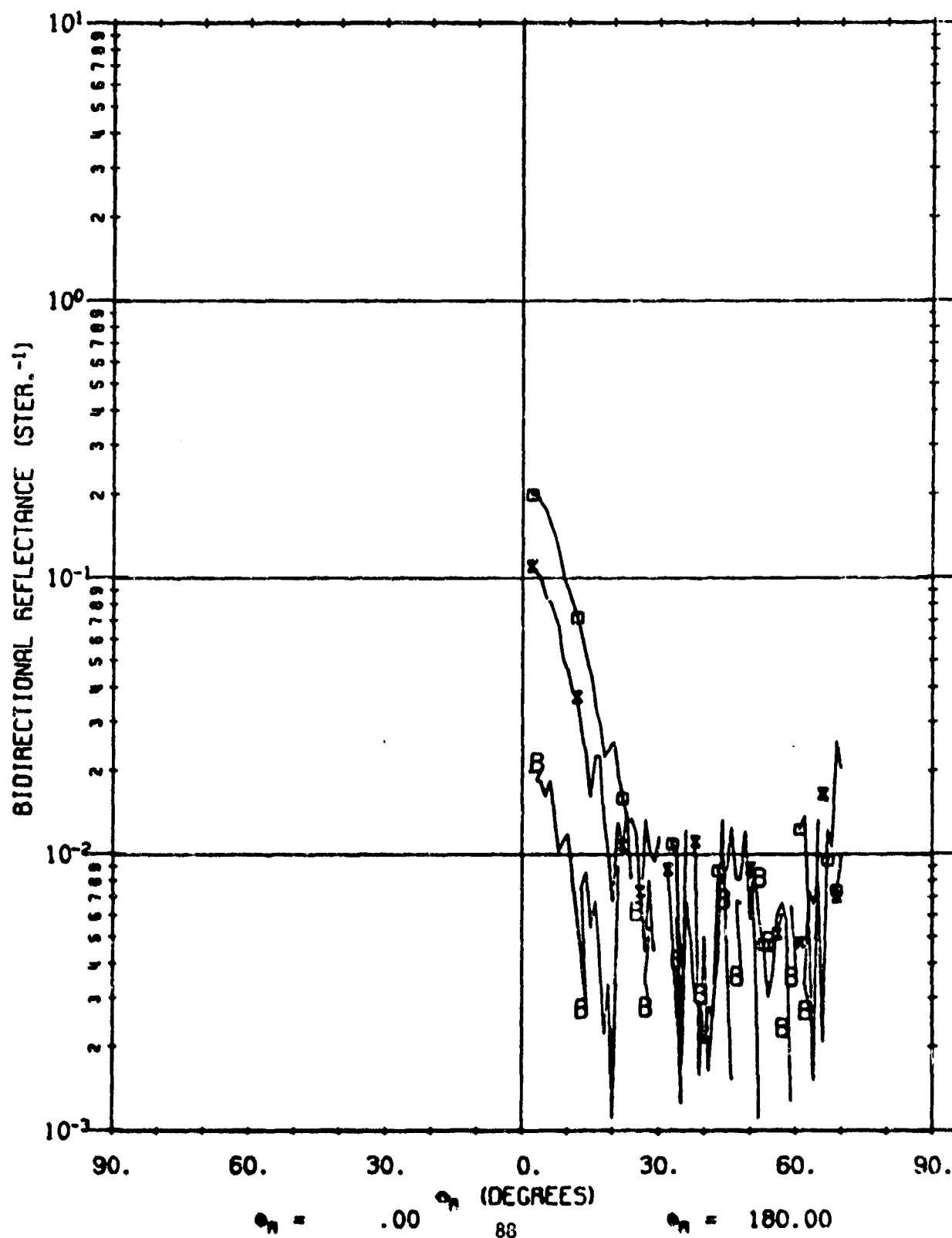
A01610 303

$\lambda = 3.39$   
 $\phi_i = \phi_n = 2.0$   
 $\phi_i = .0$



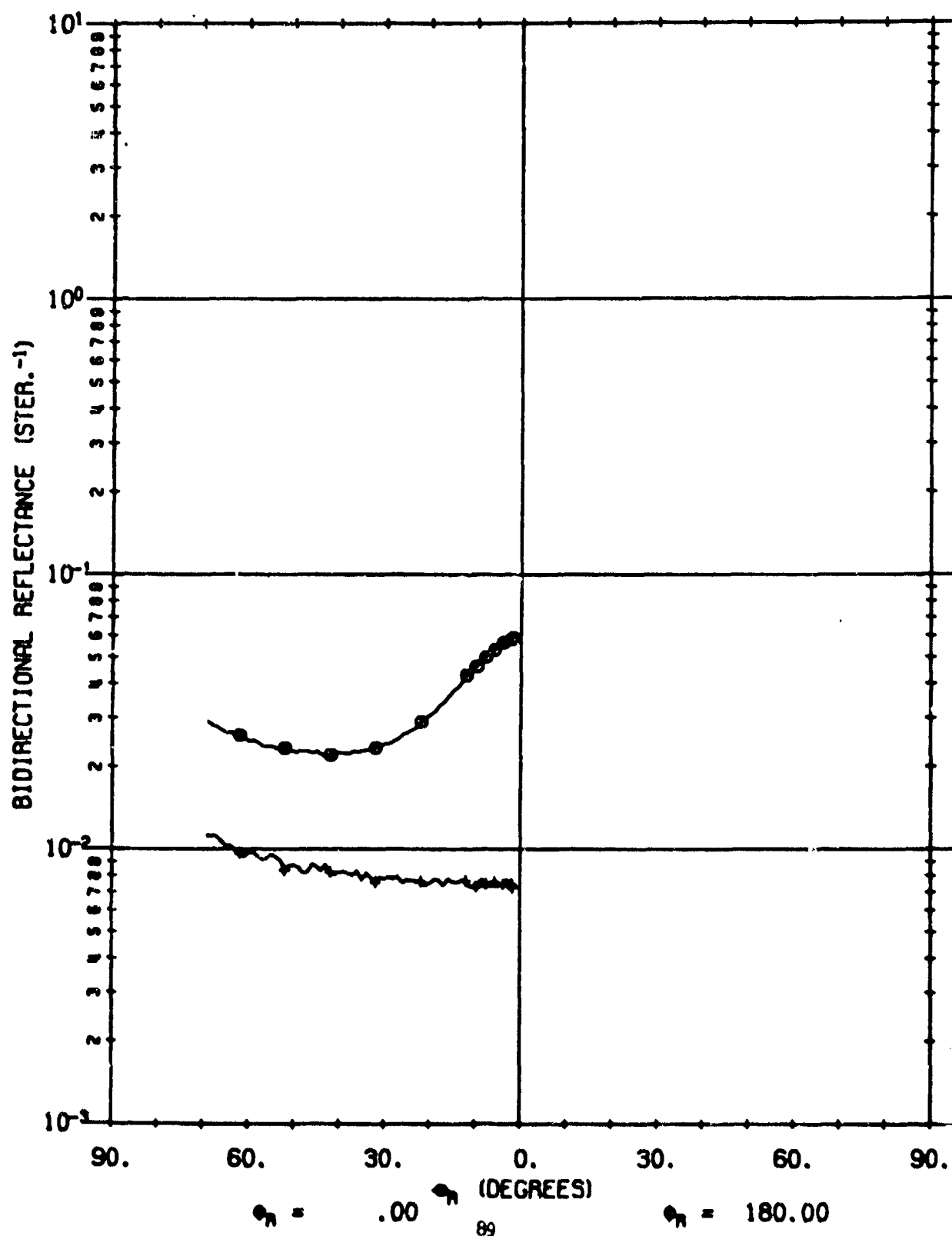
A01610 303

$\lambda = 3.39$   
 $\phi_1 = \phi_2 = -2.0$   
 $\phi_1 = 180.0$



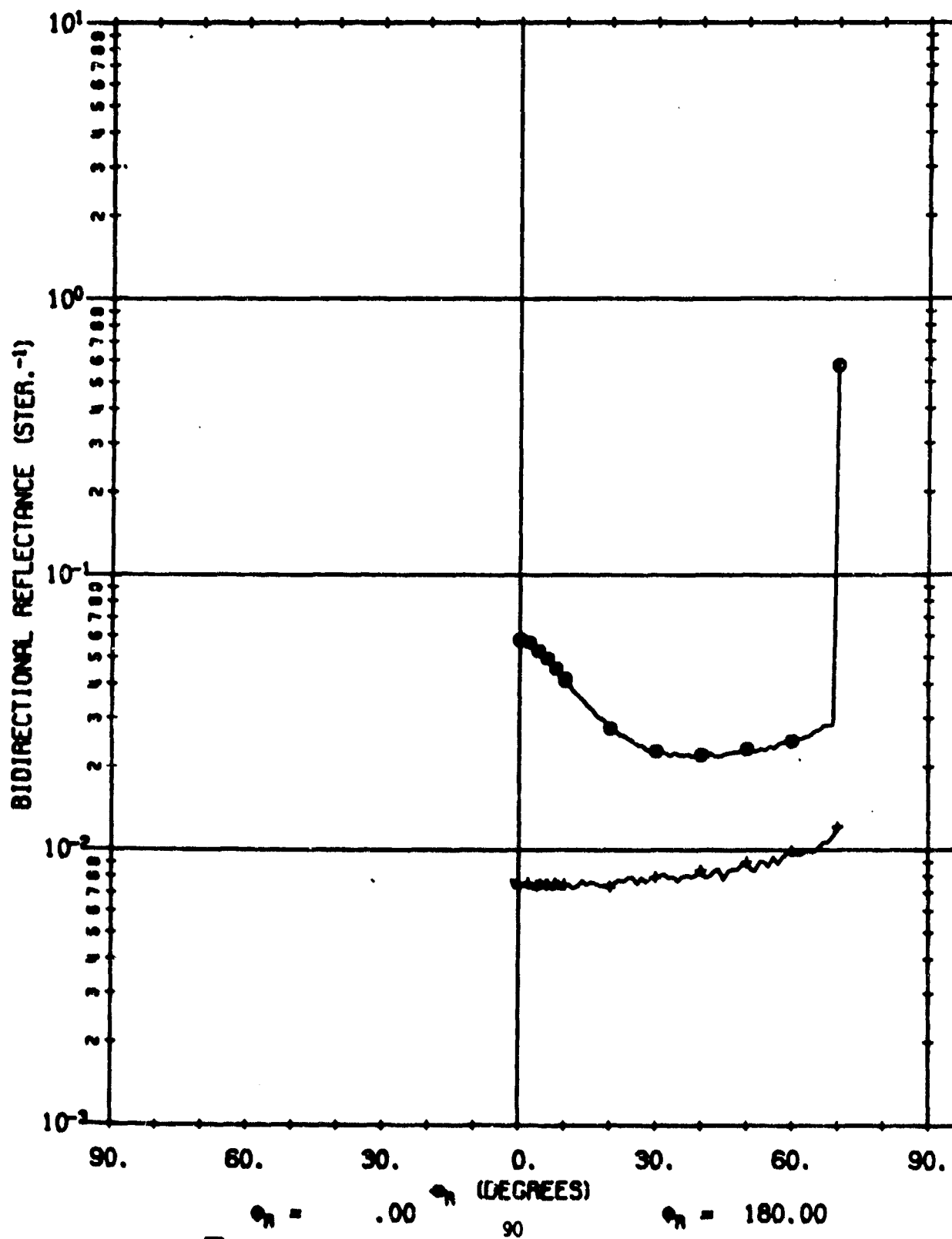
A01610 101

$$\begin{aligned} \lambda &= .63 \\ \phi_1 &= \phi_n + .63 \\ \phi_1 &= \phi_n + .0 \end{aligned}$$



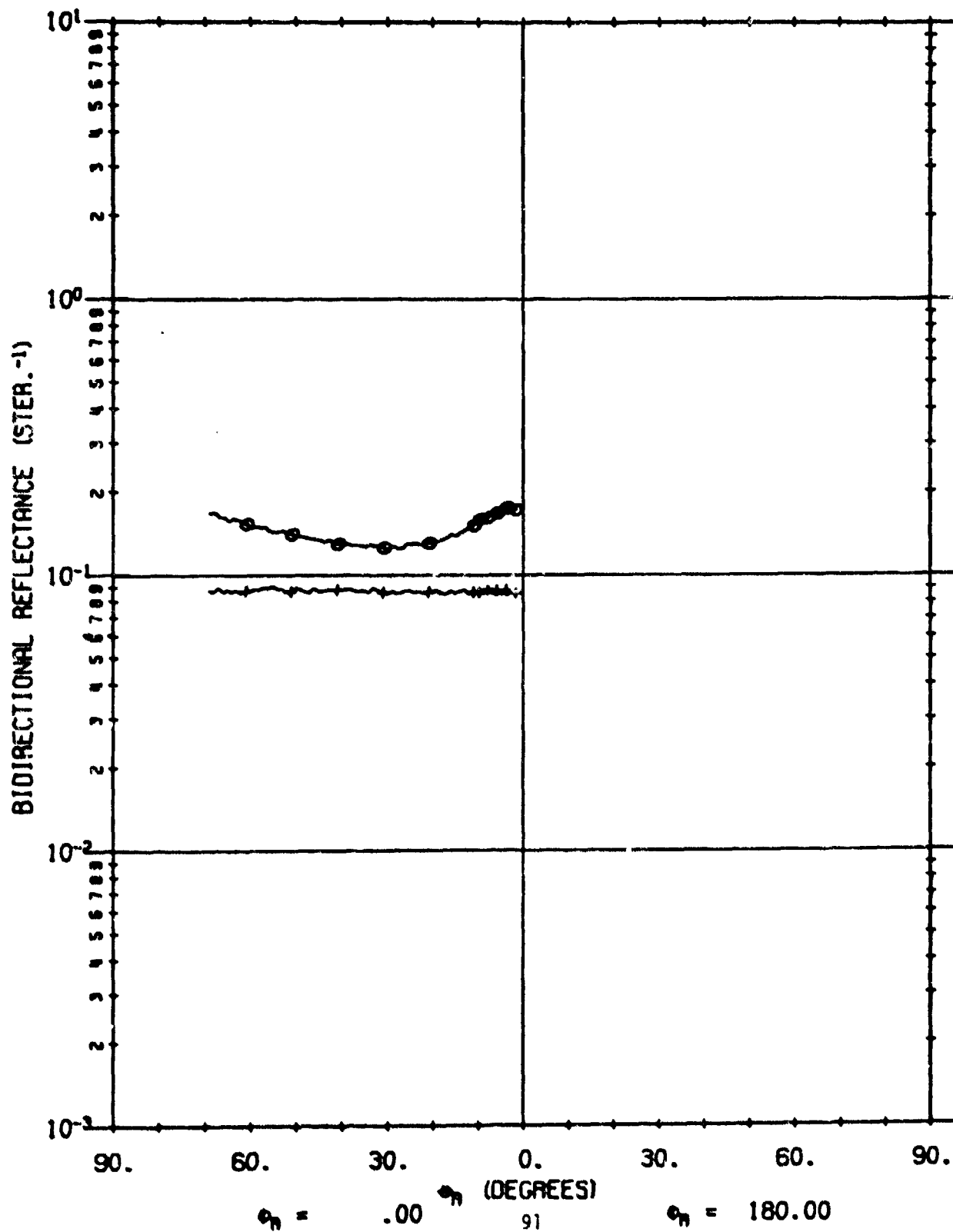
A01610 101

$\lambda = .63$   
 $\phi_1 = \phi_2 + 1.7$   
 $\phi_1 = 180.0$



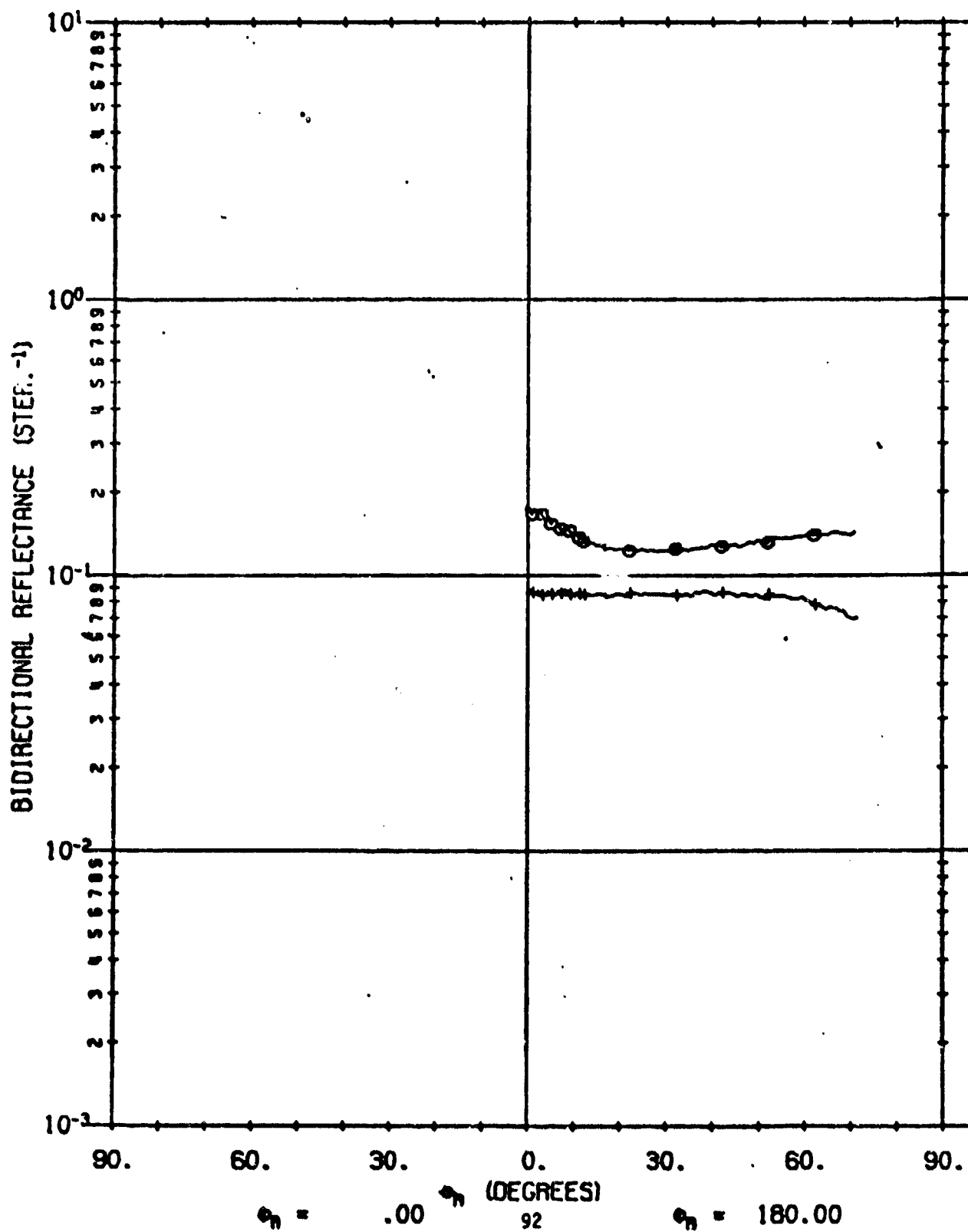
A01610 102

$$\begin{aligned}\lambda &= 1.06 \\ \theta_i &= \theta_r + 1.7 \\ \theta_i &= .0\end{aligned}$$



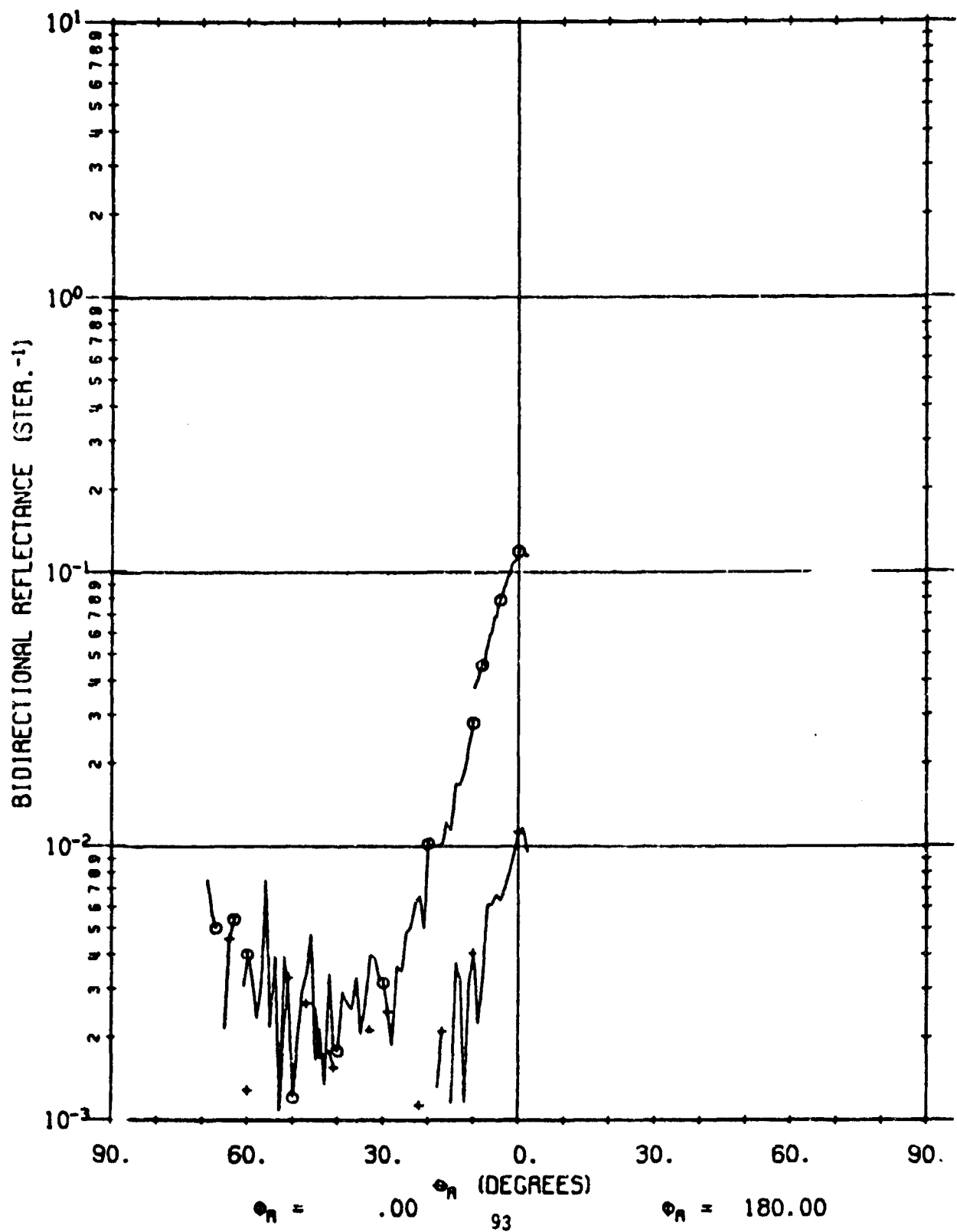
001610 102

$$\begin{aligned}\lambda &= 1.06 \\ \phi_1 &= \phi_n + 1.7 \\ \phi_1 &= .0\end{aligned}$$



A01610 302

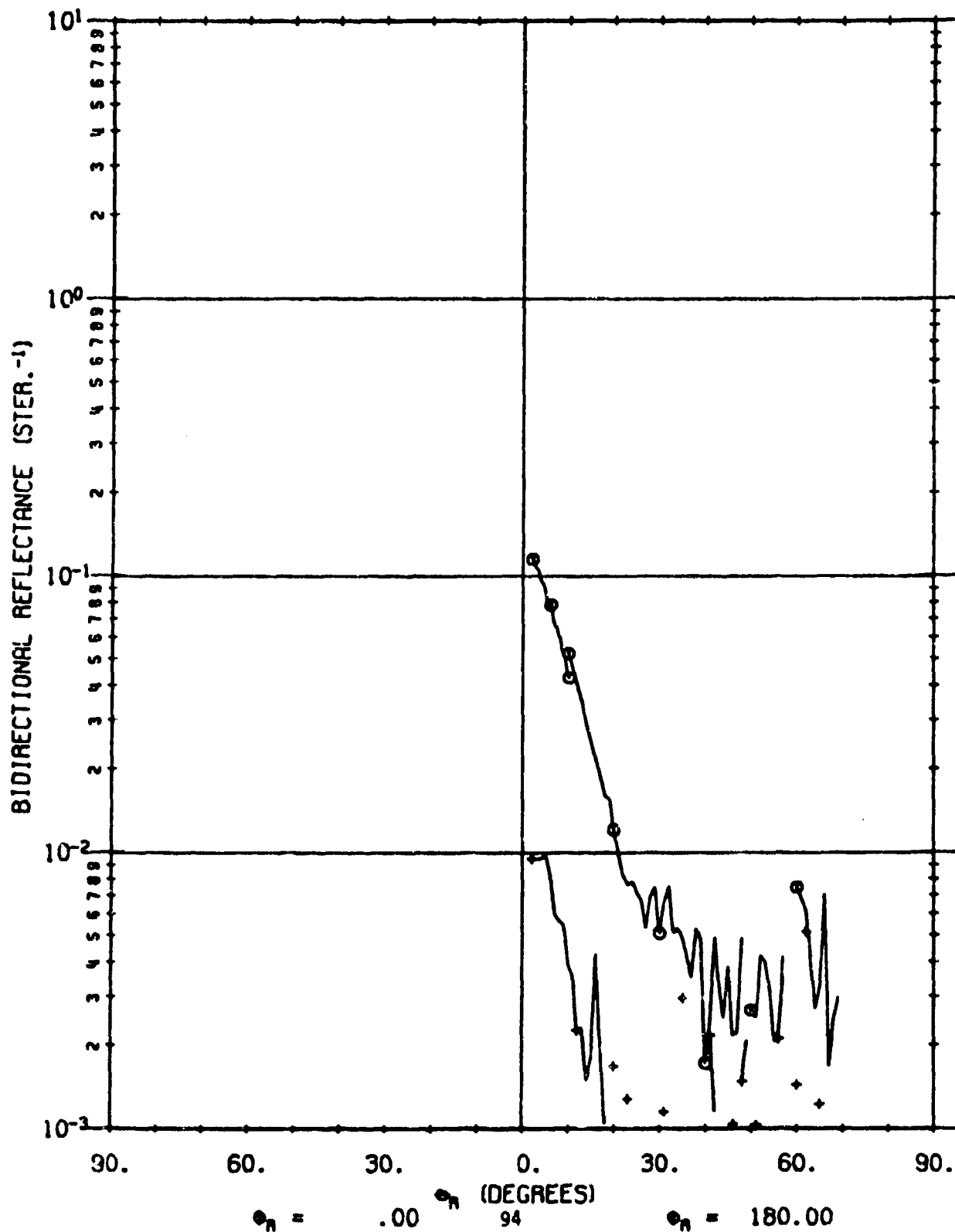
$\lambda = 3.39$   
 $\phi_i = \phi_r^+ 2.0$   
 $\phi_i = .0$





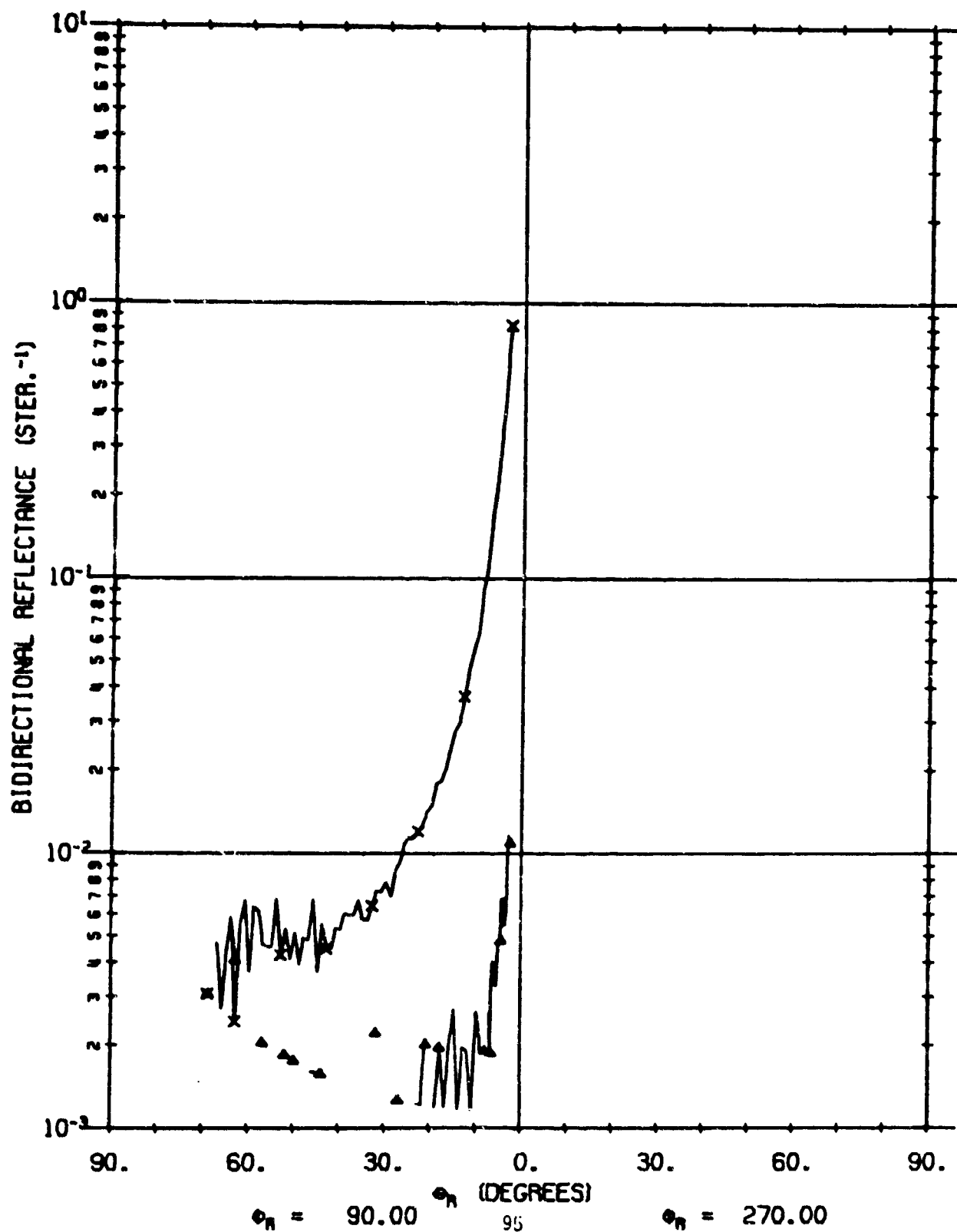
A01610 302

$\lambda = 3.39$   
 $\theta_i = -2.0$   
 $\phi_i = 180.0$



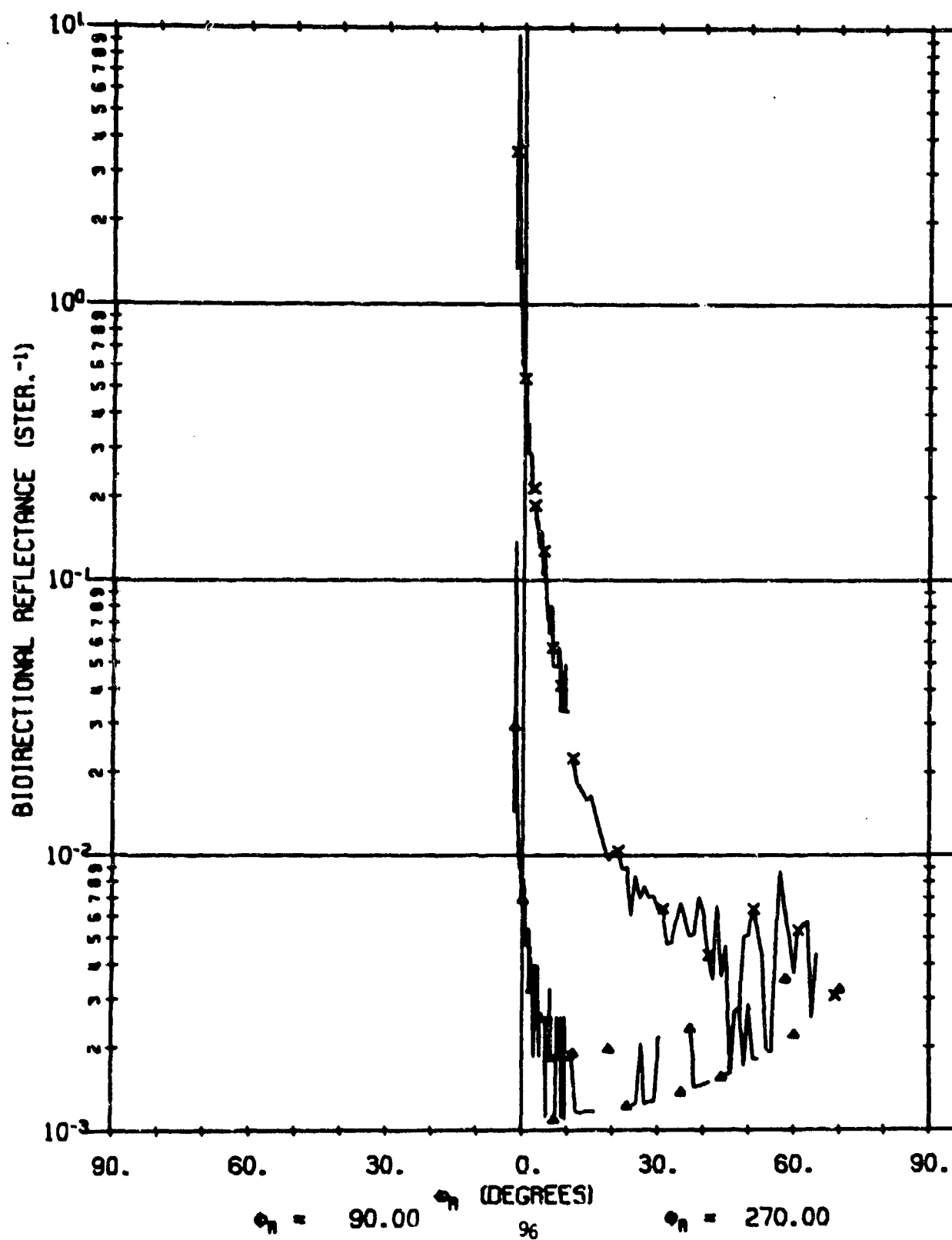
A01610 201

$\lambda = 10.60$   
 $\phi_1 = \phi_2 = -2.5$   
 $\phi_1 = 90.0$



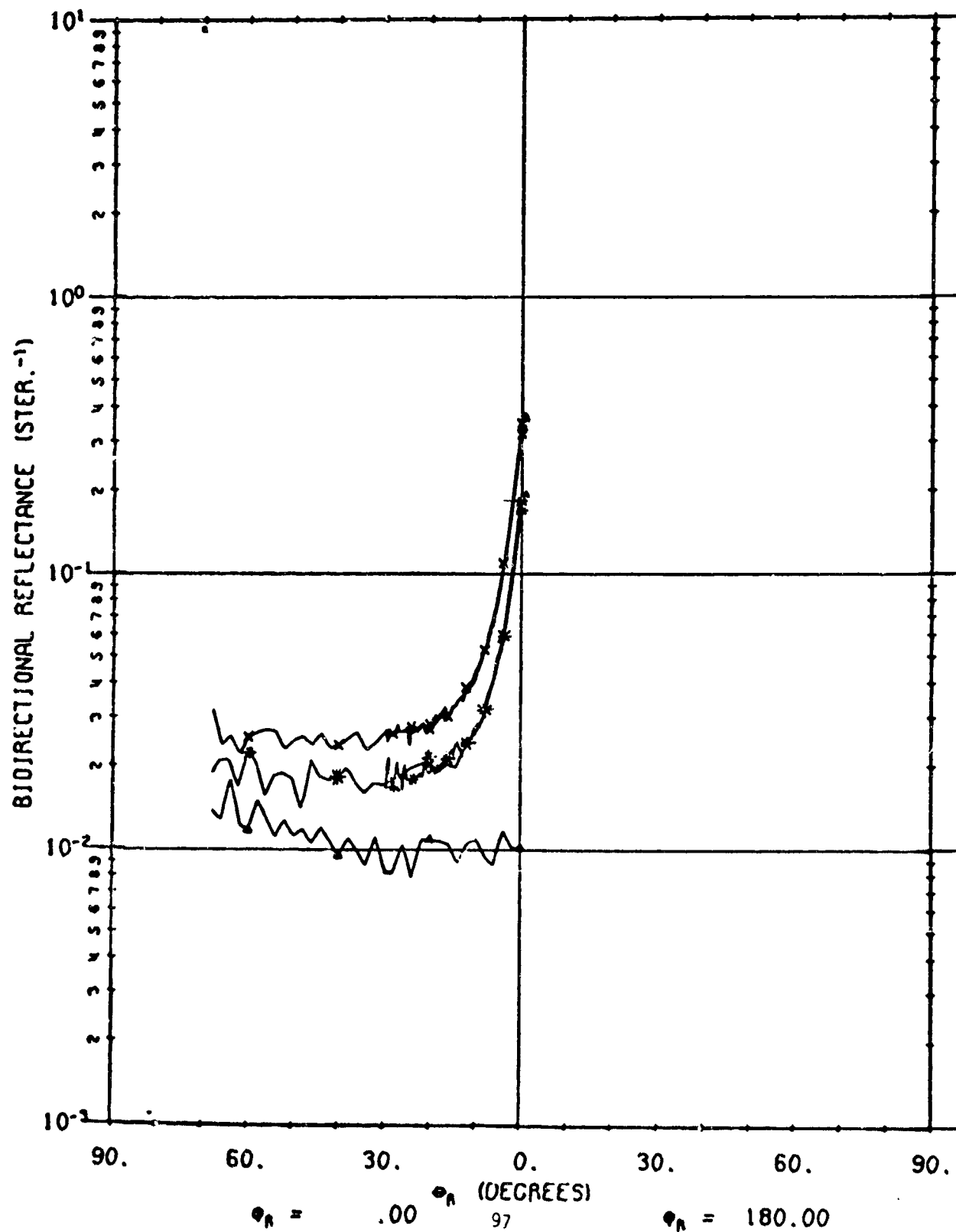
A01610 201

$\lambda = 10.60$   
 $\phi_i = 2.5$   
 $\phi_f = 270.0$



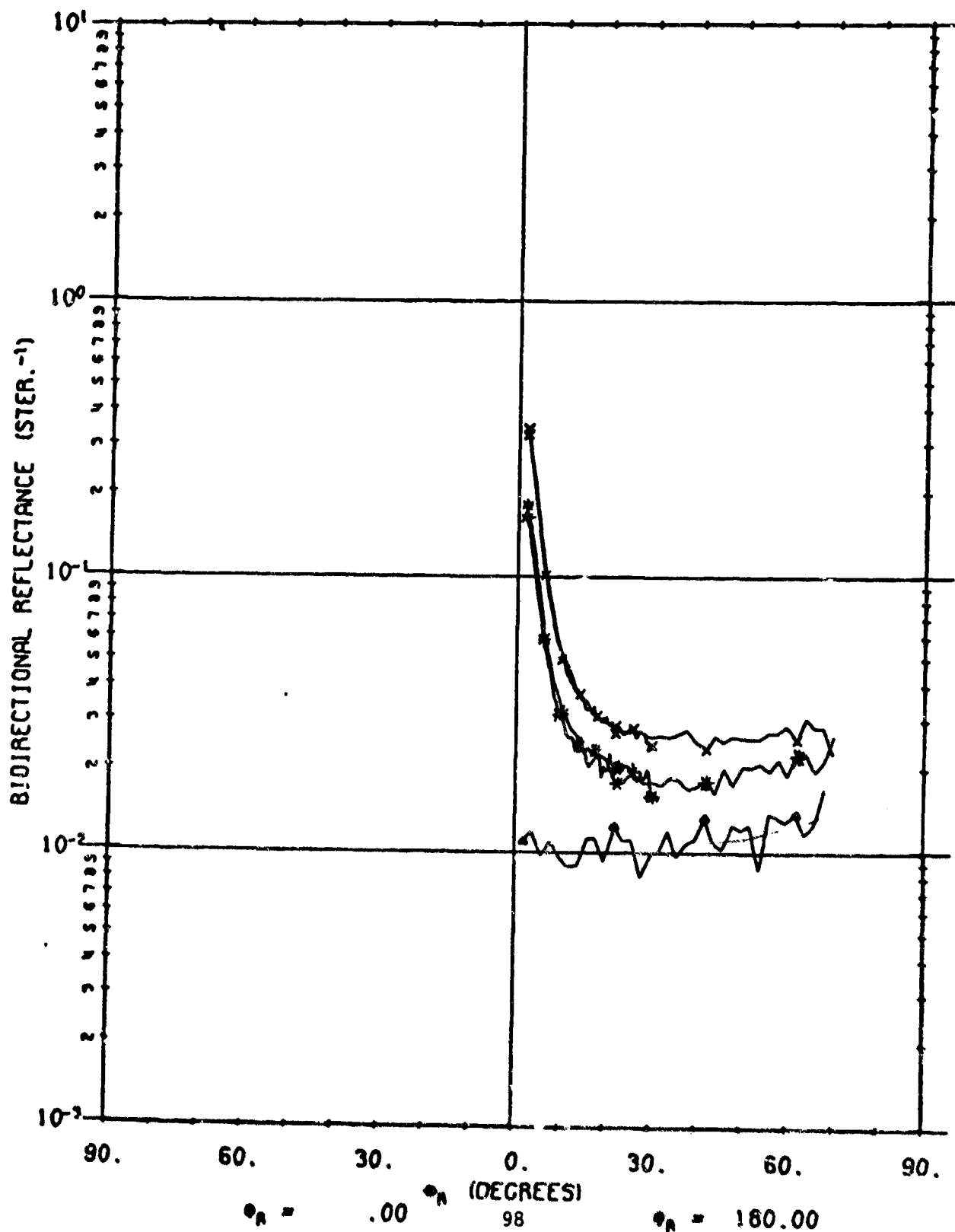
A02022 202

$\lambda = .63$   
 $\theta_i = \theta_r = 1.7$   
 $\phi_i = .0$



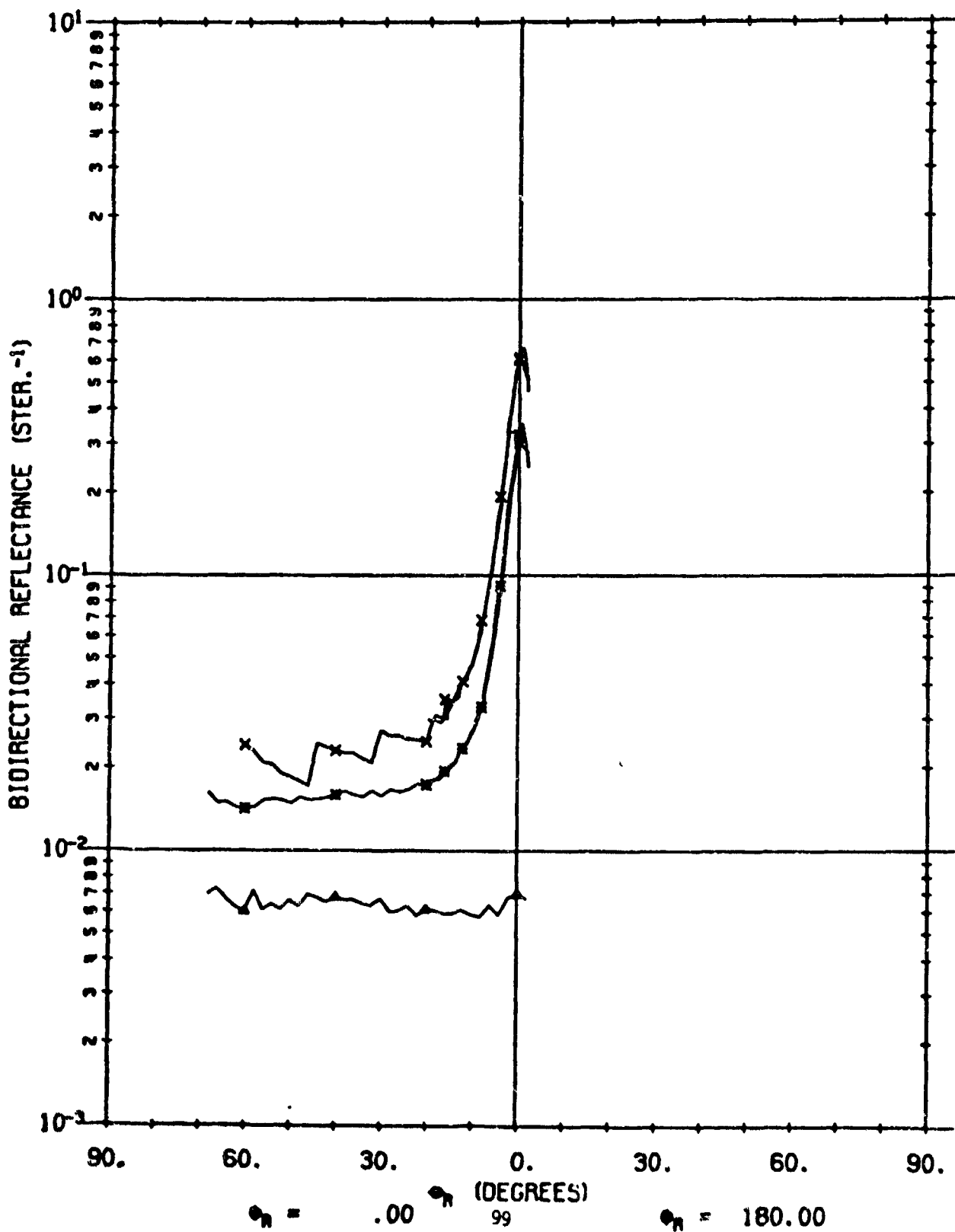
A02022 202

$\lambda = .63$   
 $\phi_1 = \phi_2 = -1.7$   
 $\phi_1 = 180.0$



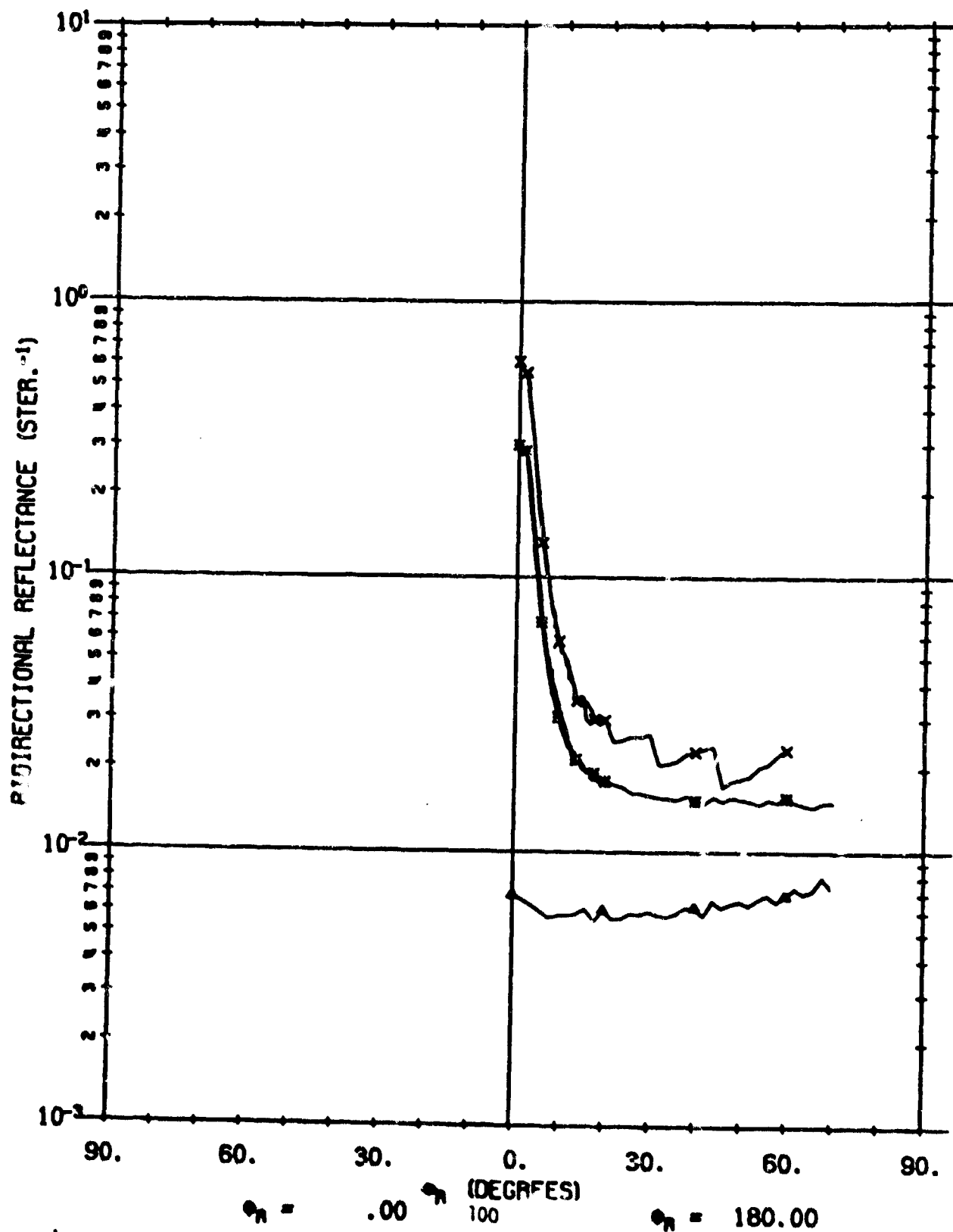
A02022 201

$\lambda = 1.06$   
 $\phi_1 = \phi_n + 1.7$   
 $\phi_1 = .0$

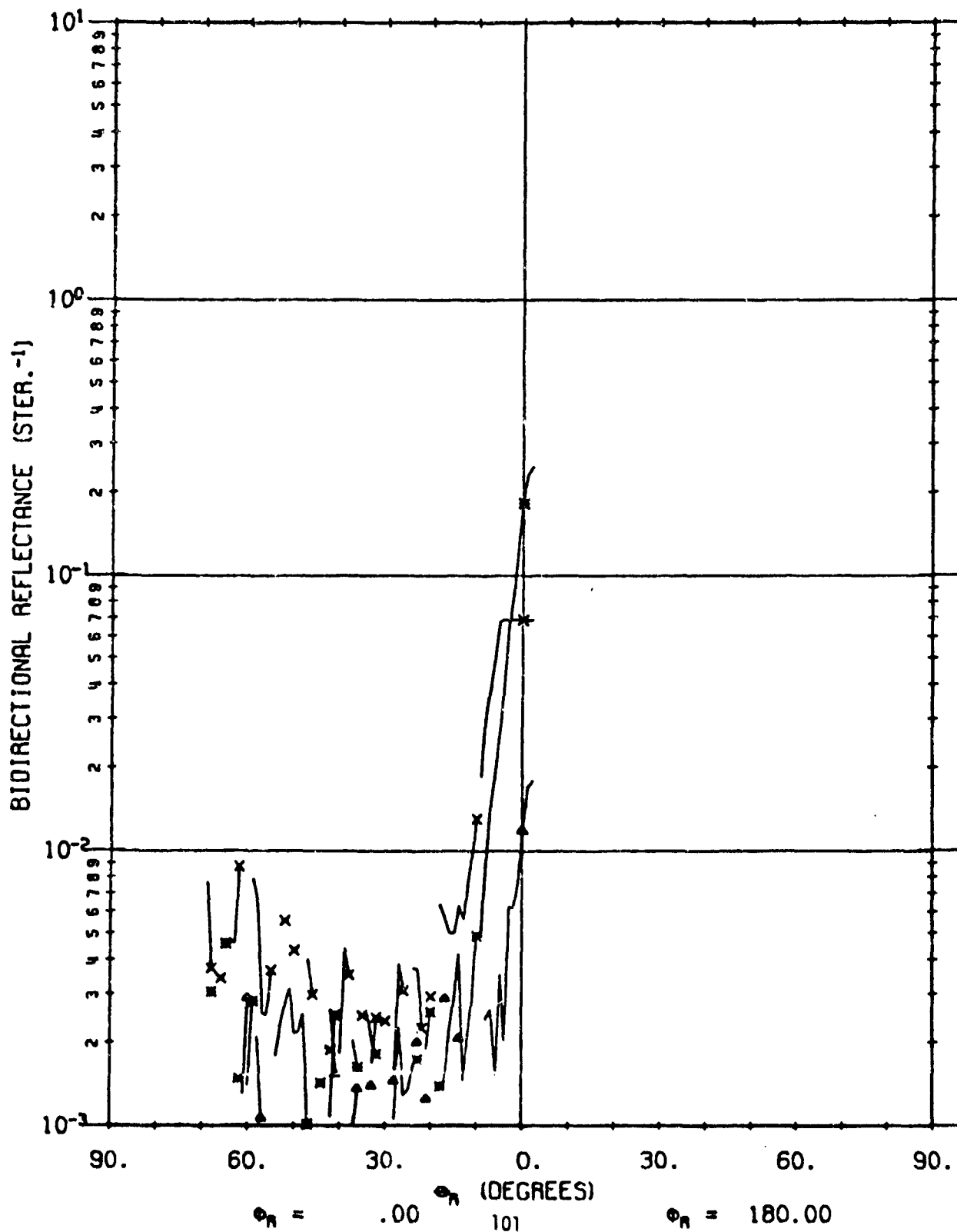


AD2022 201

$\lambda = 1.06$   
 $\phi_1 = -1.0$   
 $\phi_2 = 180.0$



701

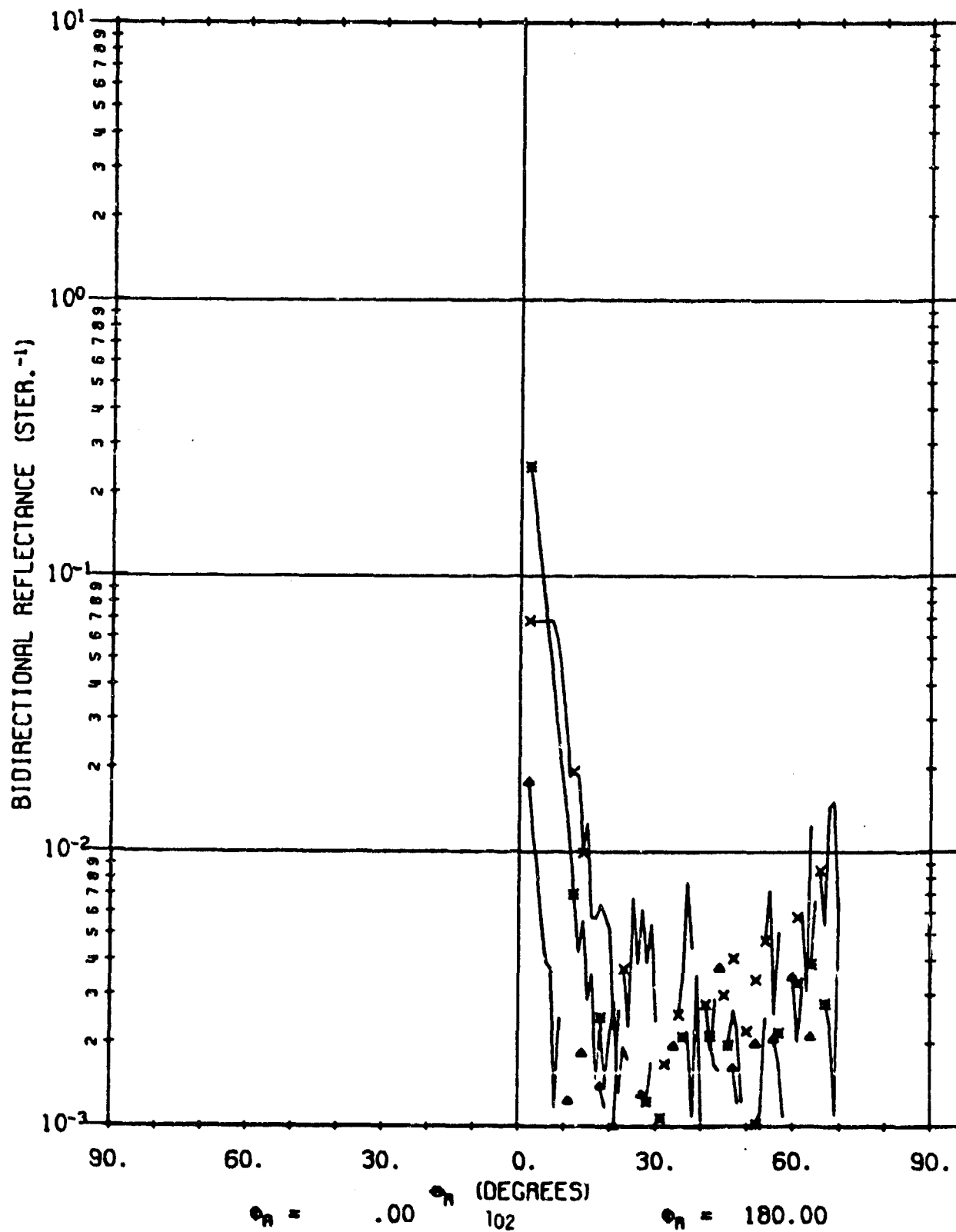
$$\begin{aligned} \lambda &= 3.39 \\ \phi_1 &= \phi_n + 2.0 \\ \phi_1 &= .0 \end{aligned}$$




A02022 701

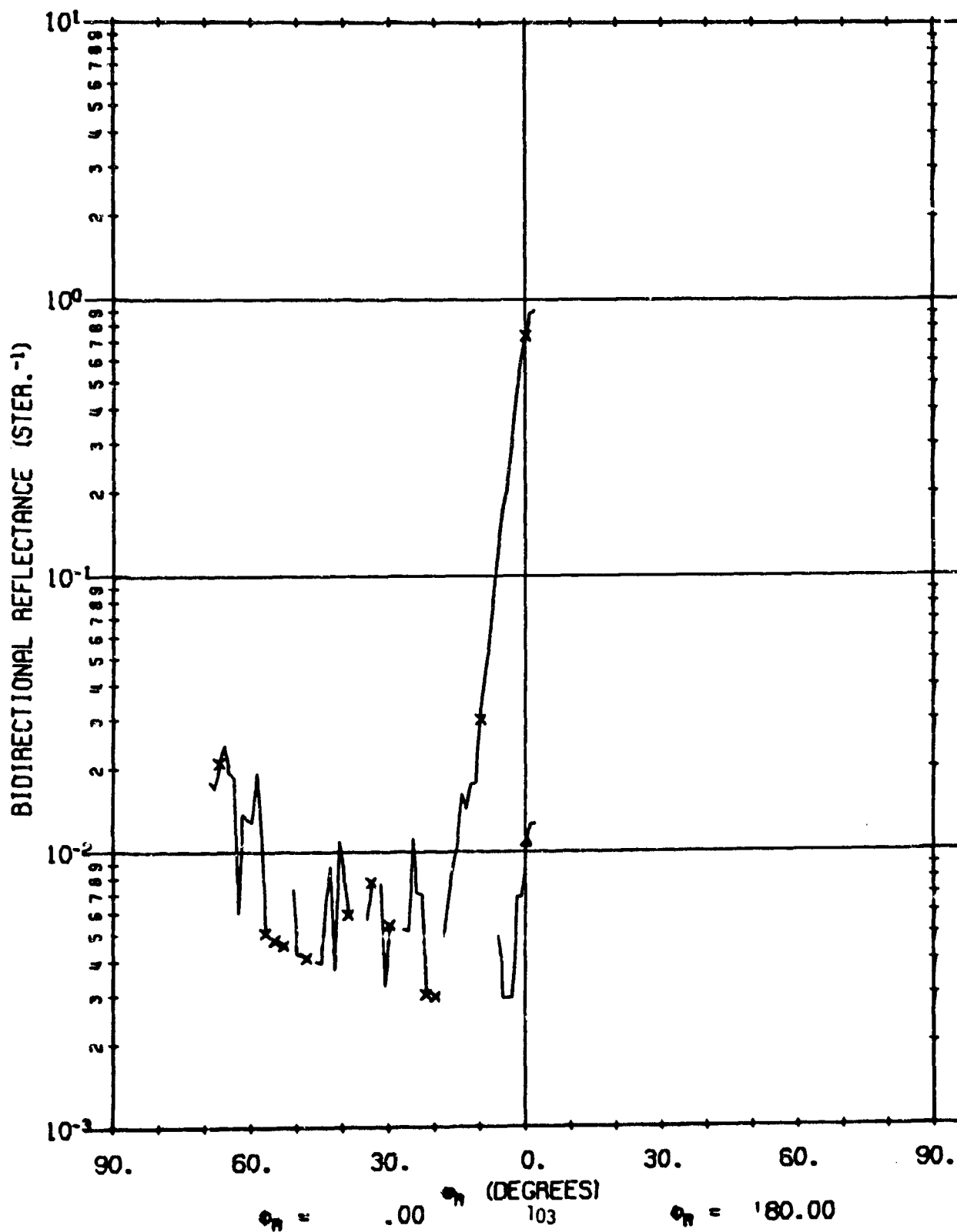
$\lambda = 3.39$   
 $\phi_1 = -2.0$   
 $\phi_2 = 180.0$

83



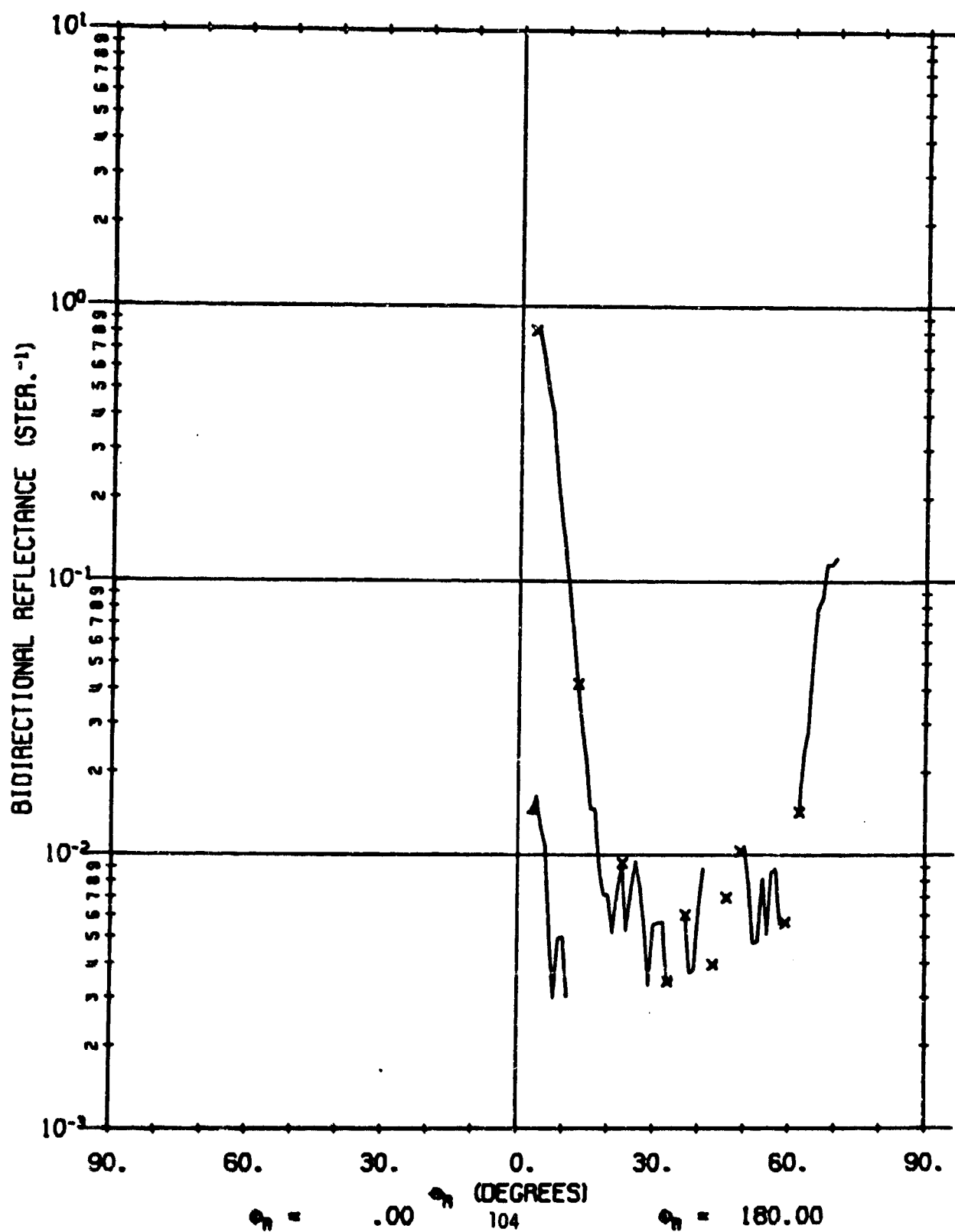
A02022 604

$\lambda = 10.60$   
 $\phi_i = \phi_n + 2.5$   
 $\phi_t = .0$



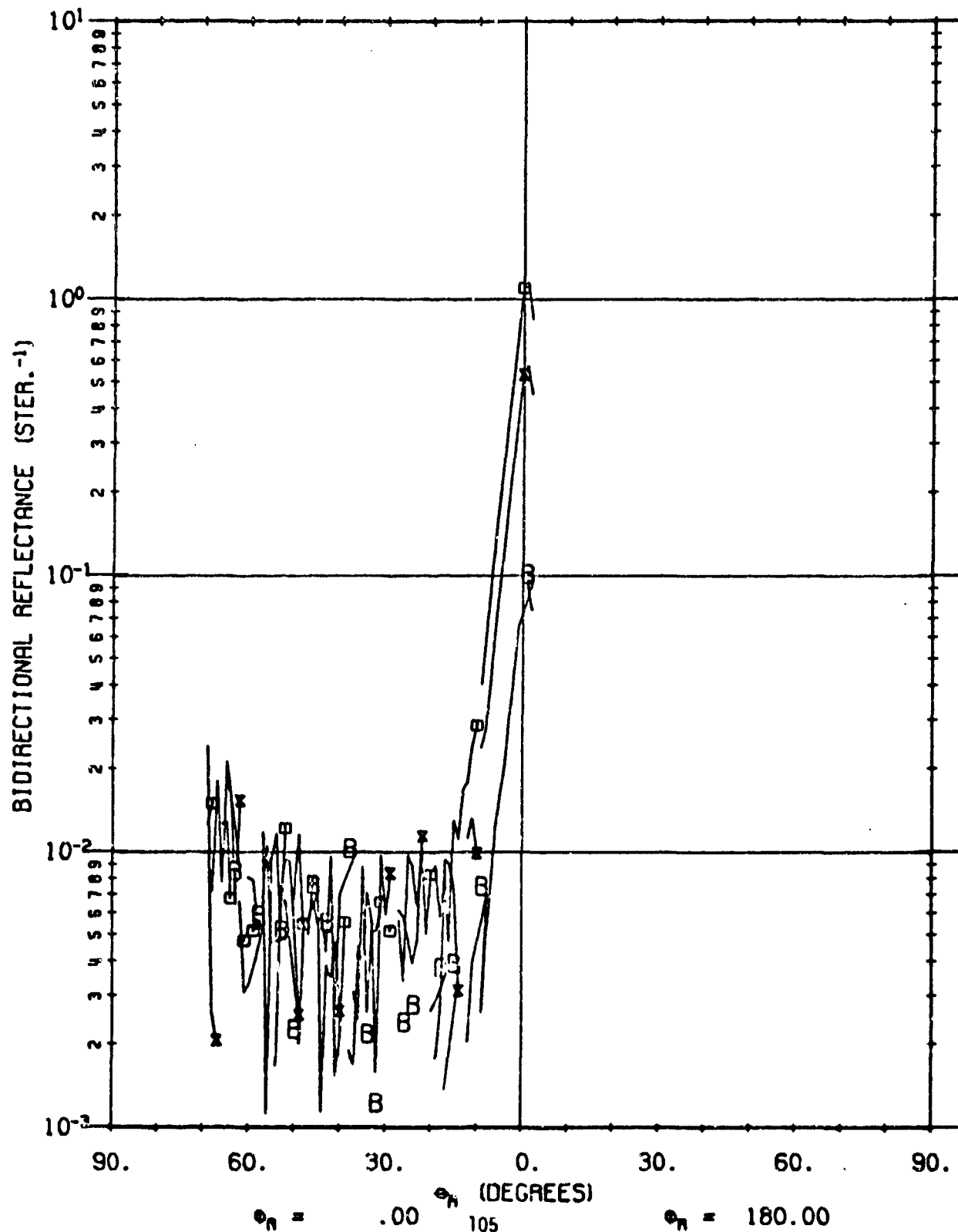
A02022

604

 $\lambda = 10.60$  $\theta_i = \theta_r = -2.5$  $\phi_i = 180.0$ 

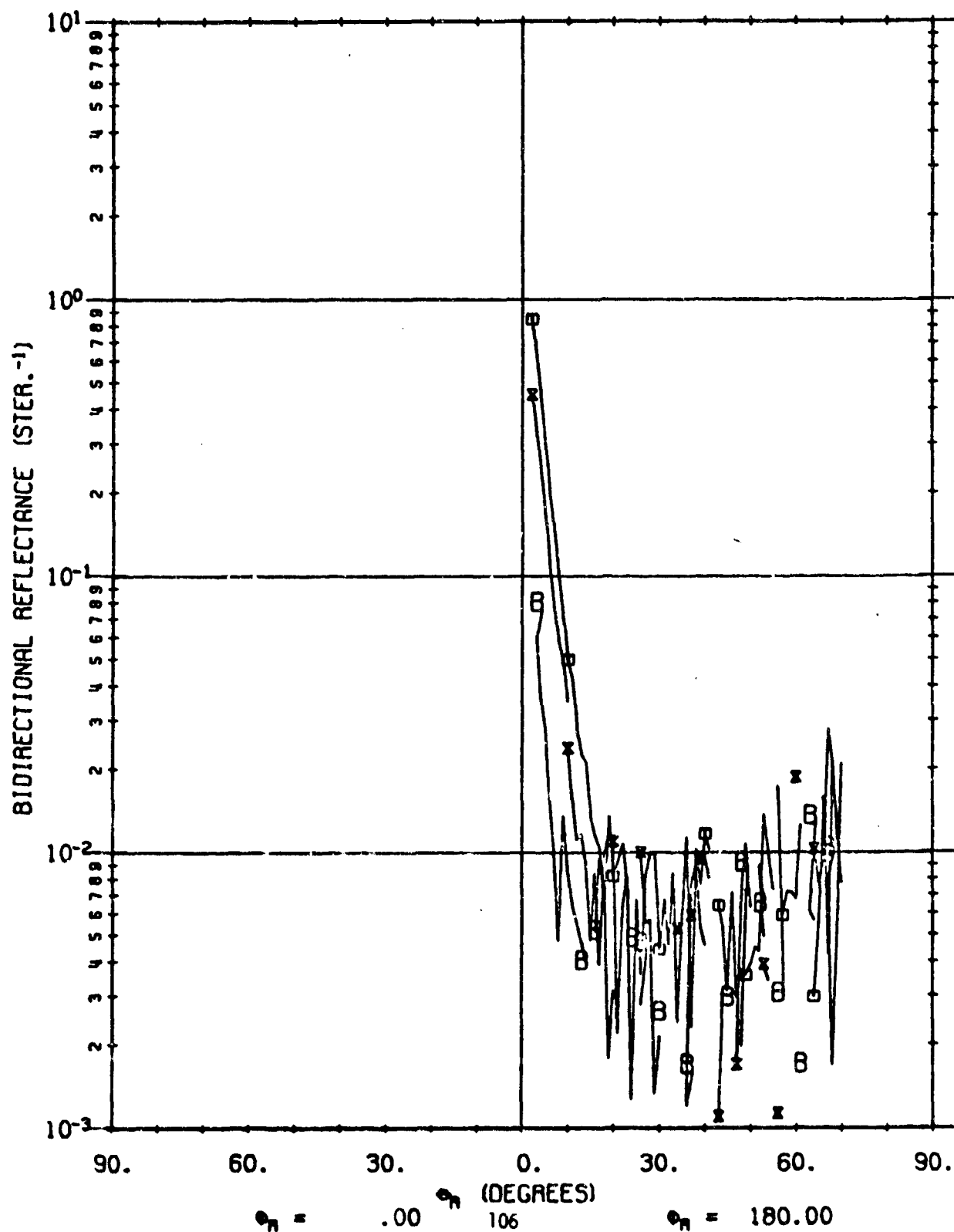
A02022 703

$\lambda = 3.39$   
 $\phi_1 = \phi_n + 2.0$   
 $\phi_1 = .0$



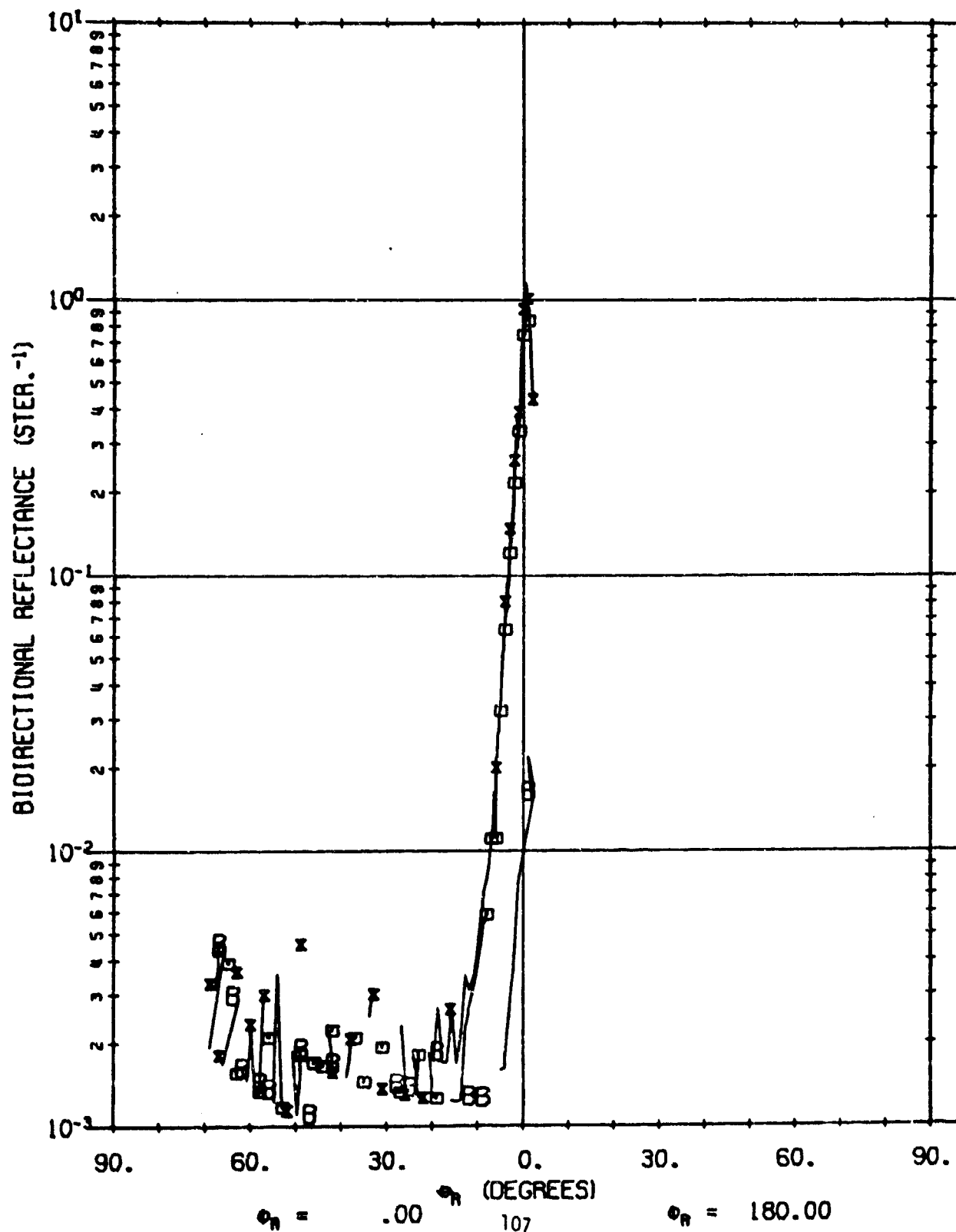
A02022 703

$\lambda = 3.39$   
 $\phi_1 = -2.0$   
 $\phi_1 = 180.0$



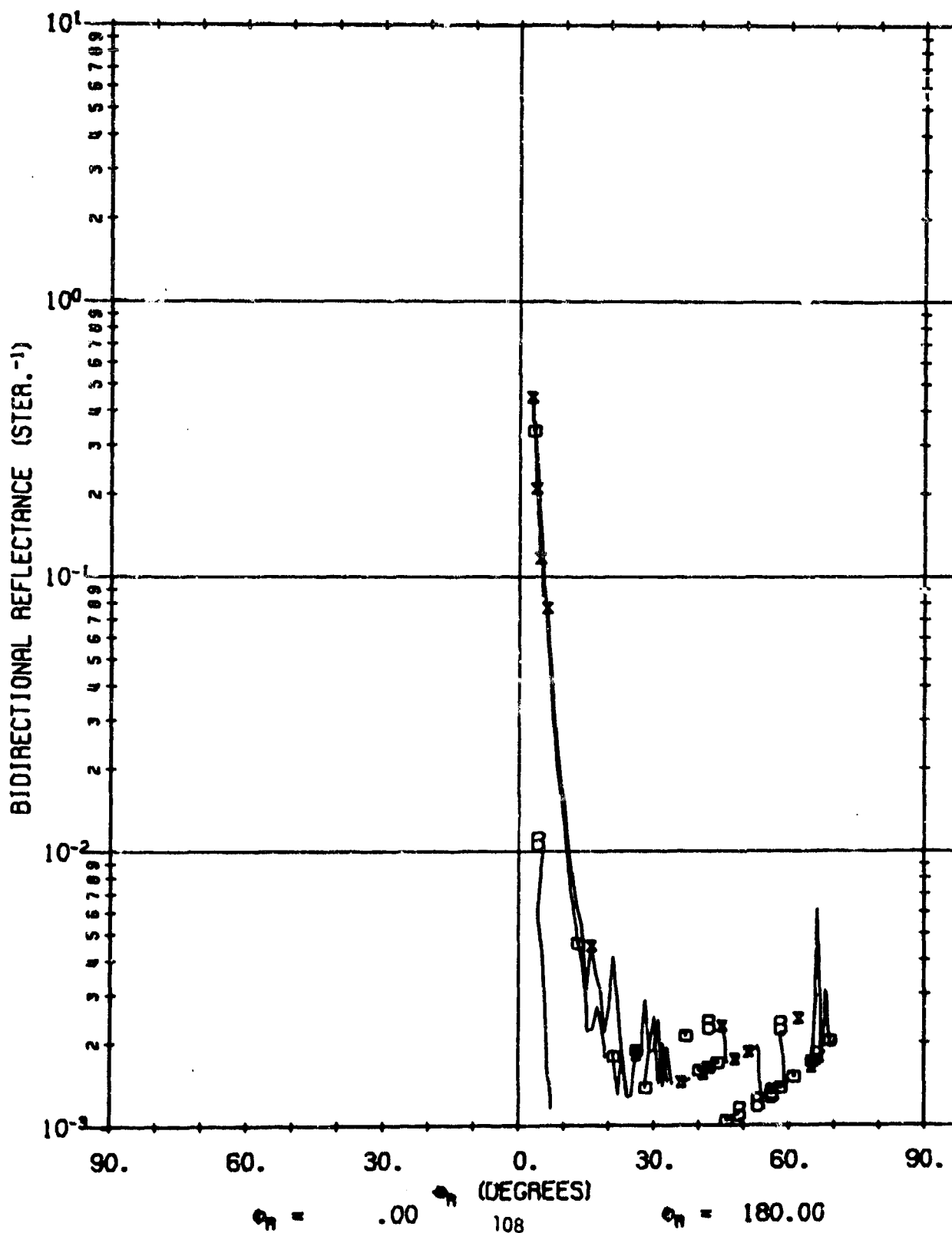
A02022 603

$\lambda = 10.60$   
 $\phi_i = \phi_n + 2.5$   
 $\phi_i = .0$



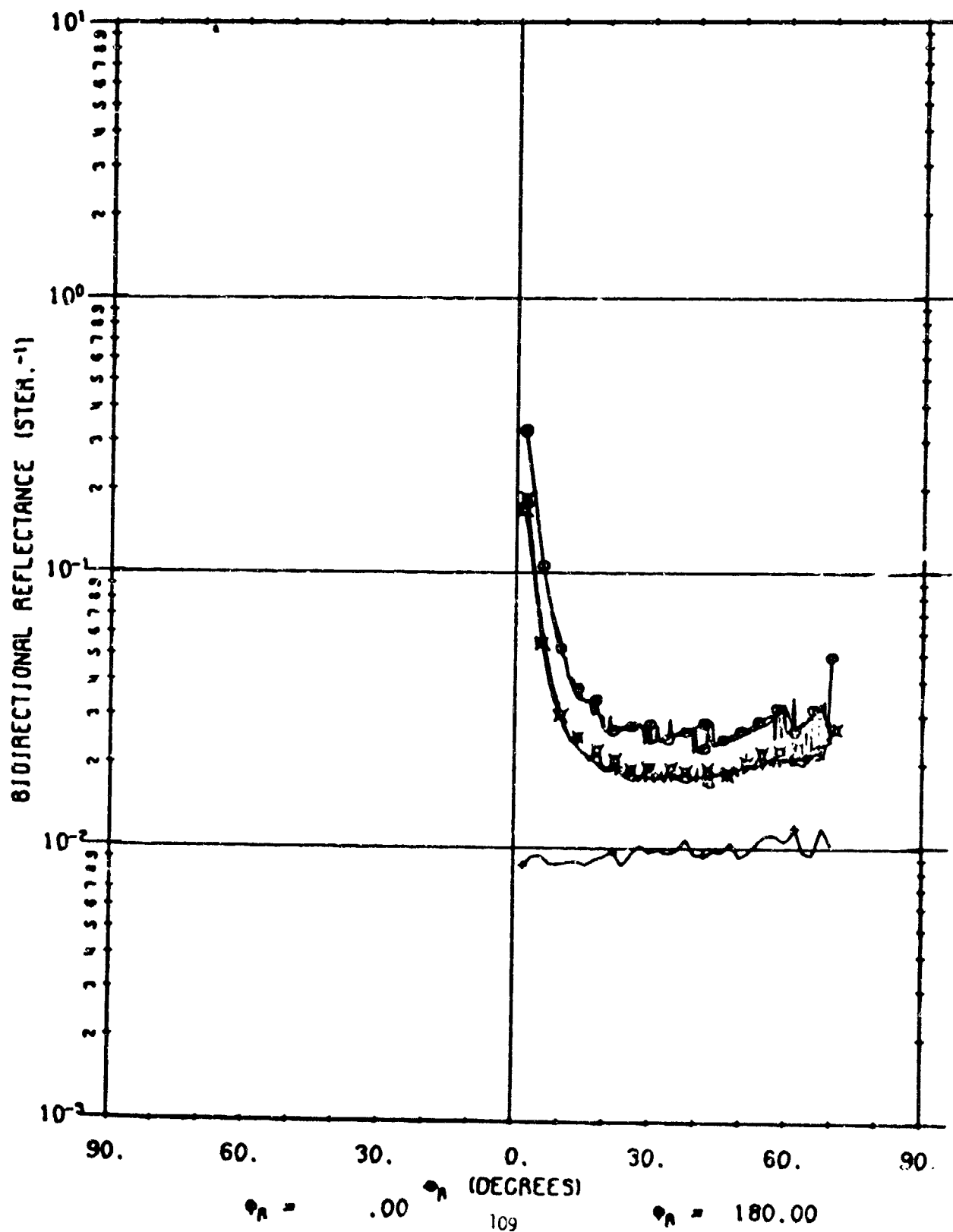
002022 603

$\lambda = 10.60$   
 $\phi_i = \phi_r = -2.5$   
 $\phi_t = 180.0$



A02022 202

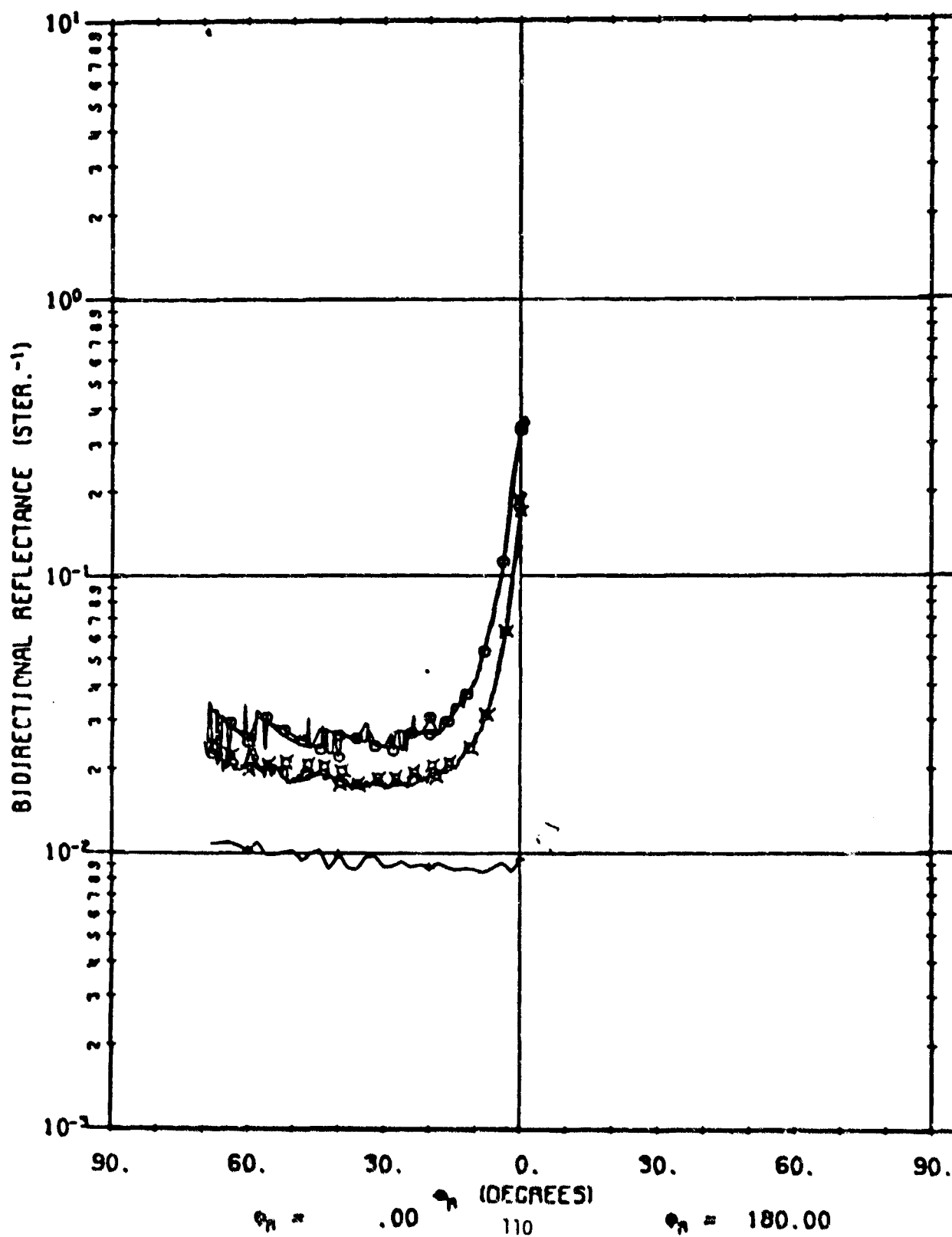
$\lambda = .63$   
 $\phi_1 = -1.7$   
 $\phi_2 = 180.0$





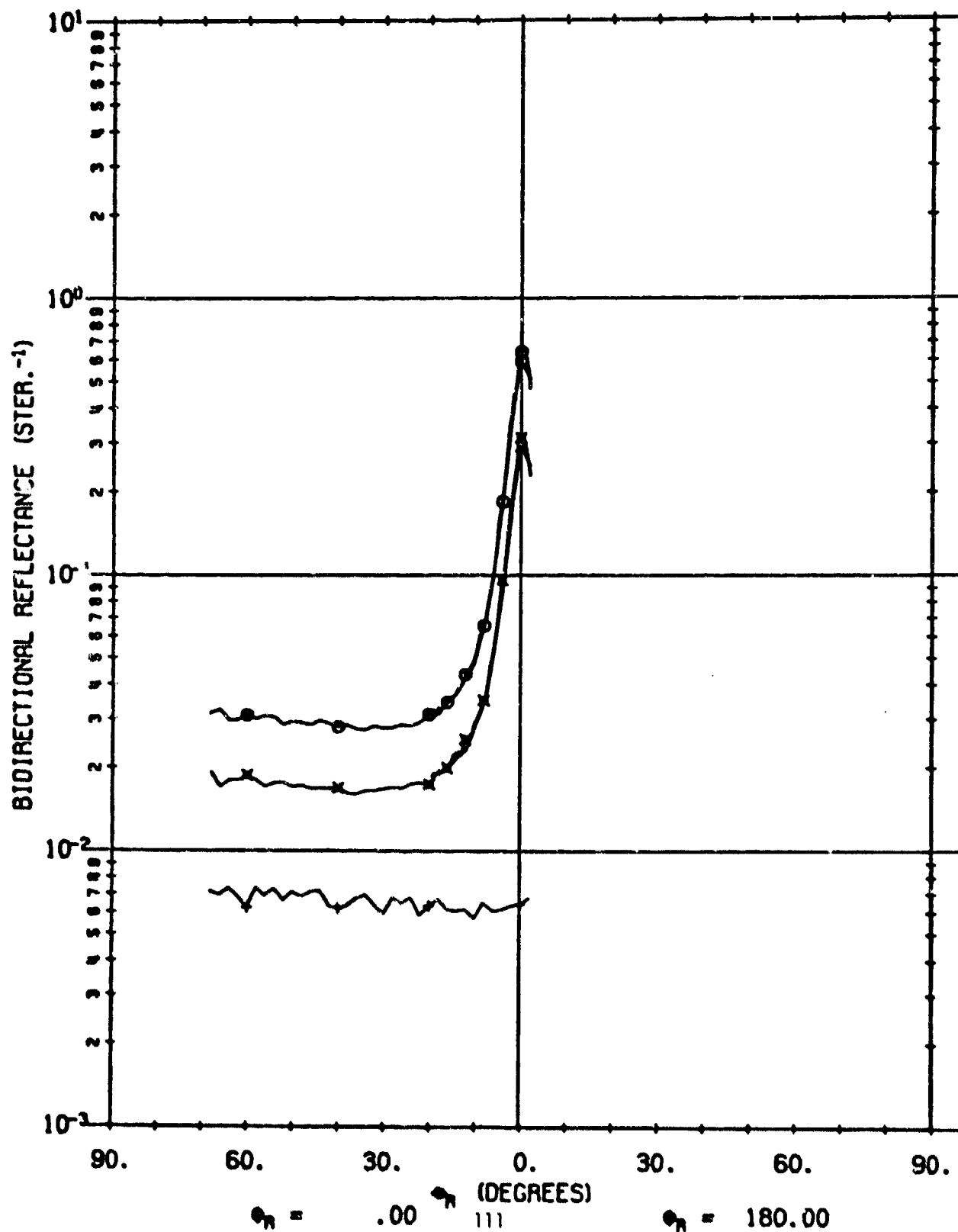
A02022 202

$\lambda = .63$   
 $\theta_i = \theta_r = 1.7$   
 $\phi_i = .0$



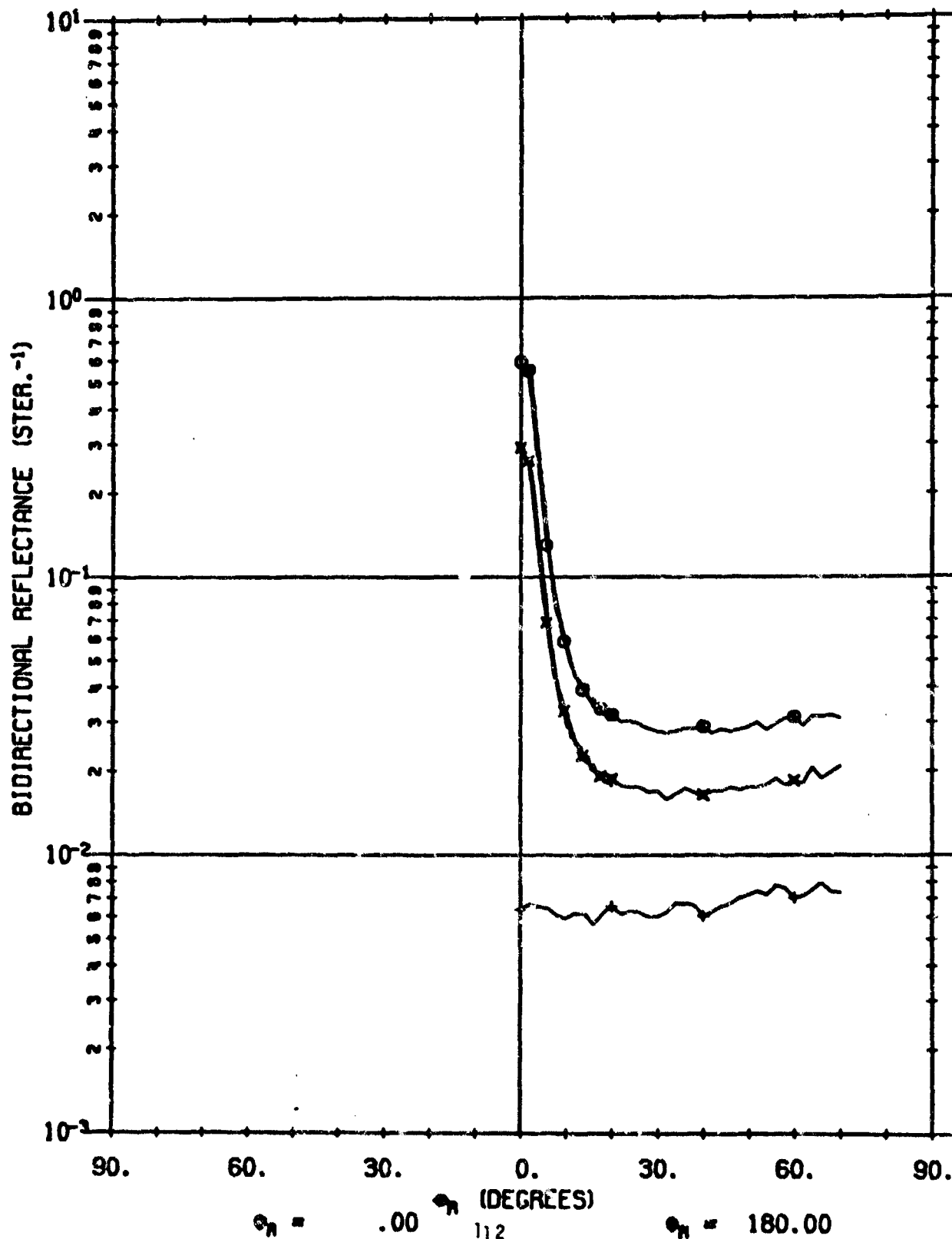
A02022 201

$\lambda = 1.06$   
 $n_1 = n_2 = 1.7$   
 $d = .0$



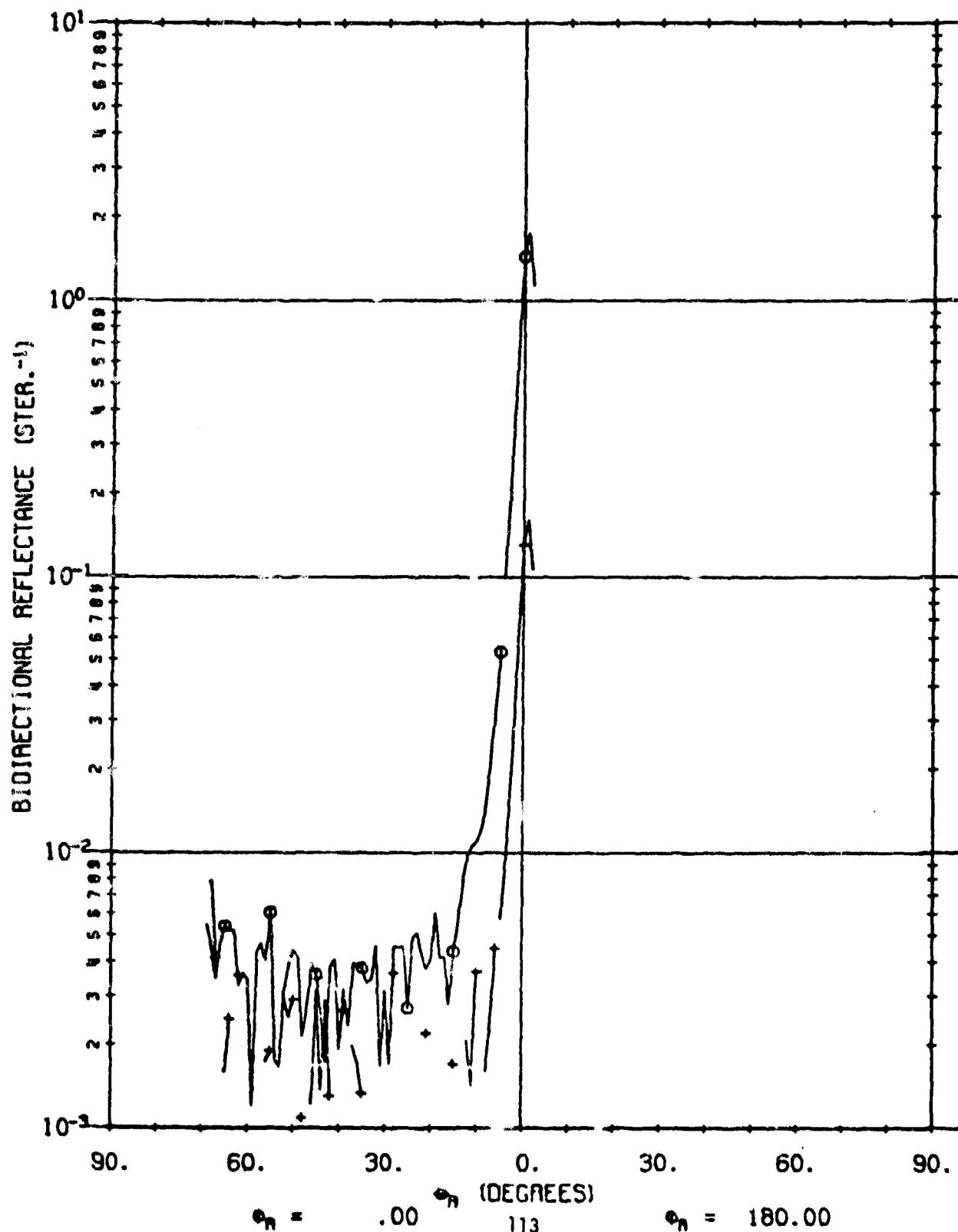
A02022 201

$\lambda = 1.06$   
 $\theta_i = \theta_r = -1.0$   
 $\phi_i = 180.0$



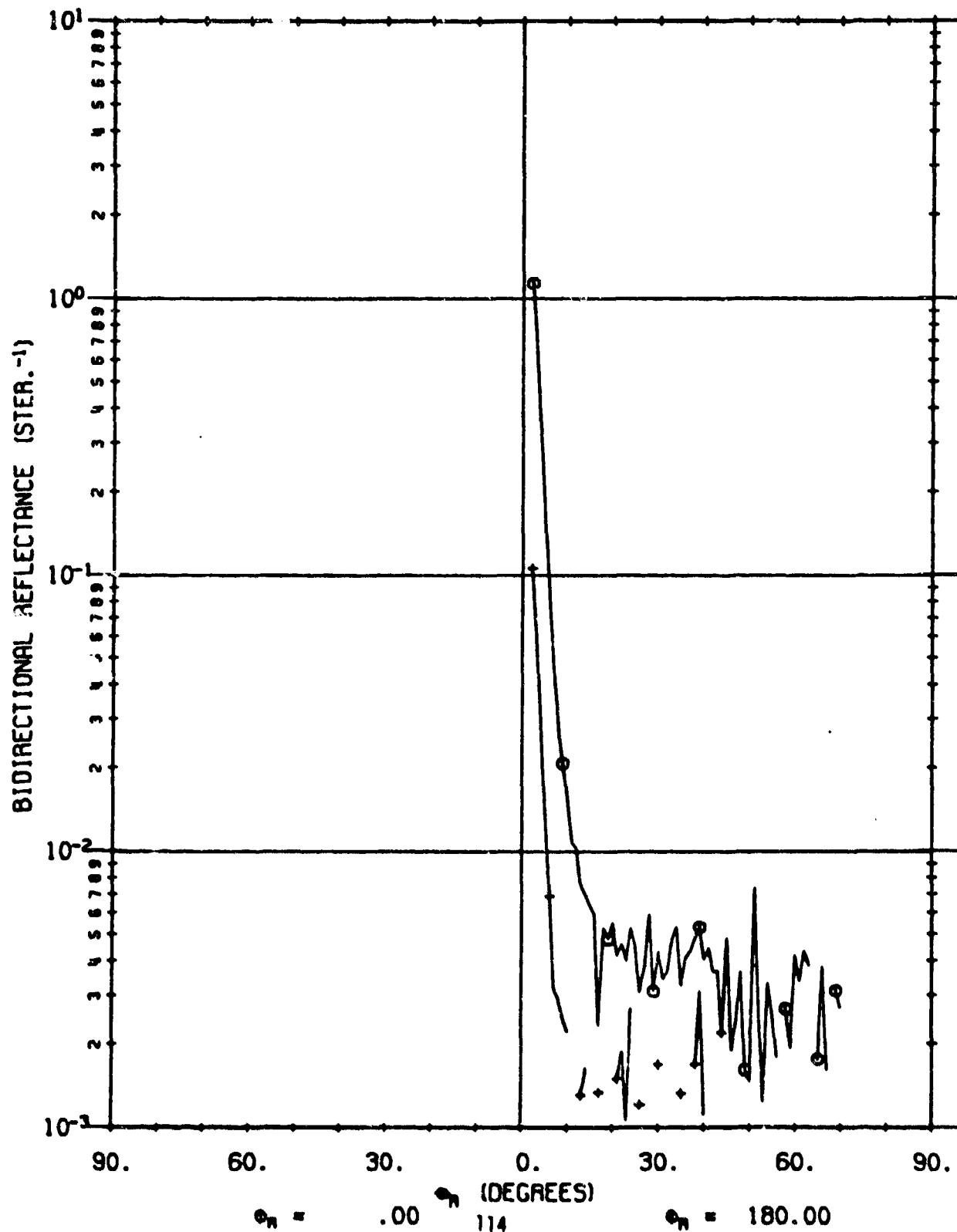
A02022 702

$\lambda = 3.39$   
 $\phi_i = \phi_n + 2.0$   
 $\phi_i = .0$



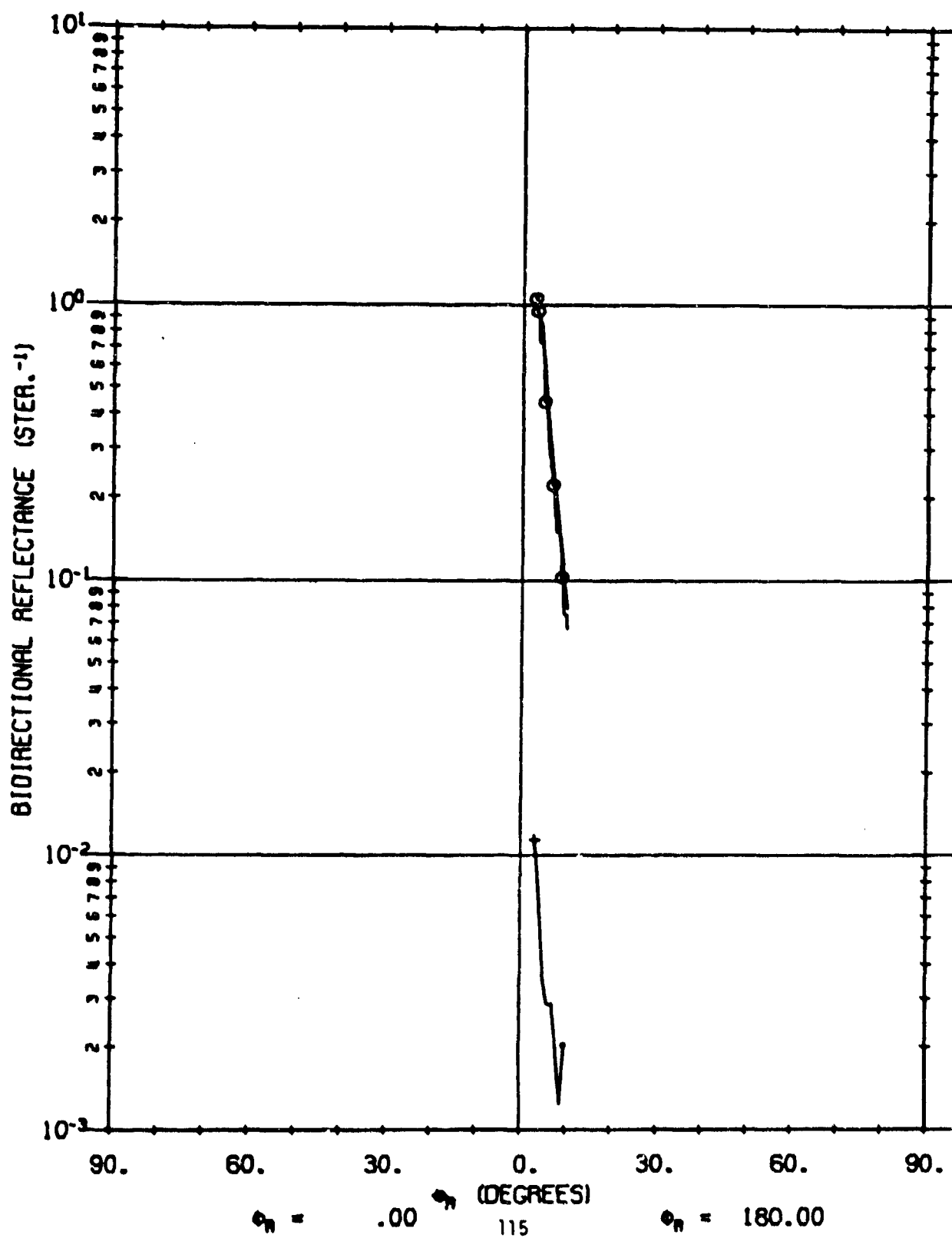
002022 702

$\lambda = 3.39$   
 $\theta_1 = -2.0$   
 $\phi_1 = 180.0$



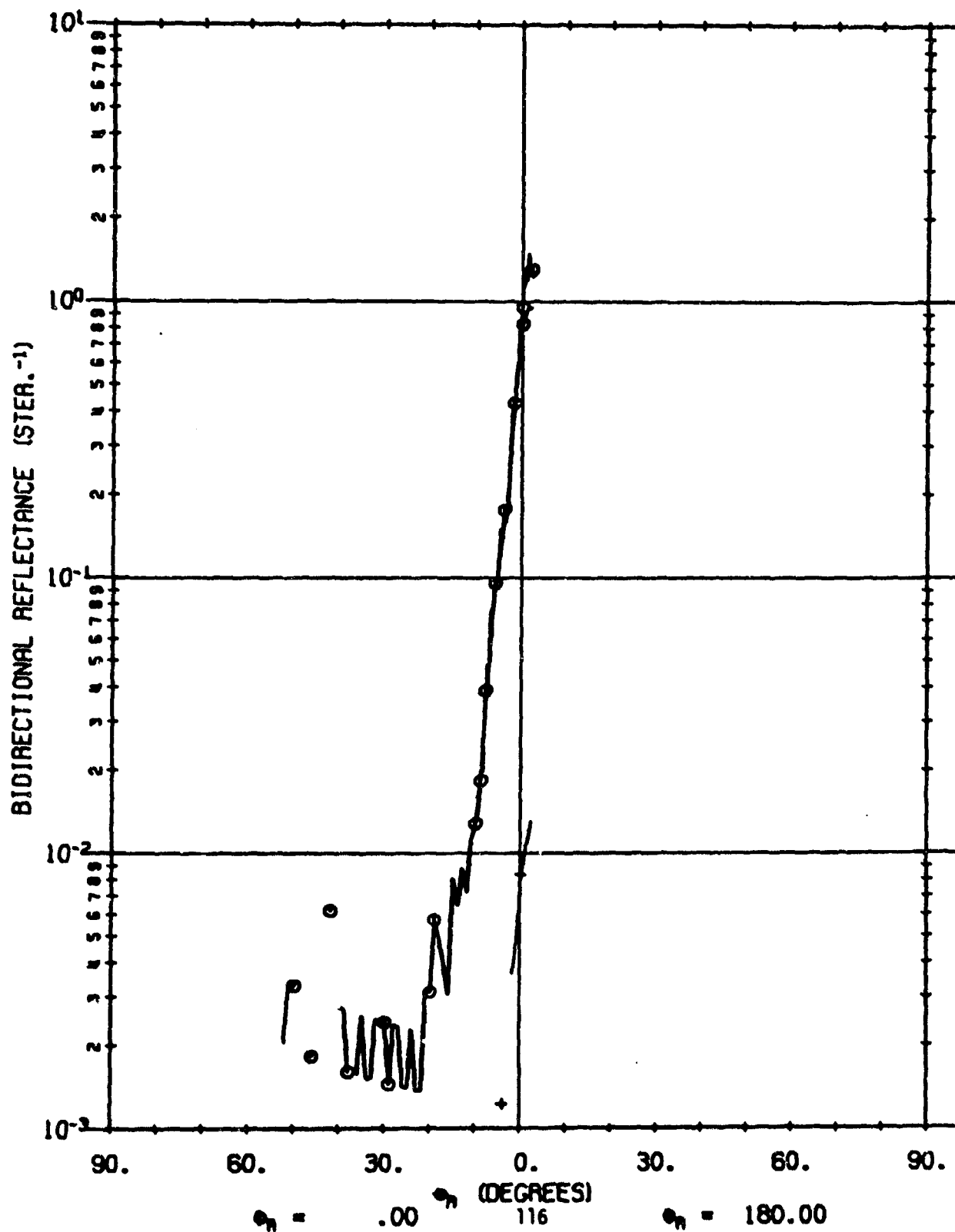
A02022 602

$\lambda = 10.60$   
 $\phi_i = -2.5$   
 $\phi_r = 180.0$



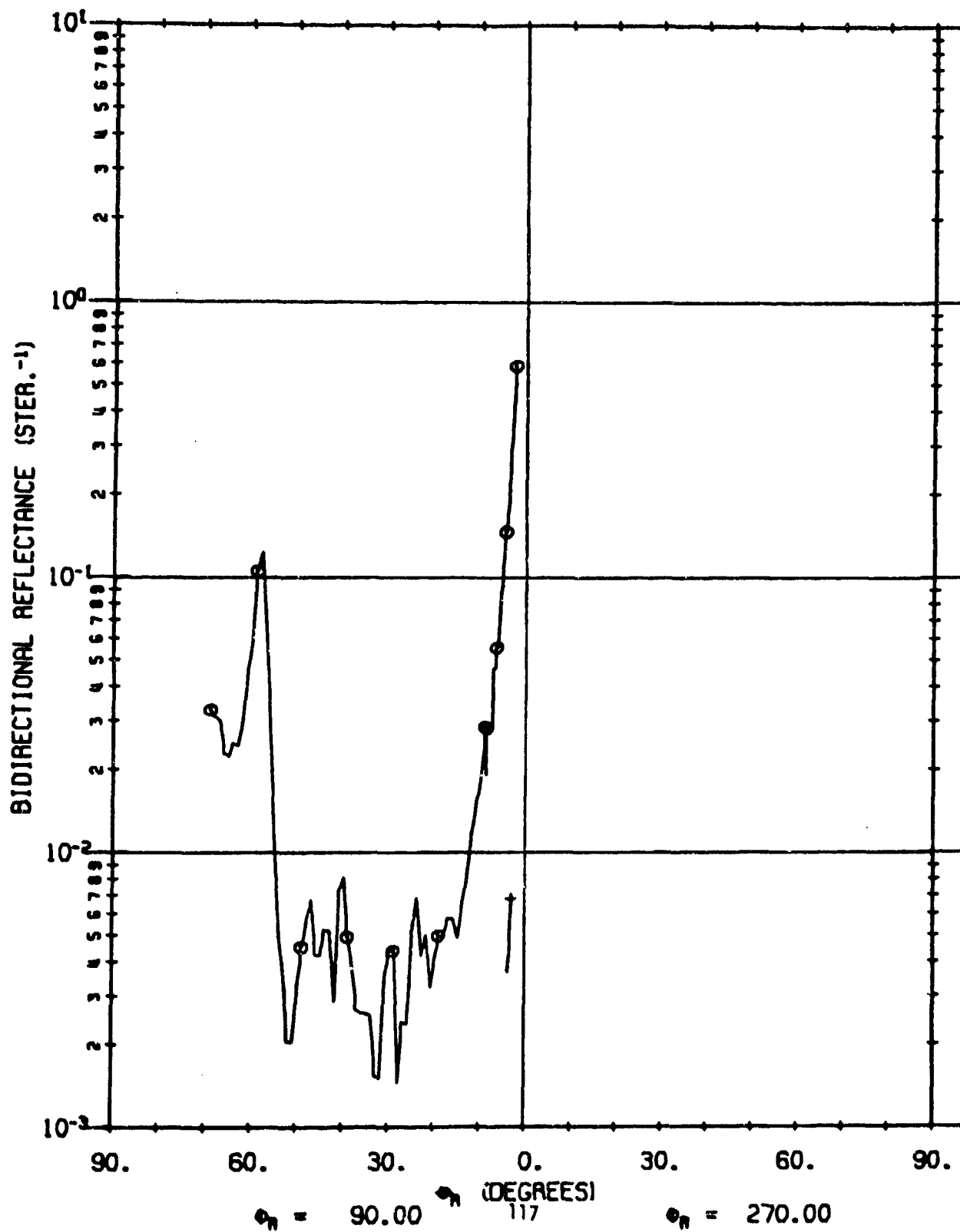
A02022 602

$\lambda = 10.60$   
 $\theta_i = \theta_r = 2.5$   
 $\phi_i = .0$



A02022 602

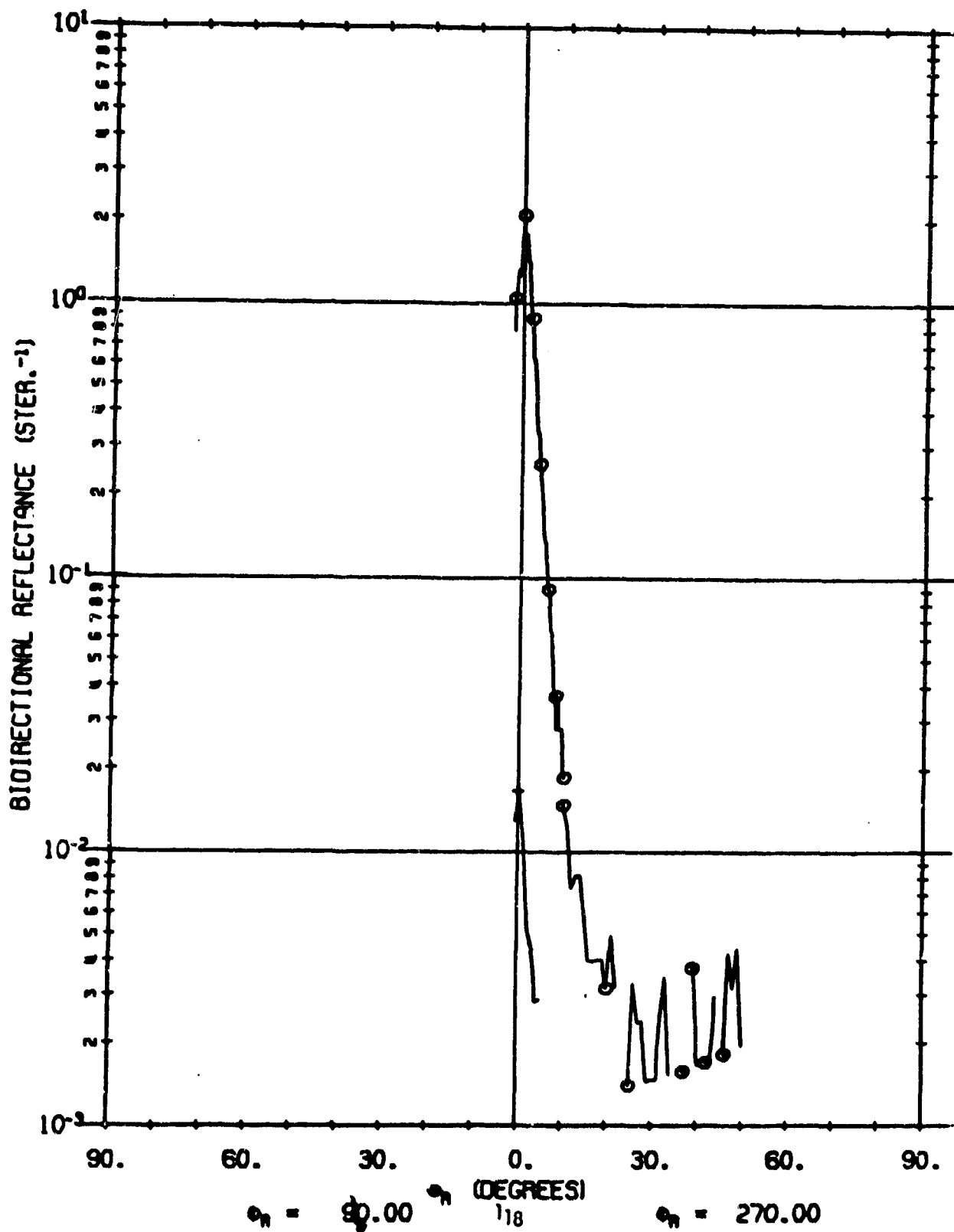
$\lambda = 10.60$   
 $\phi_i = \phi_n + -2.5$   
 $\phi_i = 90.0$





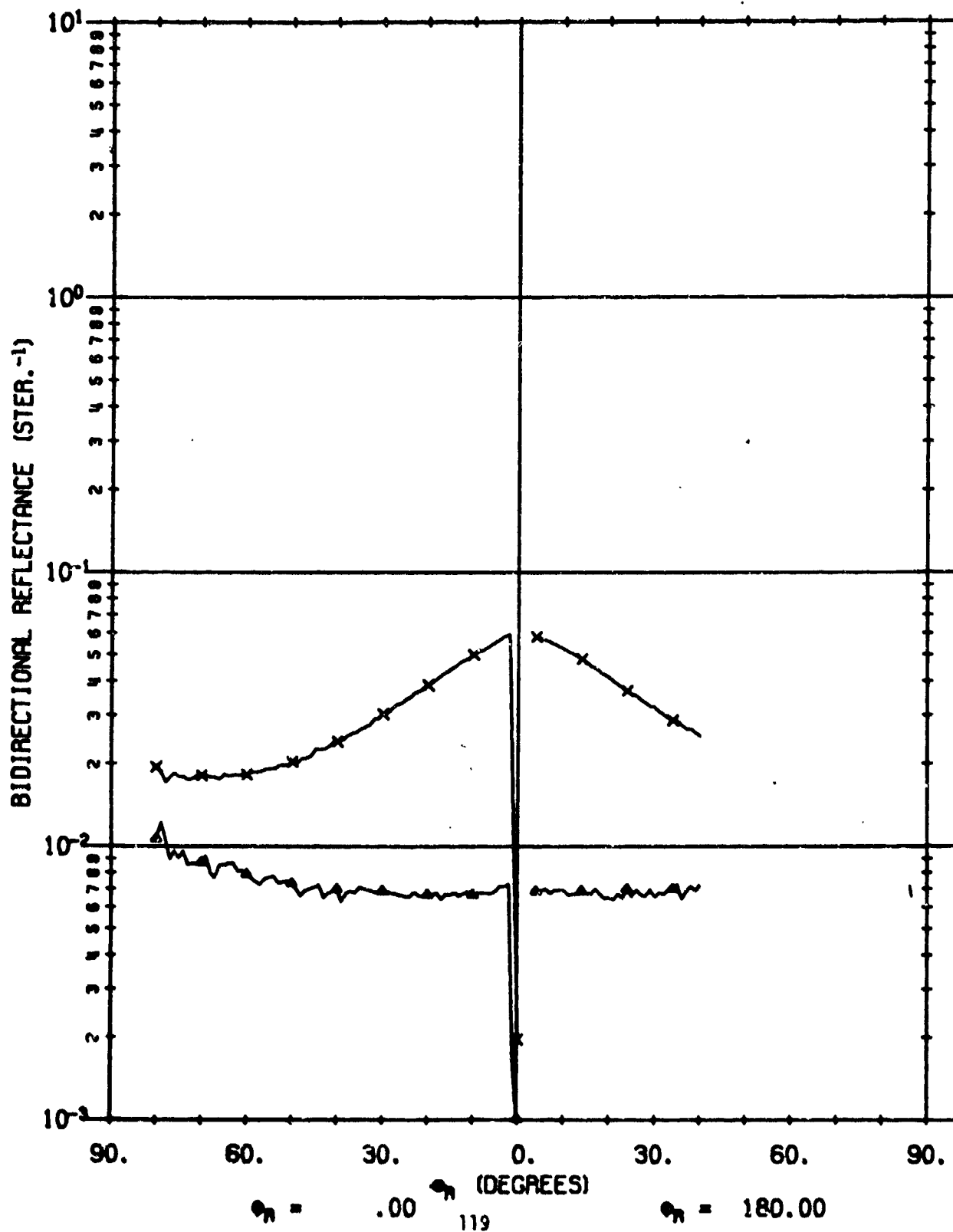
A02022 602

$\lambda = 10.60$   
 $\phi_i = 2.5$   
 $\phi_f = 270.0$



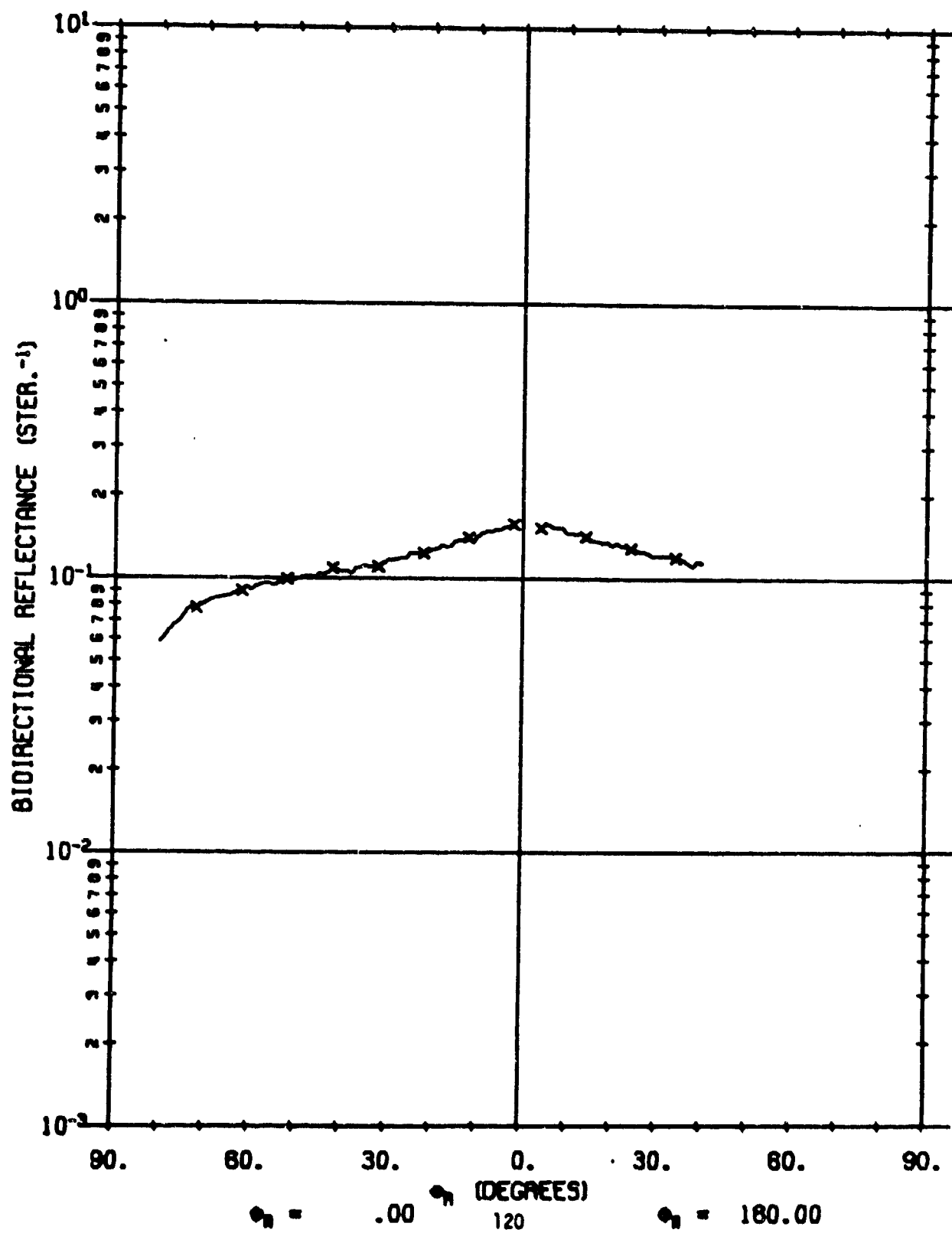
A01610 101

$\lambda = .63$   
 $\phi_i = .0$   
 $\phi_f = 180.0$



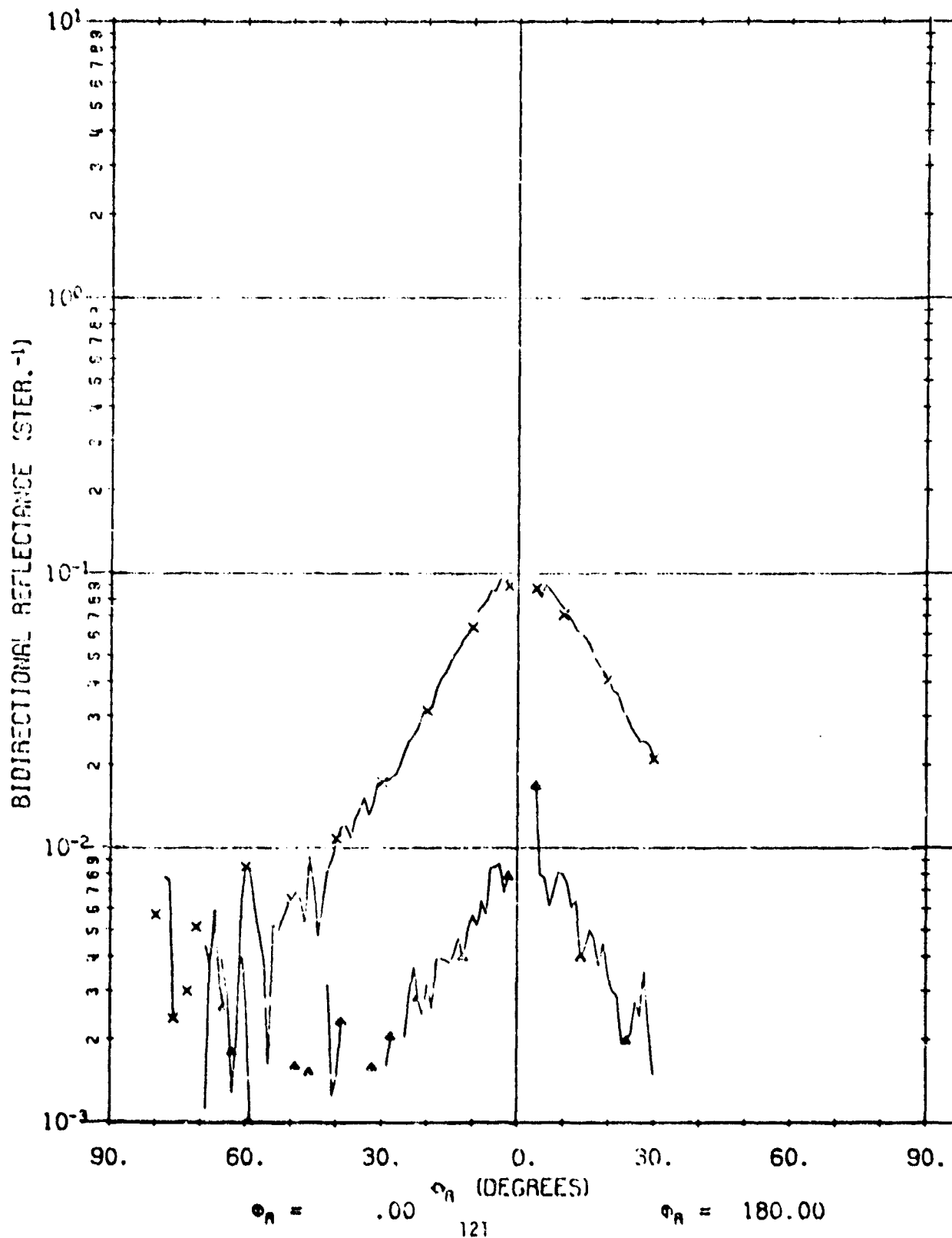
A01610 102

$\lambda = 1.06$   
 $\phi_i = .0$   
 $\phi_f = 180.0$



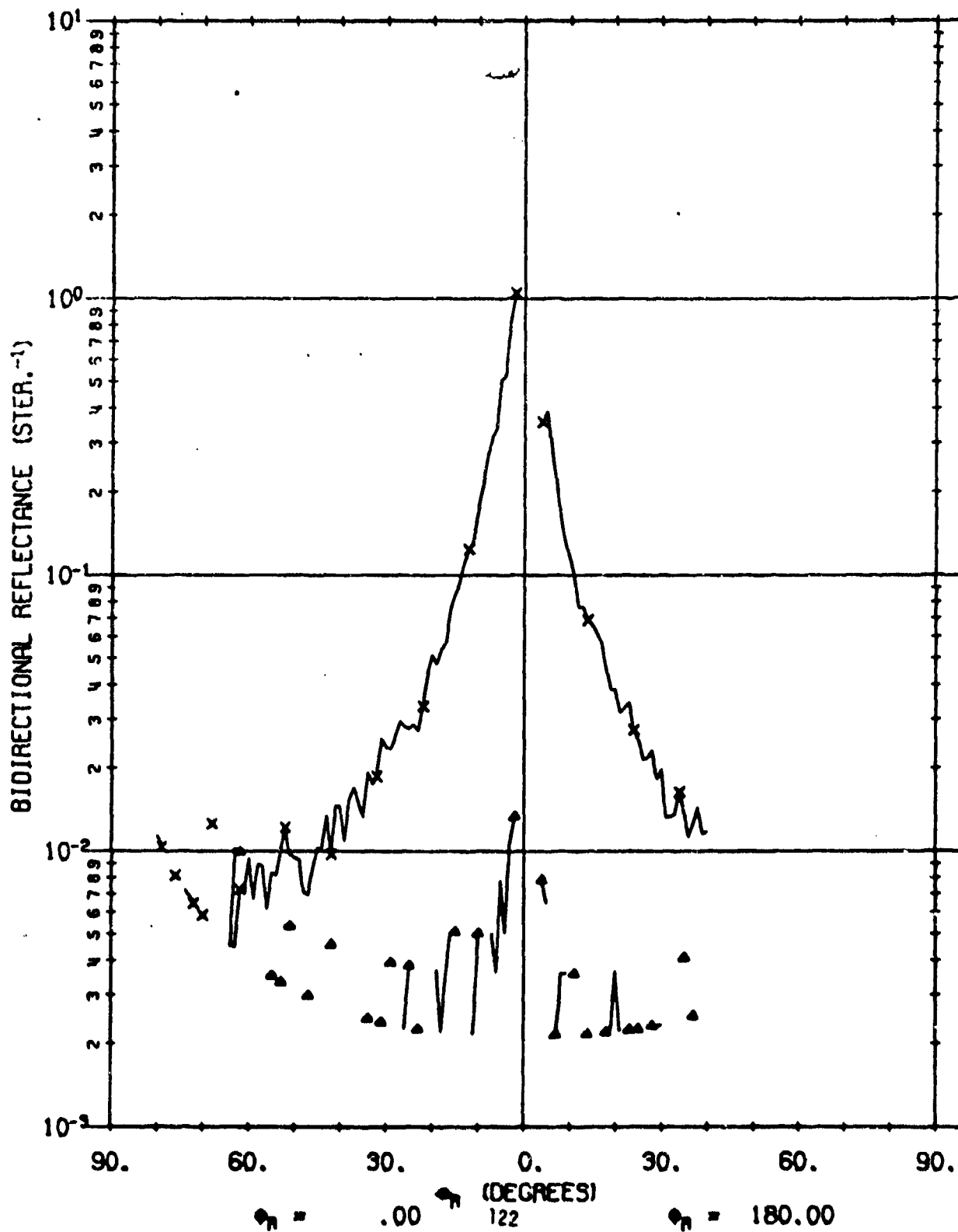
R01610 302

$\lambda = 3.39$   
 $\phi_i = .0$   
 $\phi_f = 180.0$



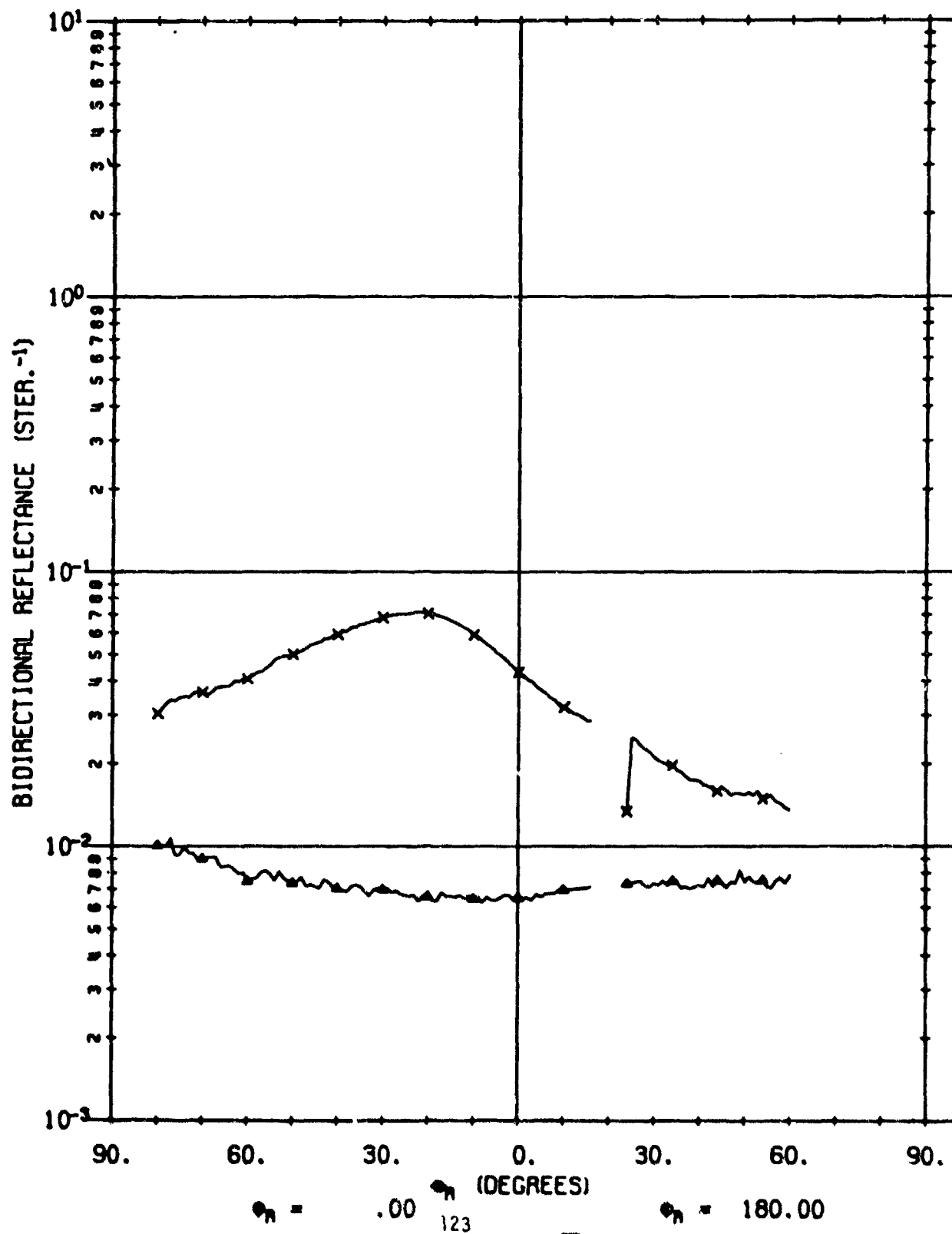
A01610 202

$\lambda = 10.60$   
 $\phi_1 = 0$   
 $\phi_2 = 180.0$



A01610 101

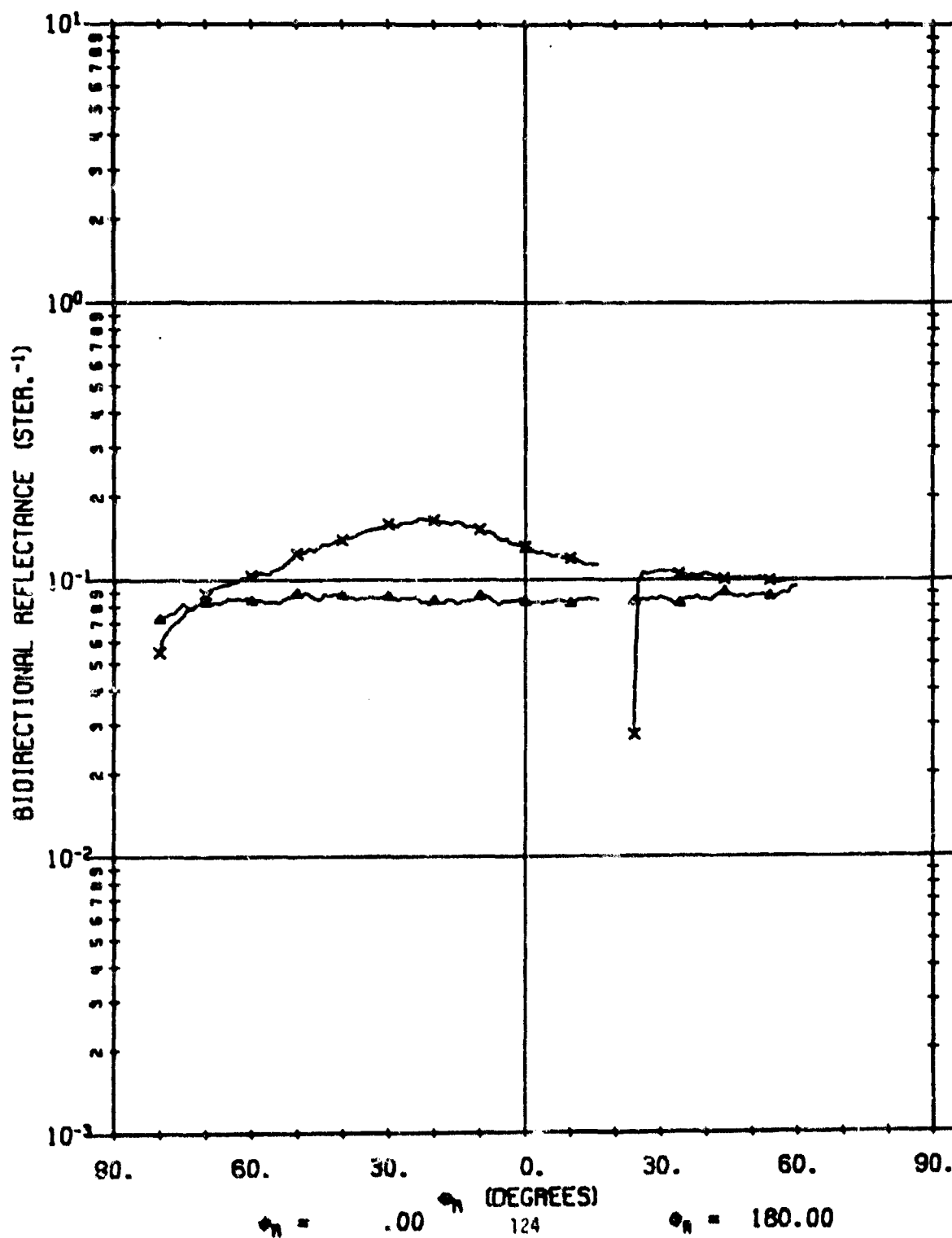
$\lambda = .63$   
 $\phi_i = 20.0$   
 $\phi_f = 180.0$



A01610 102

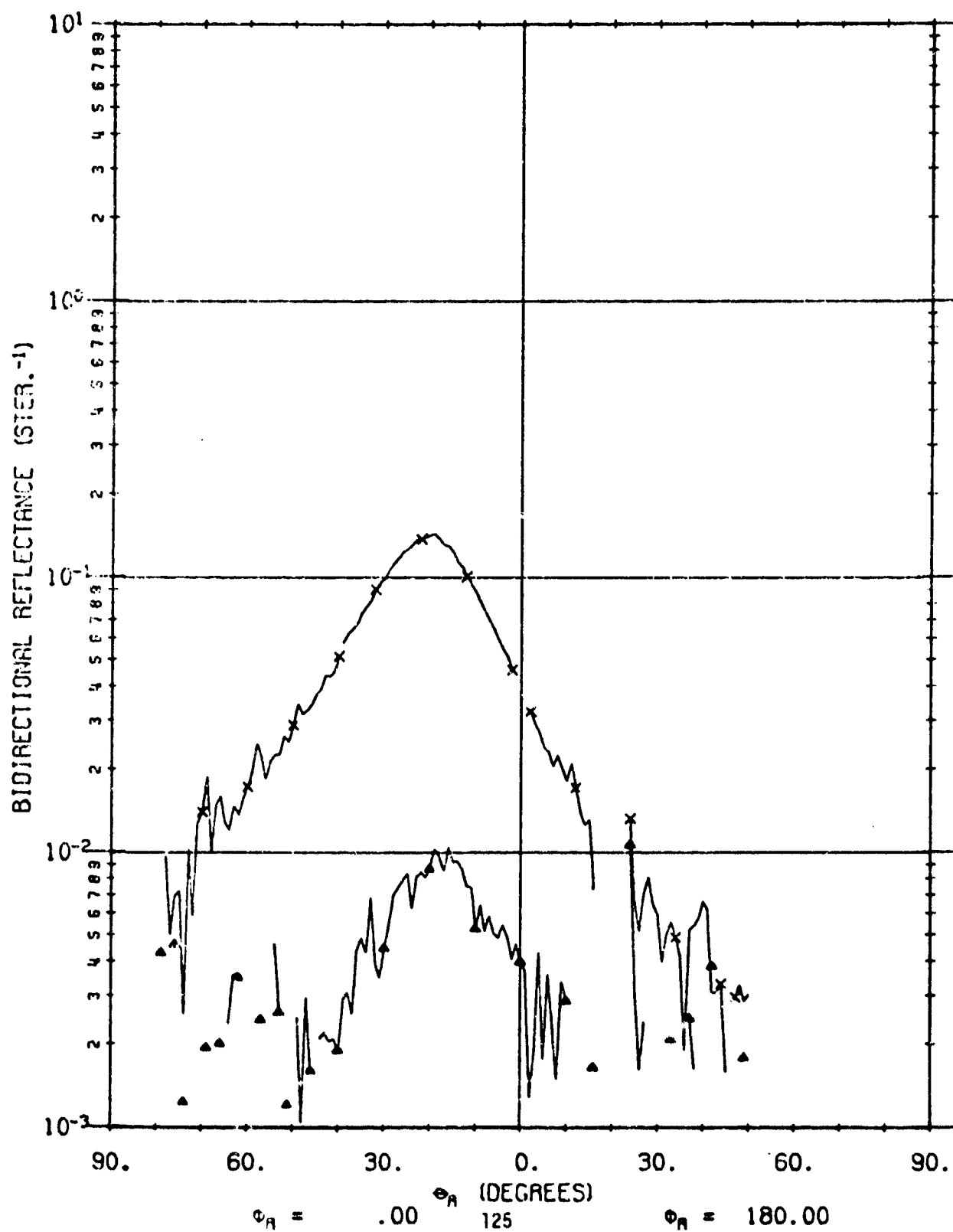
A-73

$\lambda = 1.06$   
 $\phi_i = 20.0$   
 $\phi_i = 180.0$



A01610 302

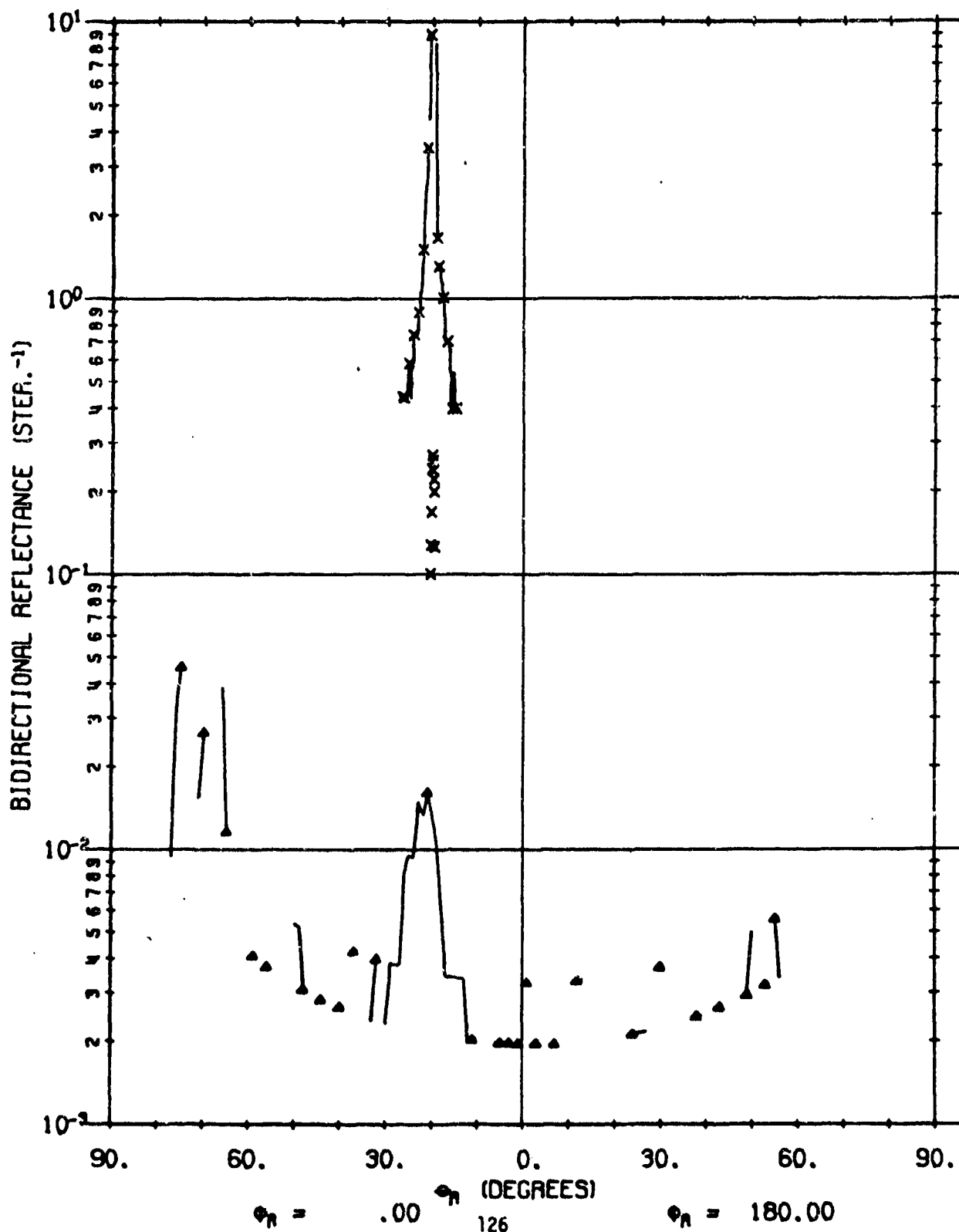
$\lambda = 3.39$   
 $\phi_i = 20.0$   
 $\phi_j = 180.0$





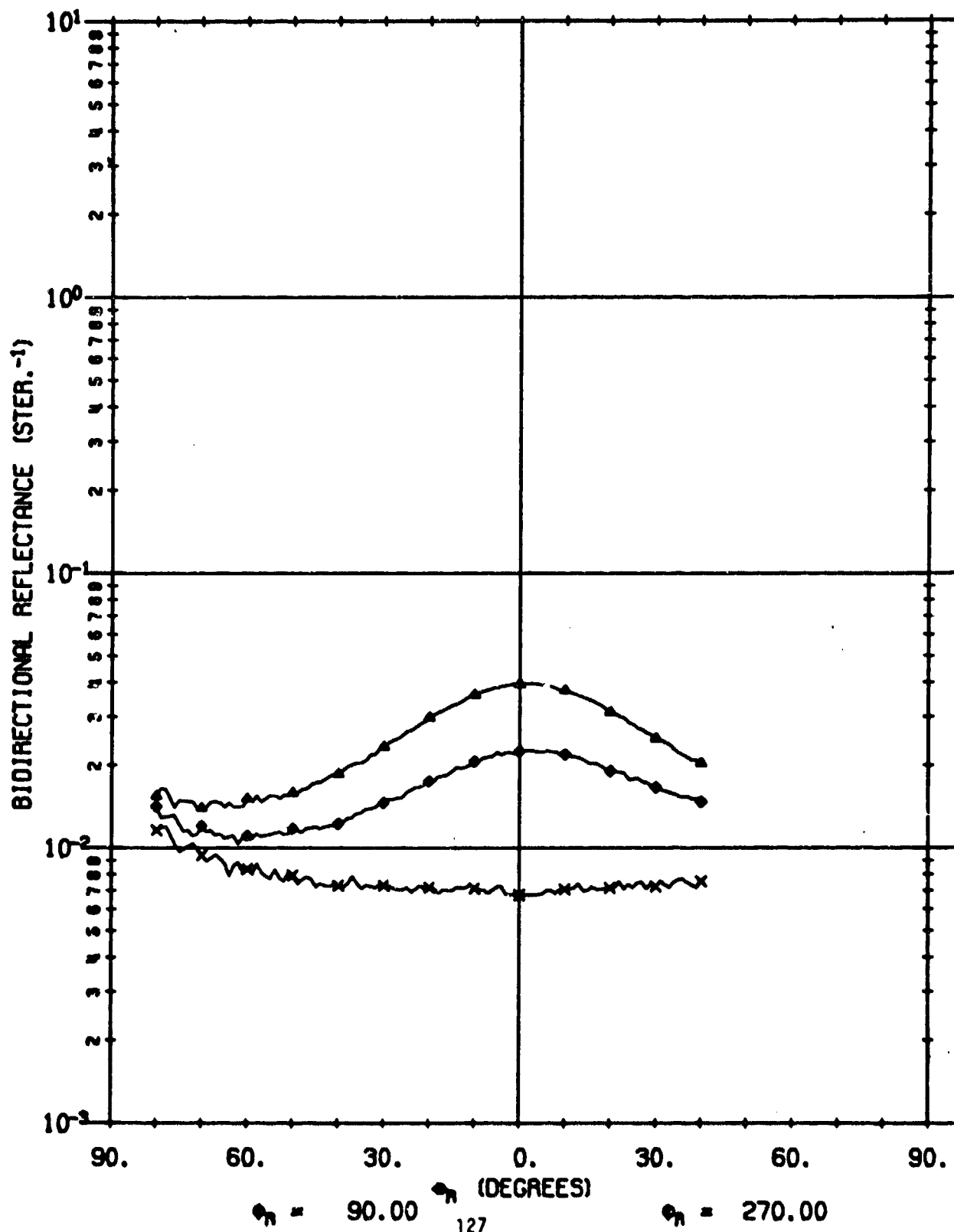
A01610 202

$\lambda = 10.60$   
 $\phi_i = 20.0$   
 $\phi_j = 180.0$



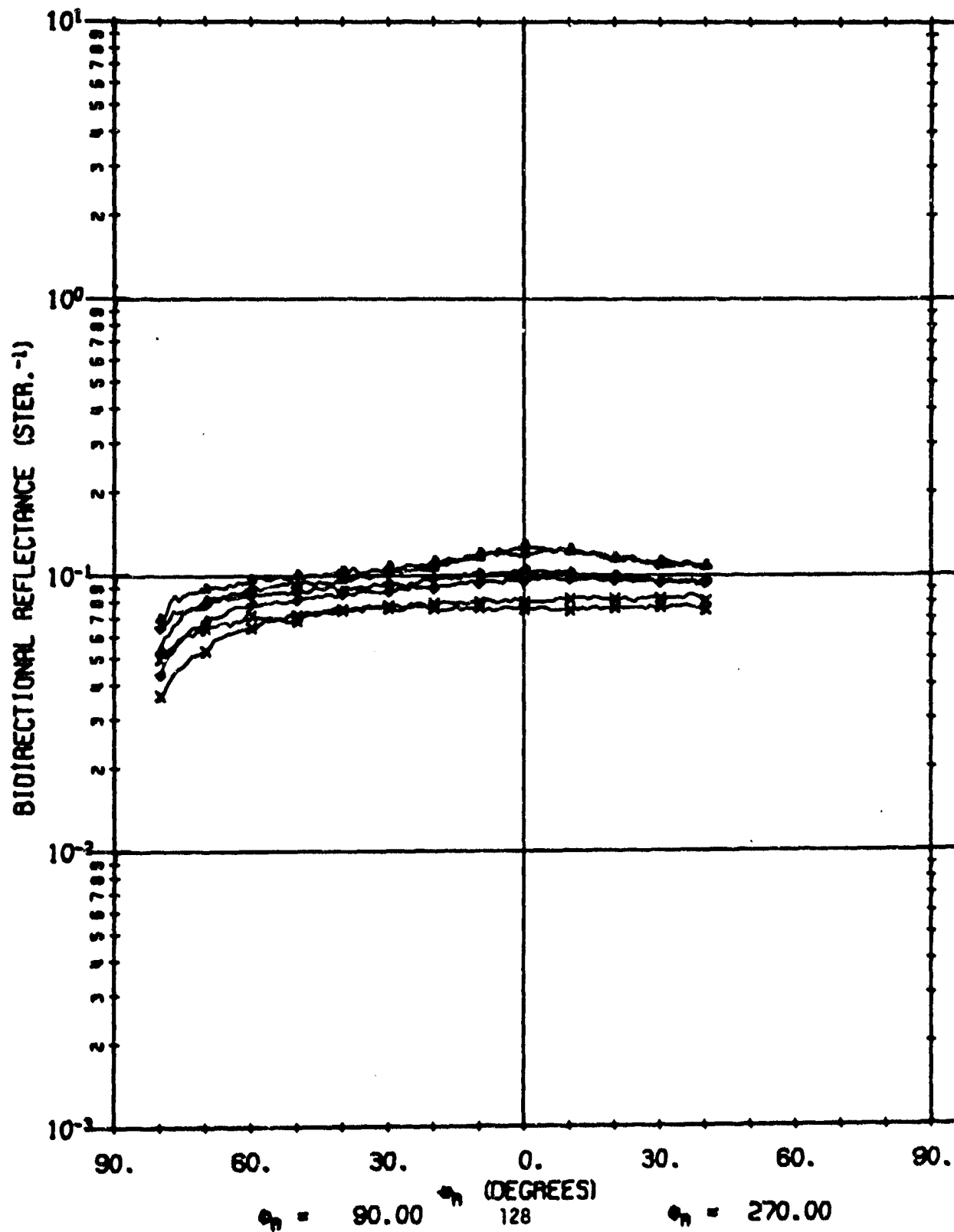
A01610 101

$\lambda = .63$   
 $\phi_i = 20.0$   
 $\phi_j = 180.0$



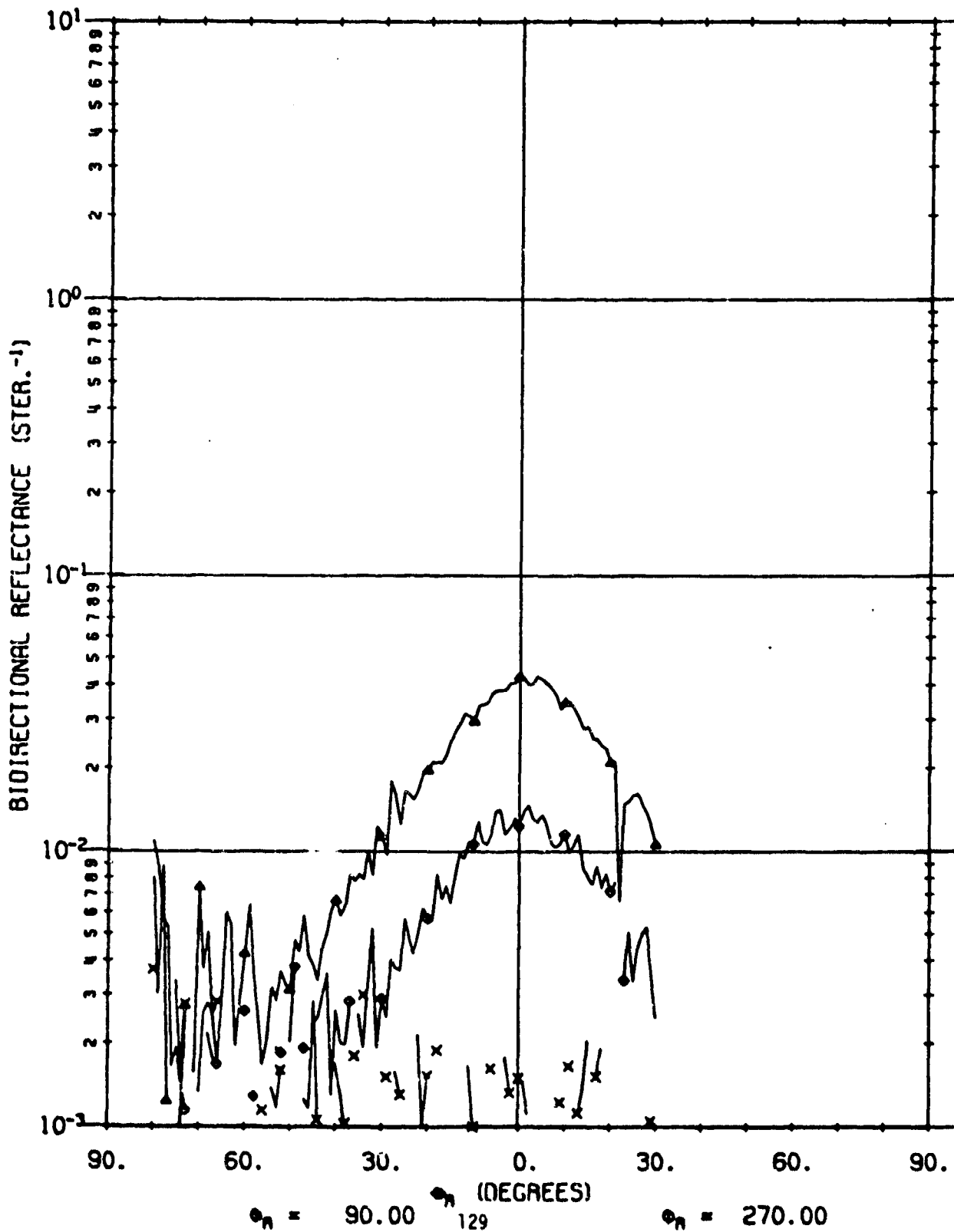
A01610 102

$\lambda = 1.06$   
 $\theta_i = 20.0$   
 $\theta_t = 180.0$



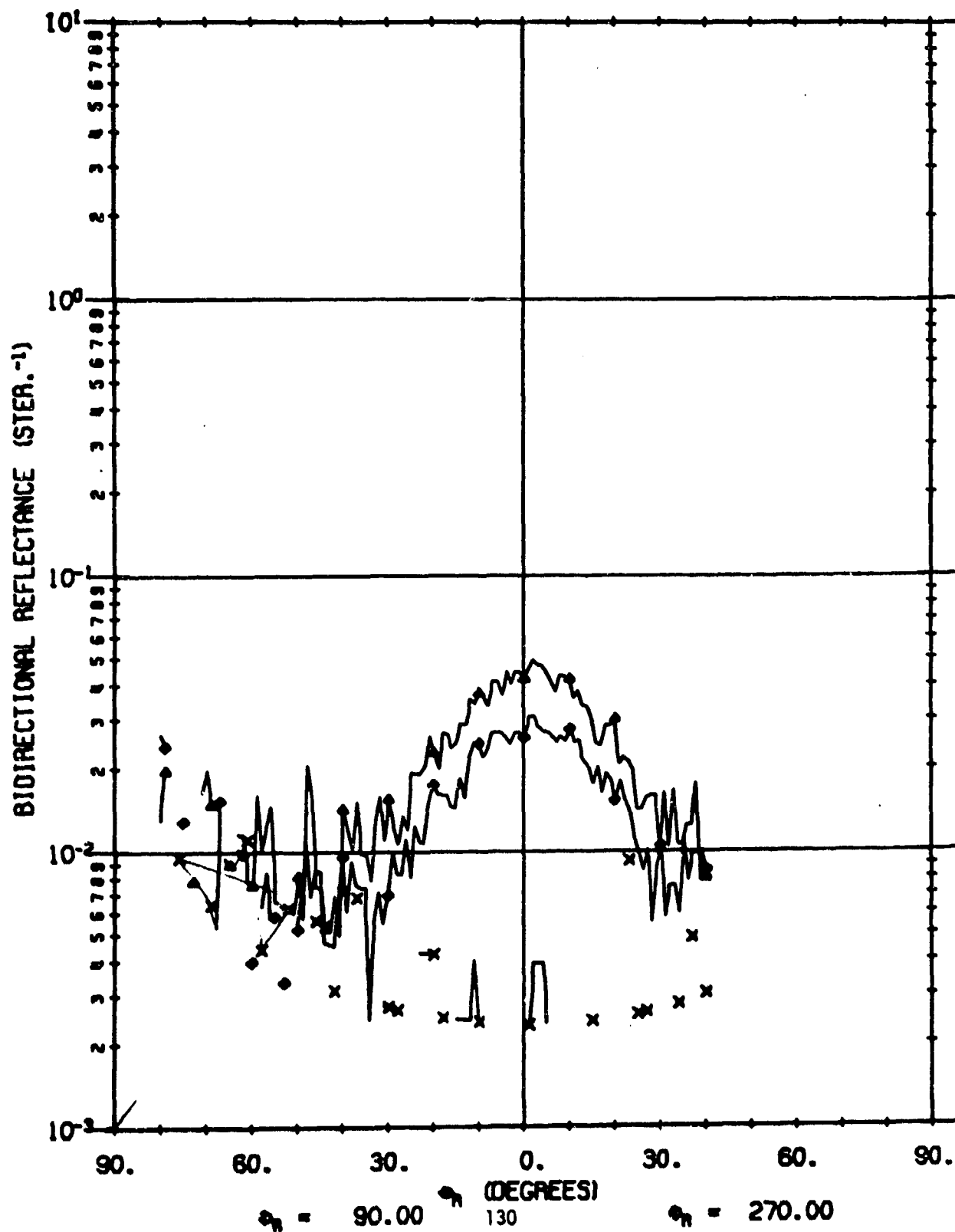
A01610 301

$\lambda = 3.39$   
 $\phi_1 = 20.0$   
 $\phi_2 = 180.0$



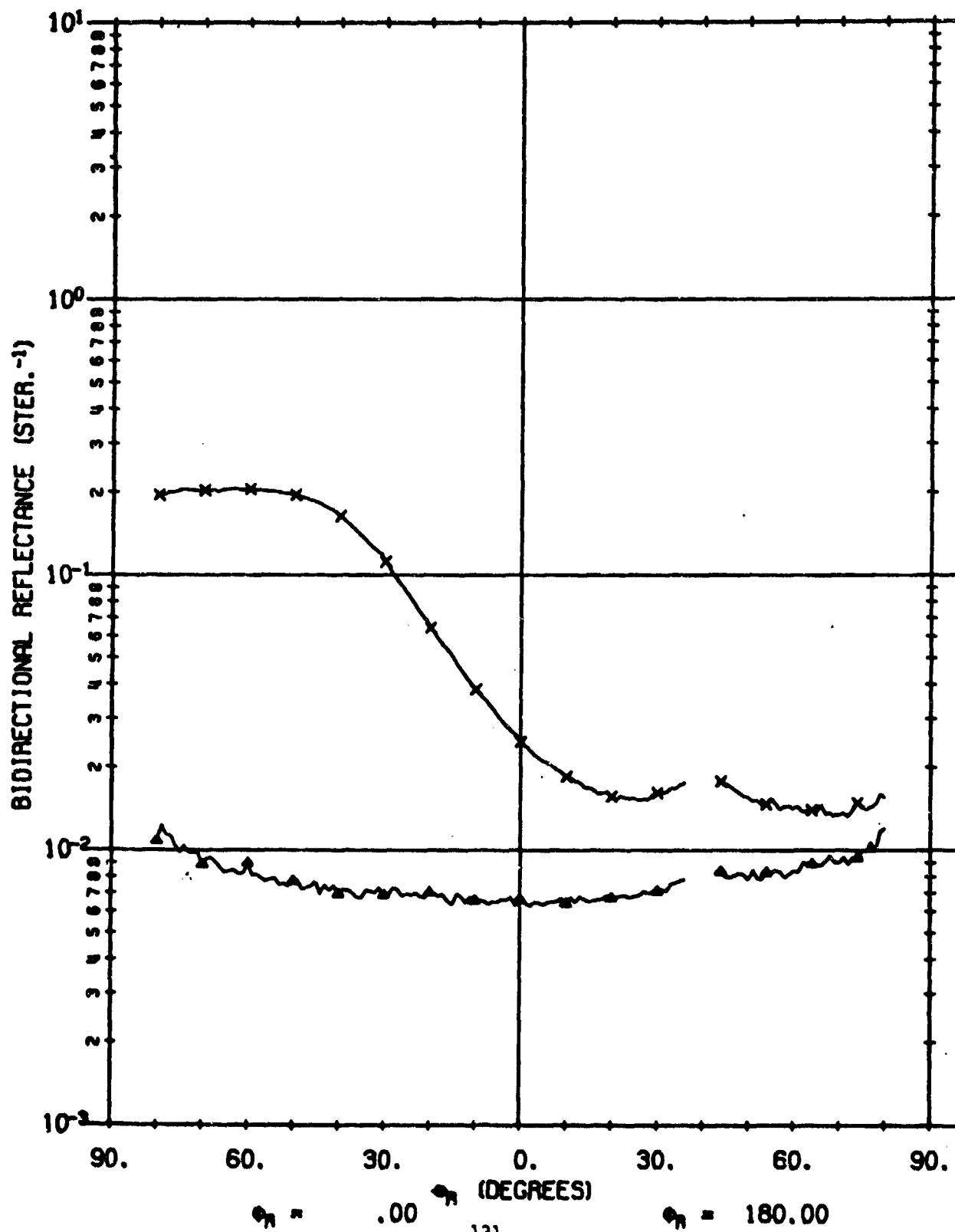
A01610 204

$\lambda = 10.60$   
 $\phi_i = 20.0$   
 $\phi_t = 180.0$



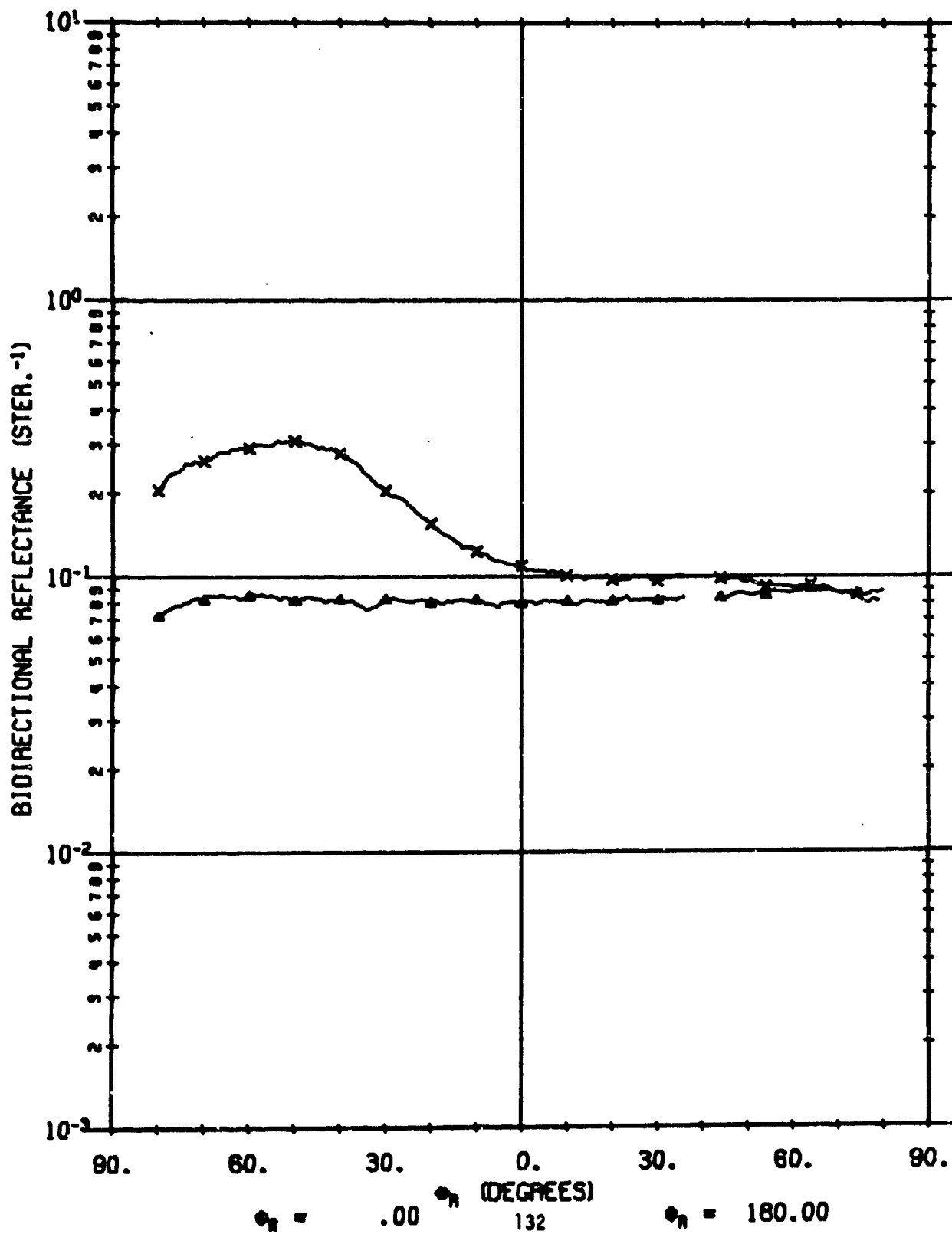
A01610 101

$\lambda = .63$   
 $\phi_i = 40.0$   
 $\phi_f = 180.0$



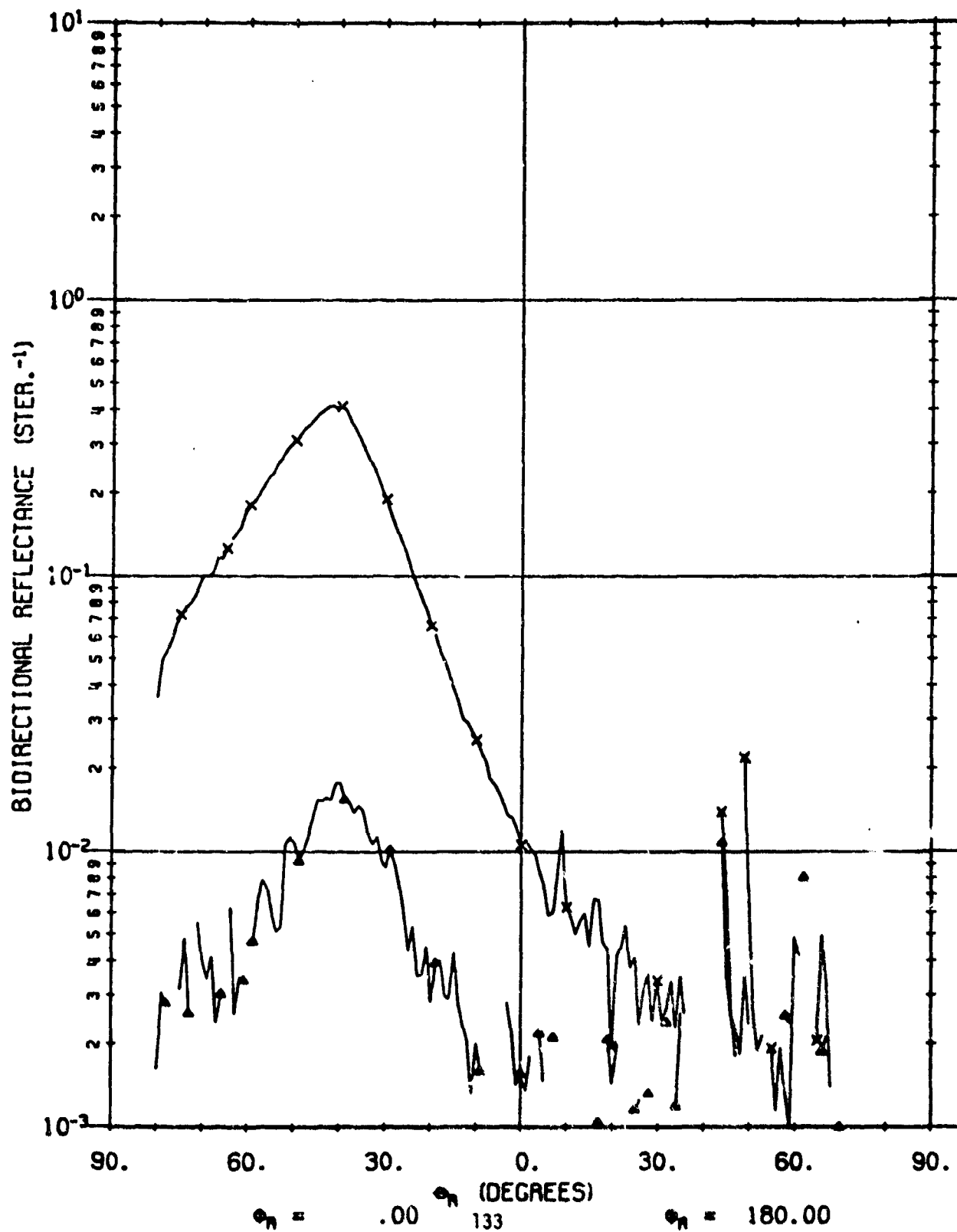
A01610 102

$\lambda = 1.06$   
 $\phi_i = 40.0$   
 $\phi_f = 180.0$



A01610 302

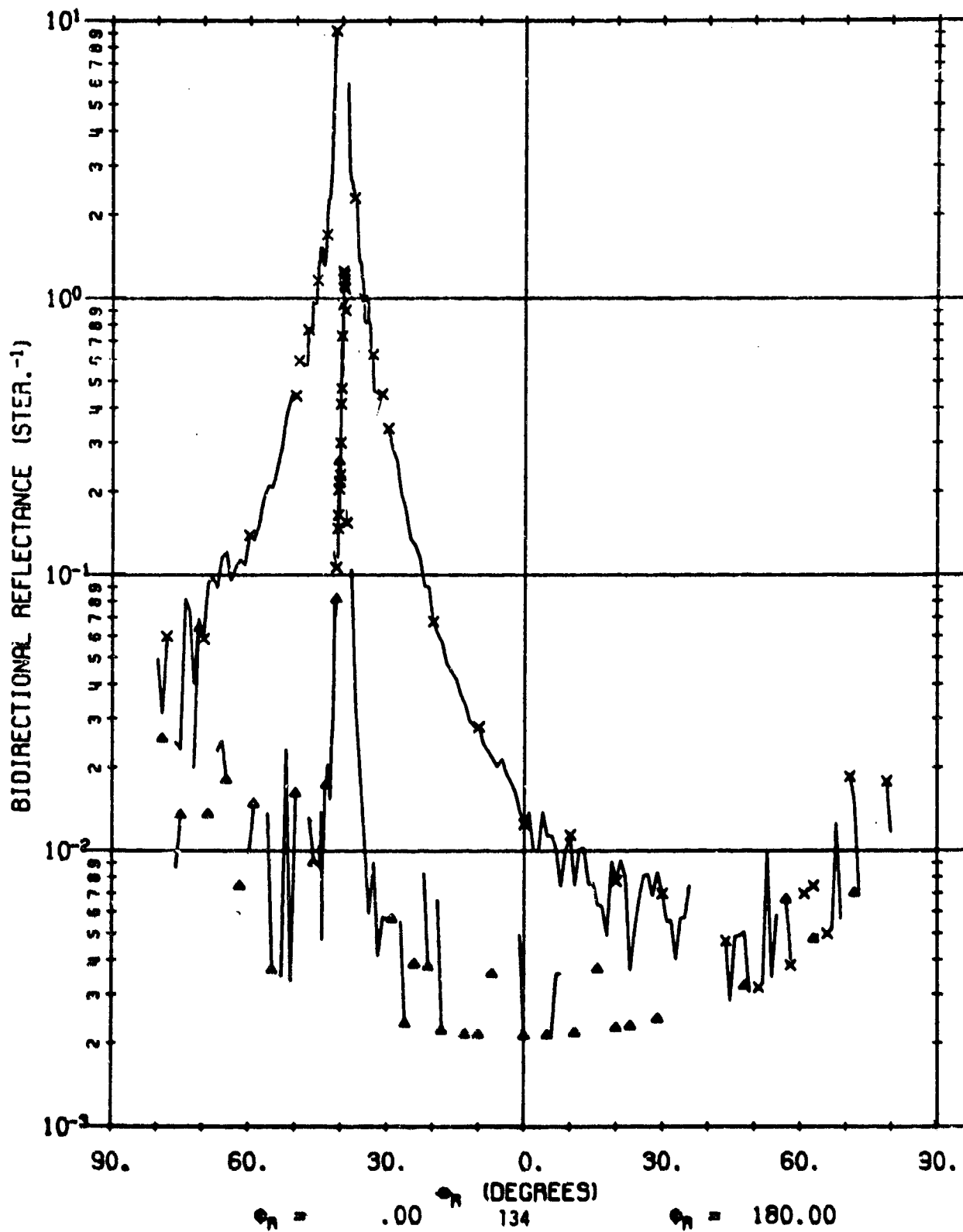
$\lambda = 3.39$   
 $\phi_i = 40.0$   
 $\phi_f = 180.0$





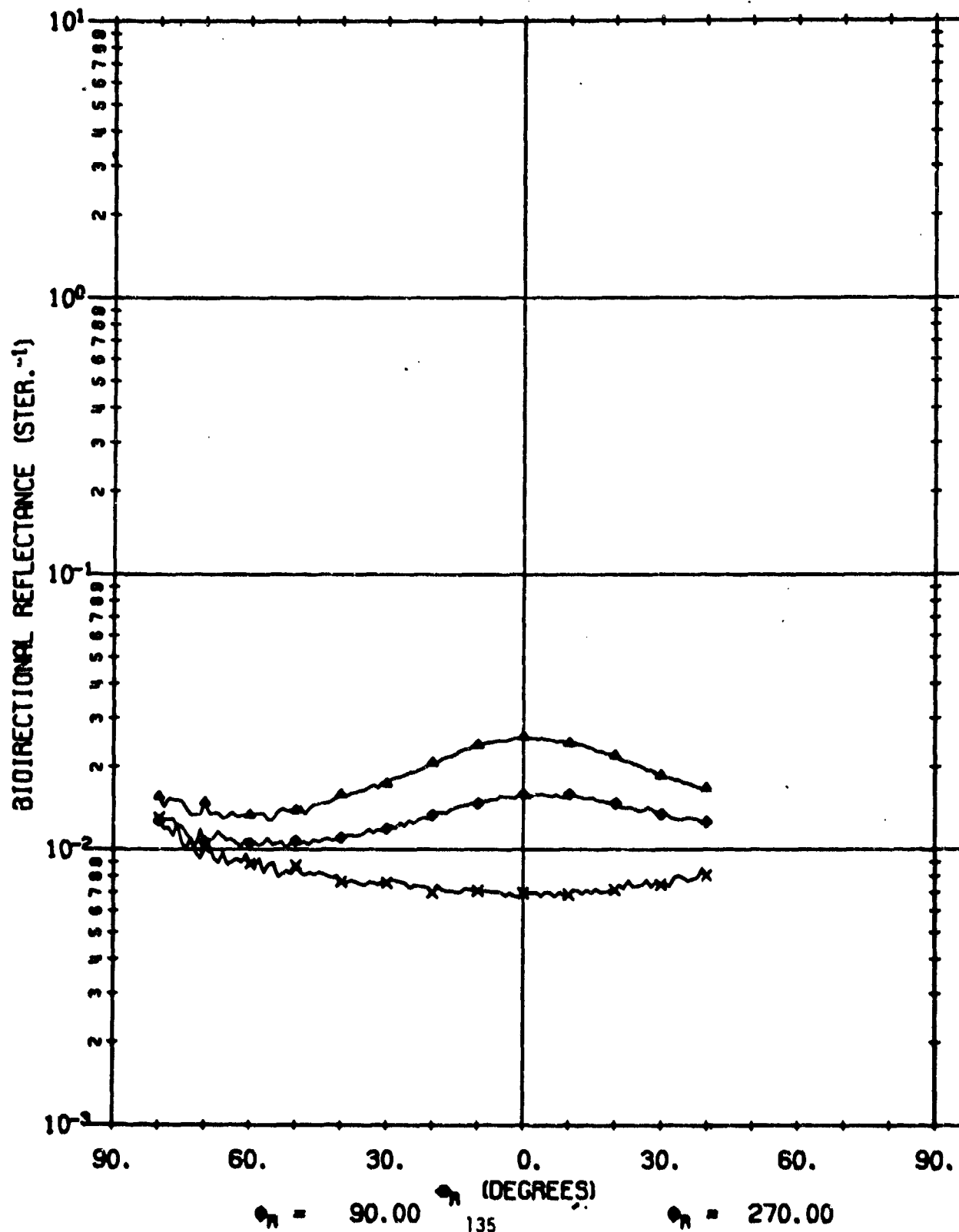
A01G10 202

$\lambda = 10.60$   
 $\phi_i = 10.0$   
 $\phi_f = 160.0$



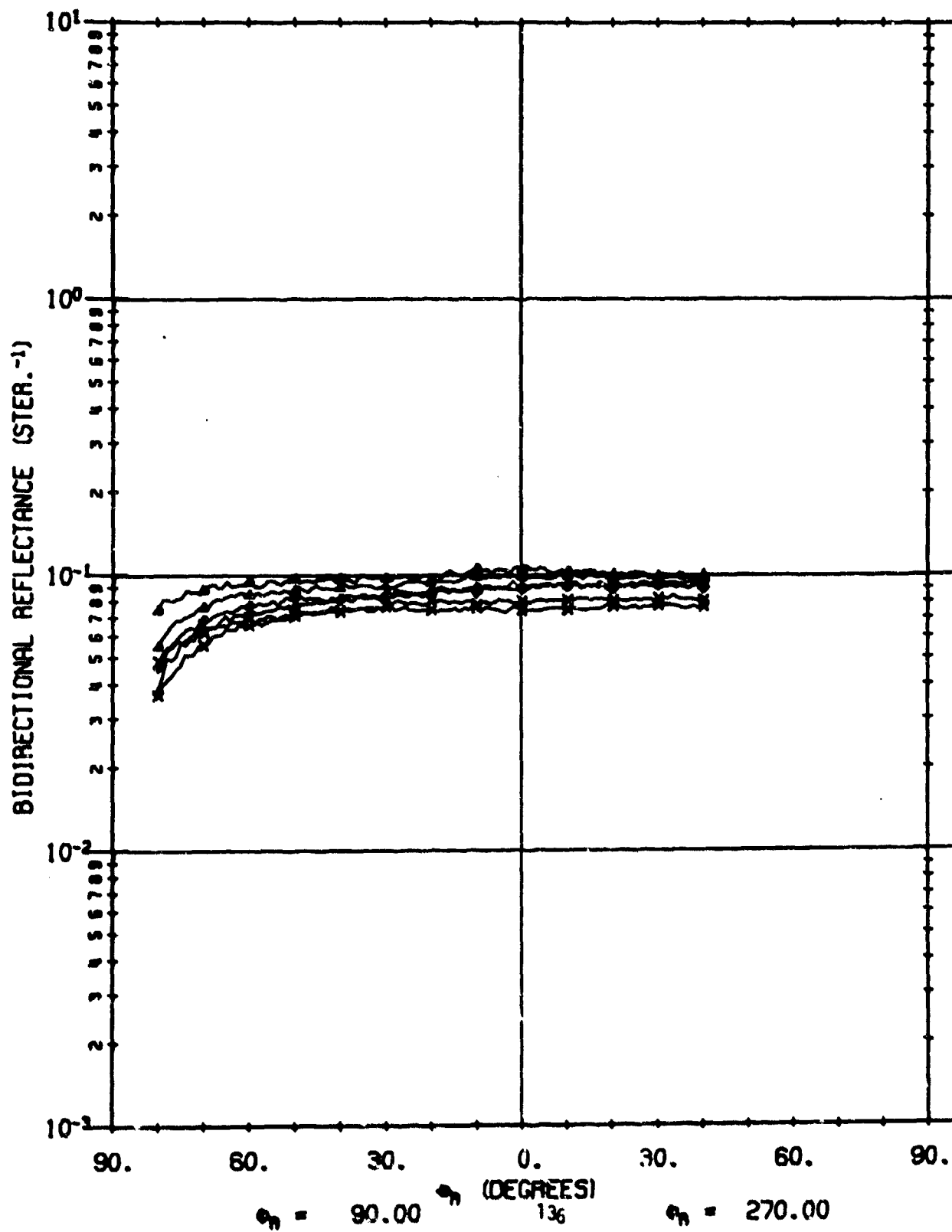
A01610 101

$\lambda = .63$   
 $\phi_1 = 40.0$   
 $\phi_2 = 180.0$



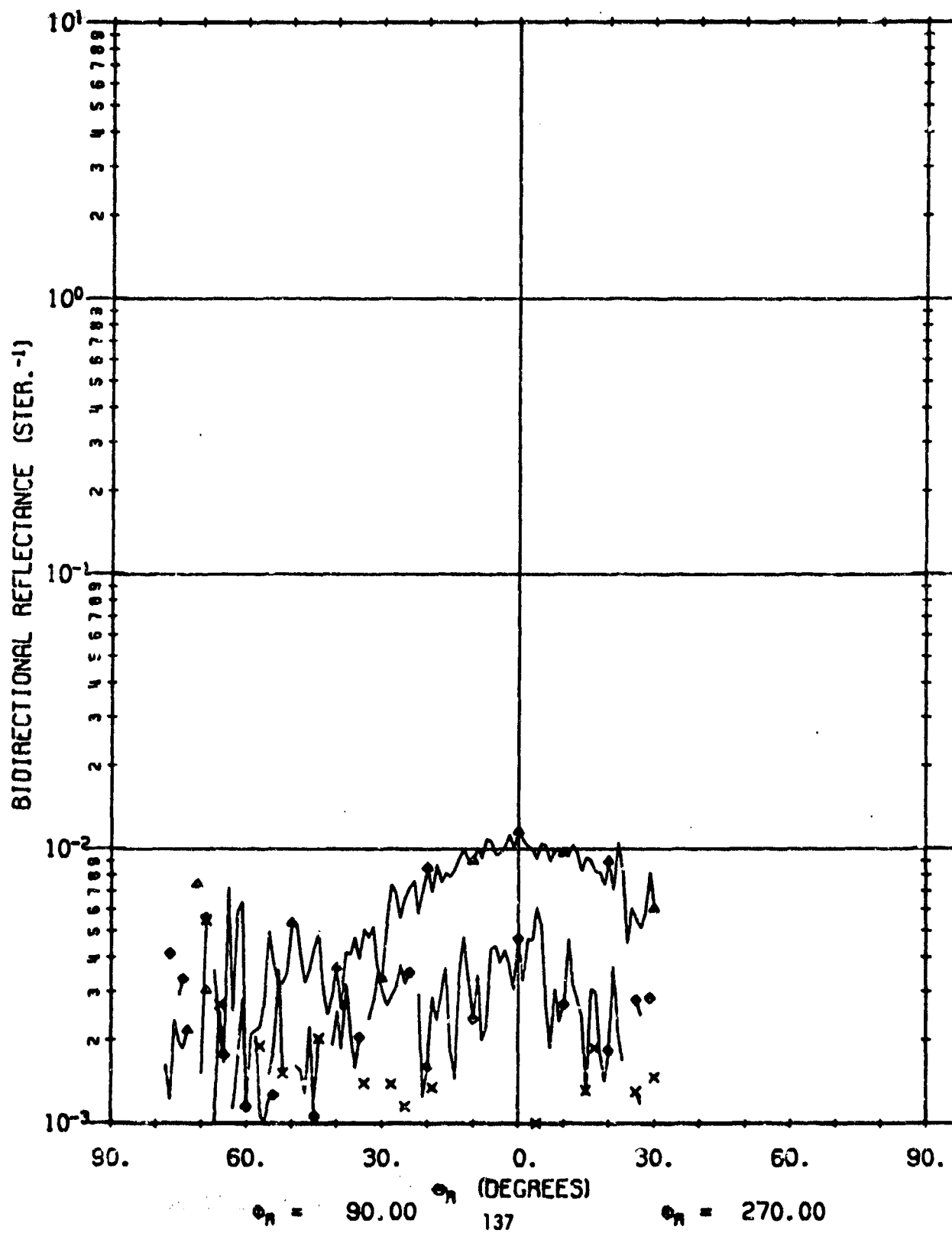
A01610 102

$\lambda = 1.06$   
 $\phi_i = 40.0$   
 $\phi_f = 180.0$



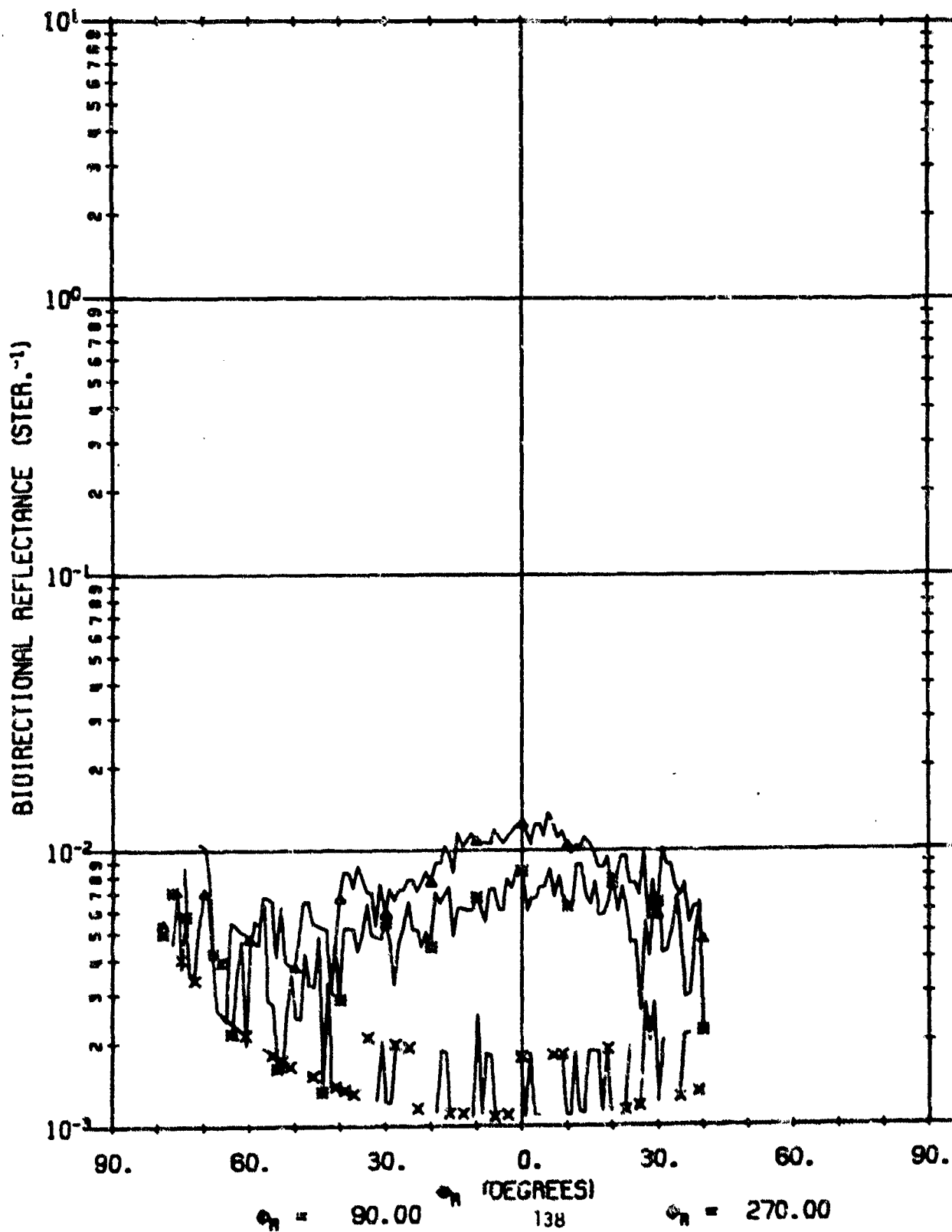
A01610 301

$\lambda = 3.39$   
 $\phi_1 = 40.0$   
 $\phi_i = 180.0$



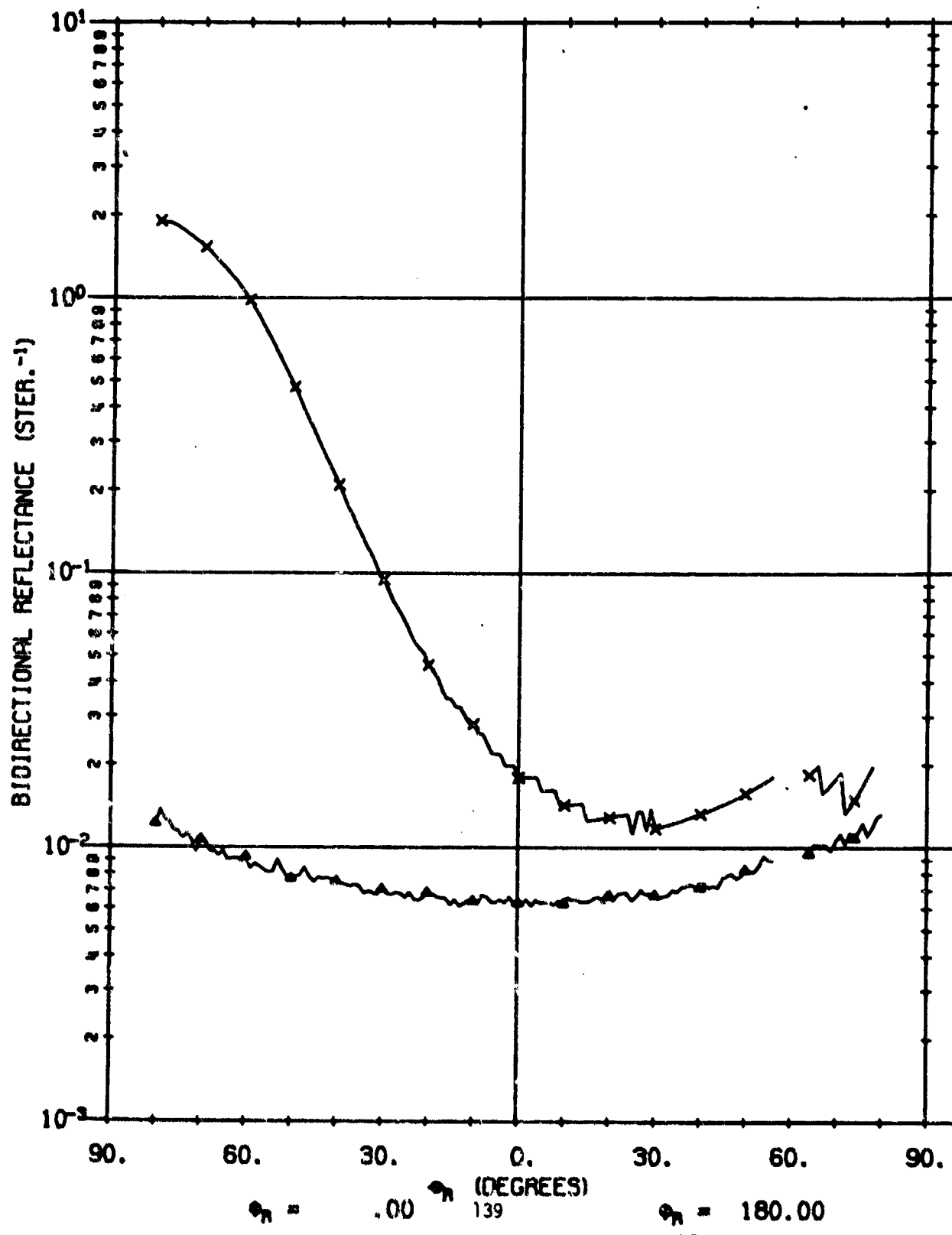
A01610 201

$\lambda = 10.60$   
 $\phi_i = 40.0$   
 $\phi_i = 180.0$



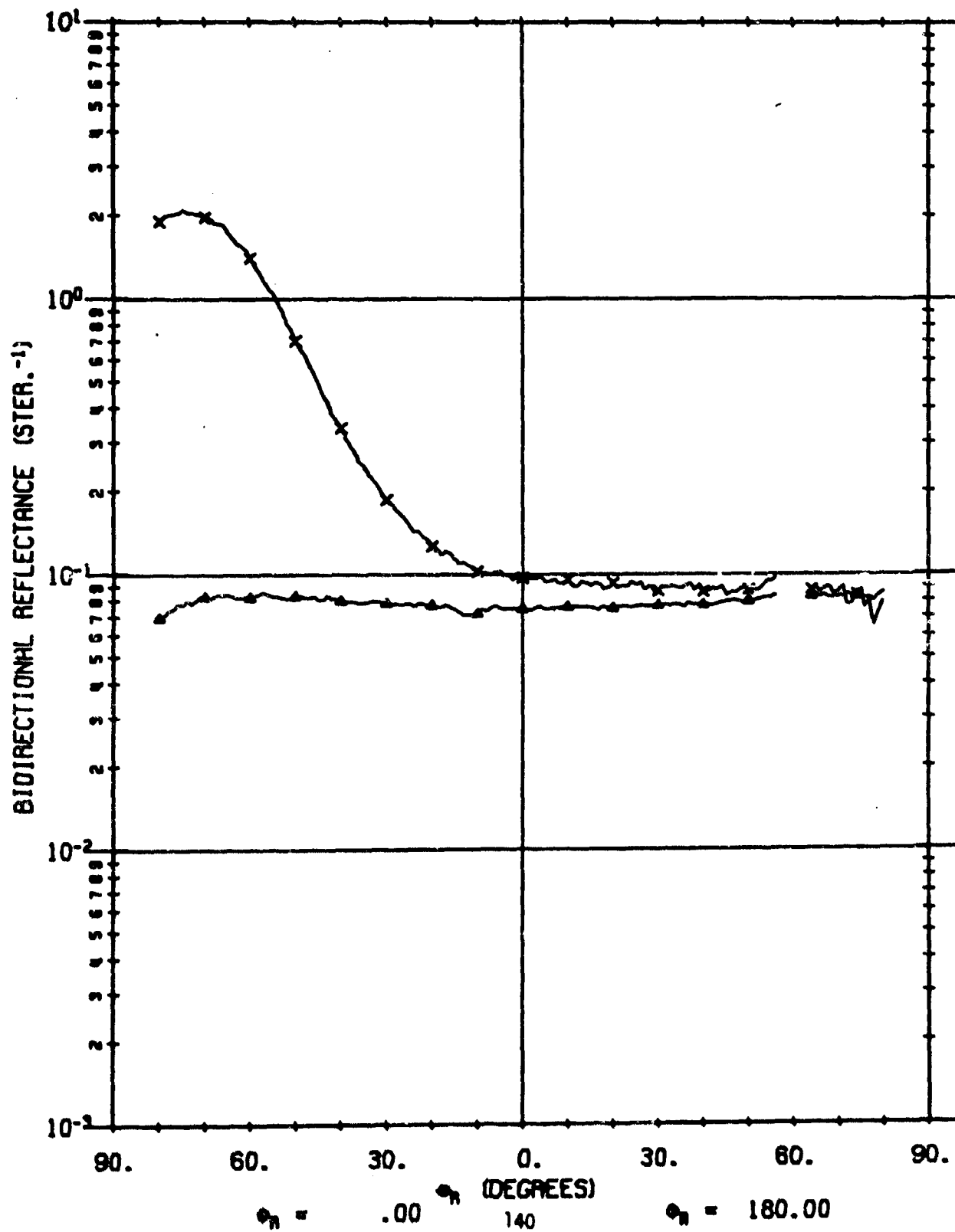
A01610 101

$\lambda = .63$   
 $\phi_1 = 60.0$   
 $\phi_2 = 180.0$



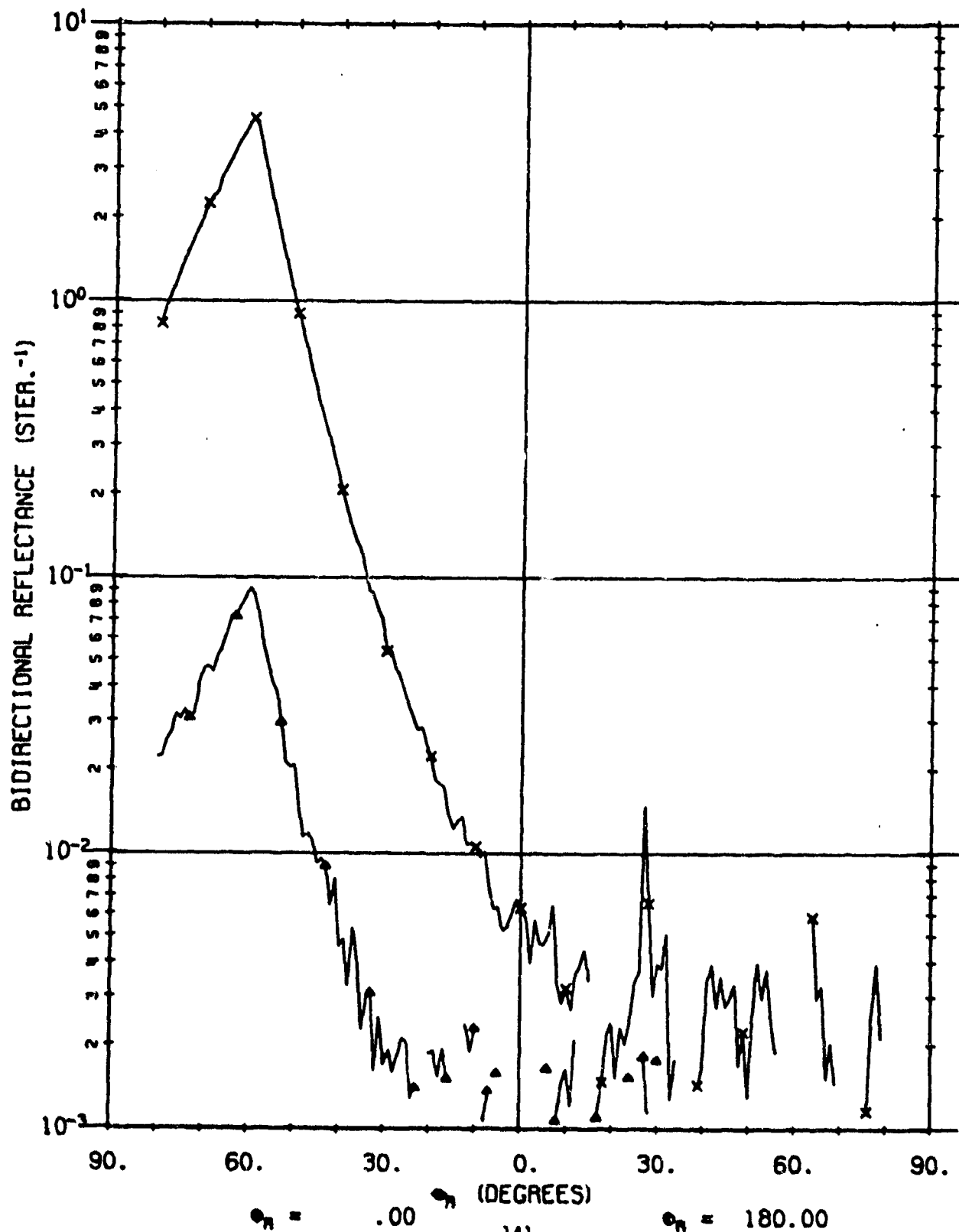
A01610 102

$\lambda = 1.06$   
 $\phi_i = 60.0$   
 $\phi_i = 180.0$



A01610 302

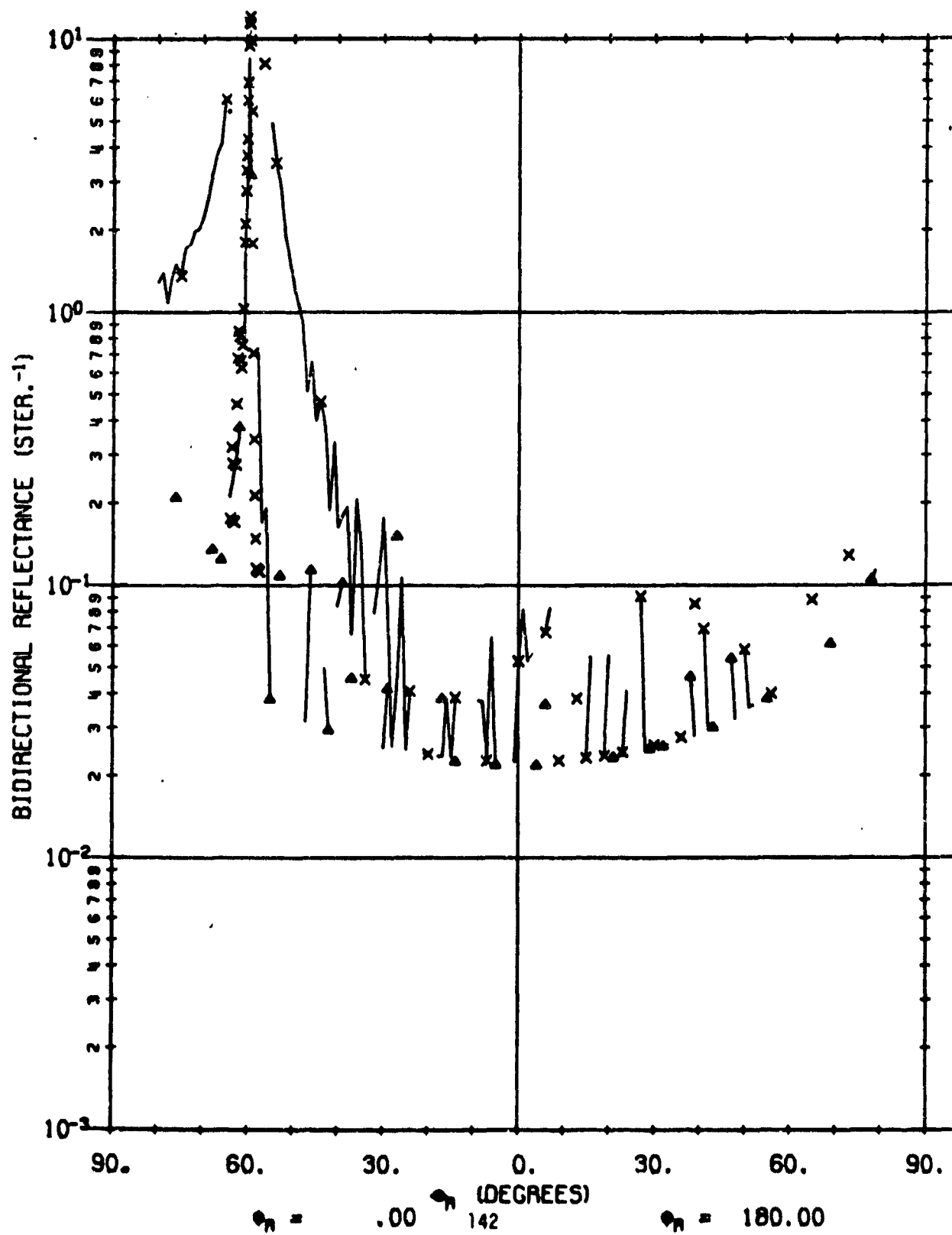
$\lambda = 3.39$   
 $\phi_i = 60.0$   
 $\phi_j = 180.0$





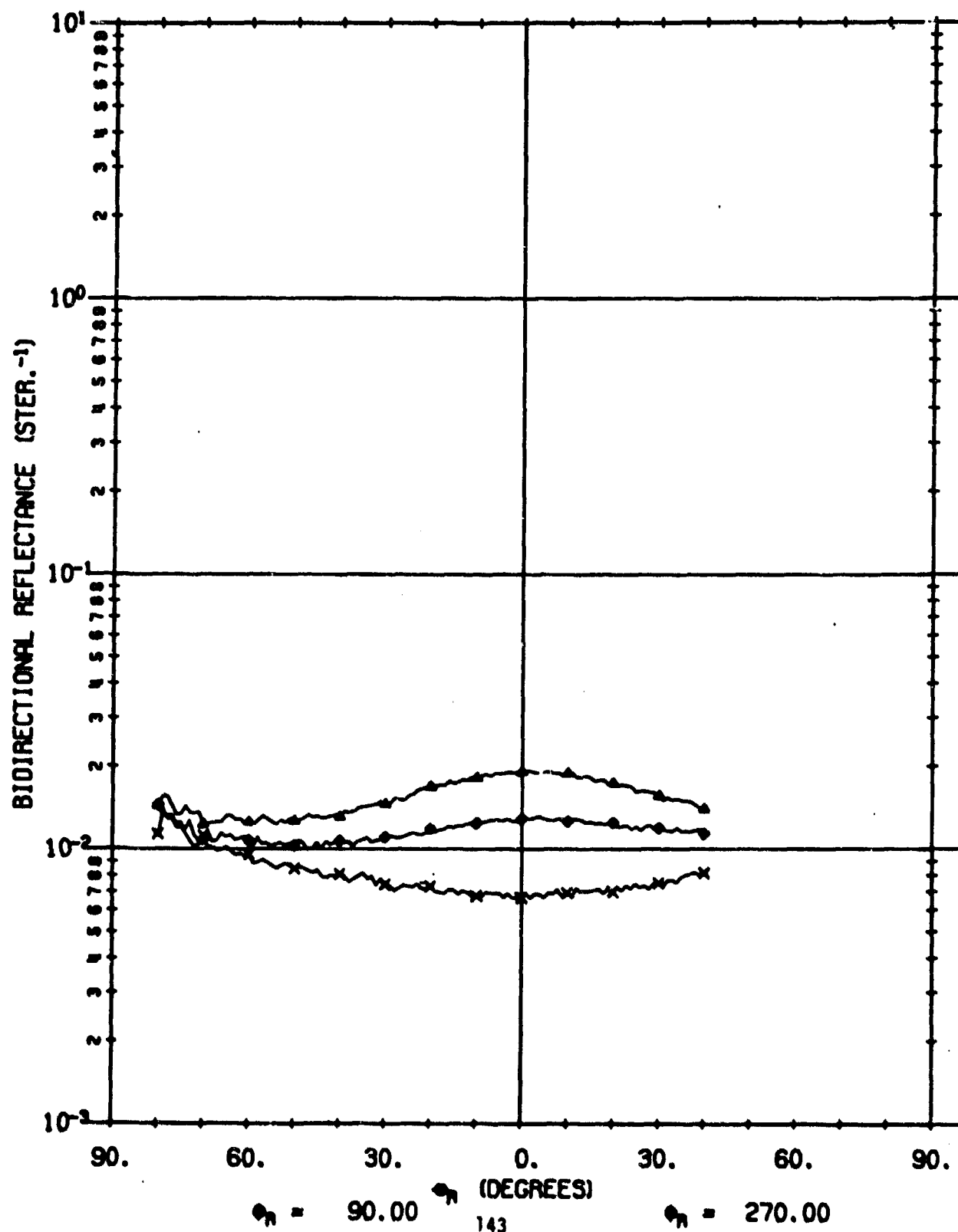
A01610 202

$\lambda = 10.60$   
 $\phi_i = 60.0$   
 $\phi_f = 180.0$



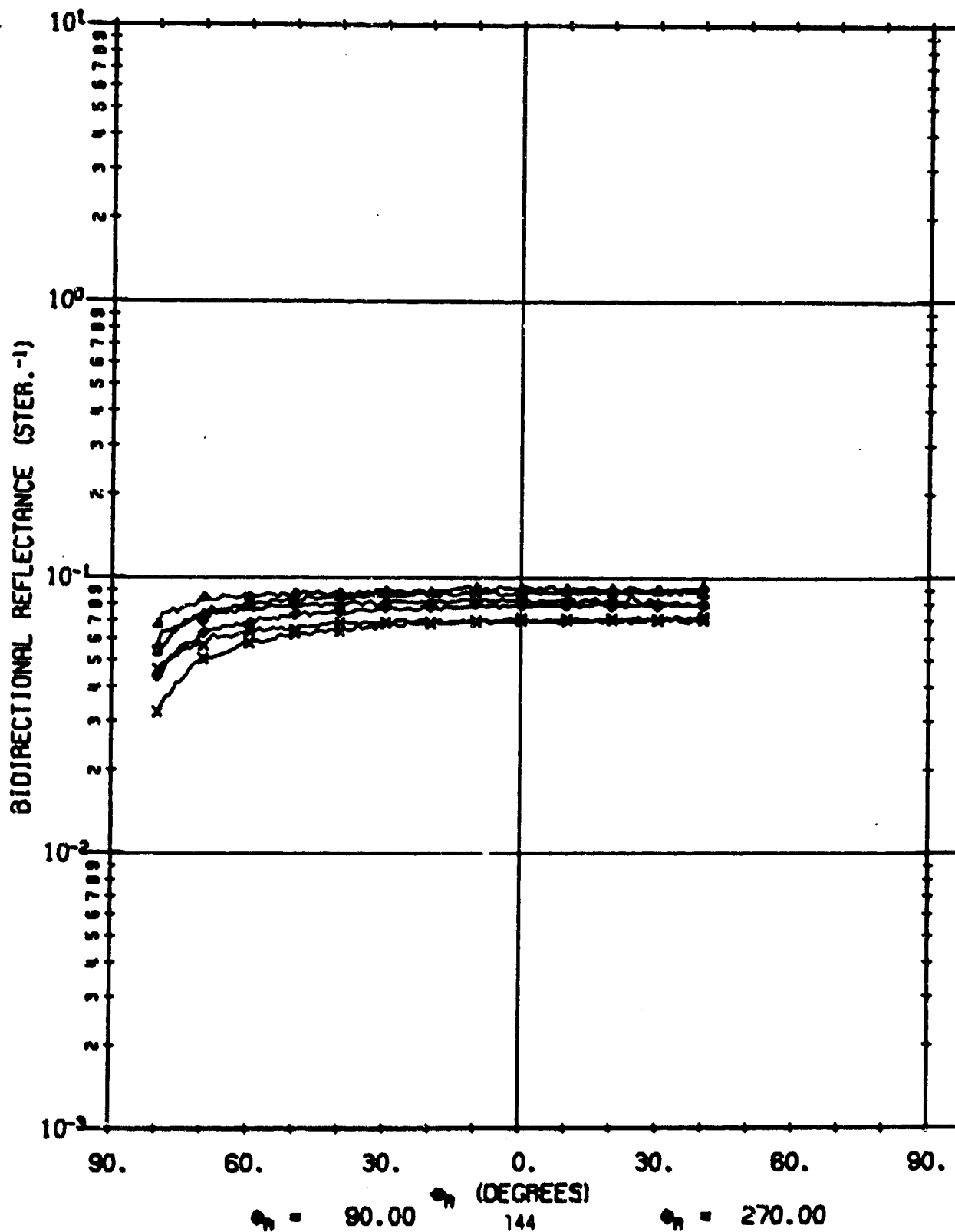
A01610 101

$\lambda = .63$   
 $\phi_1 = 60.0$   
 $\phi_2 = 180.0$



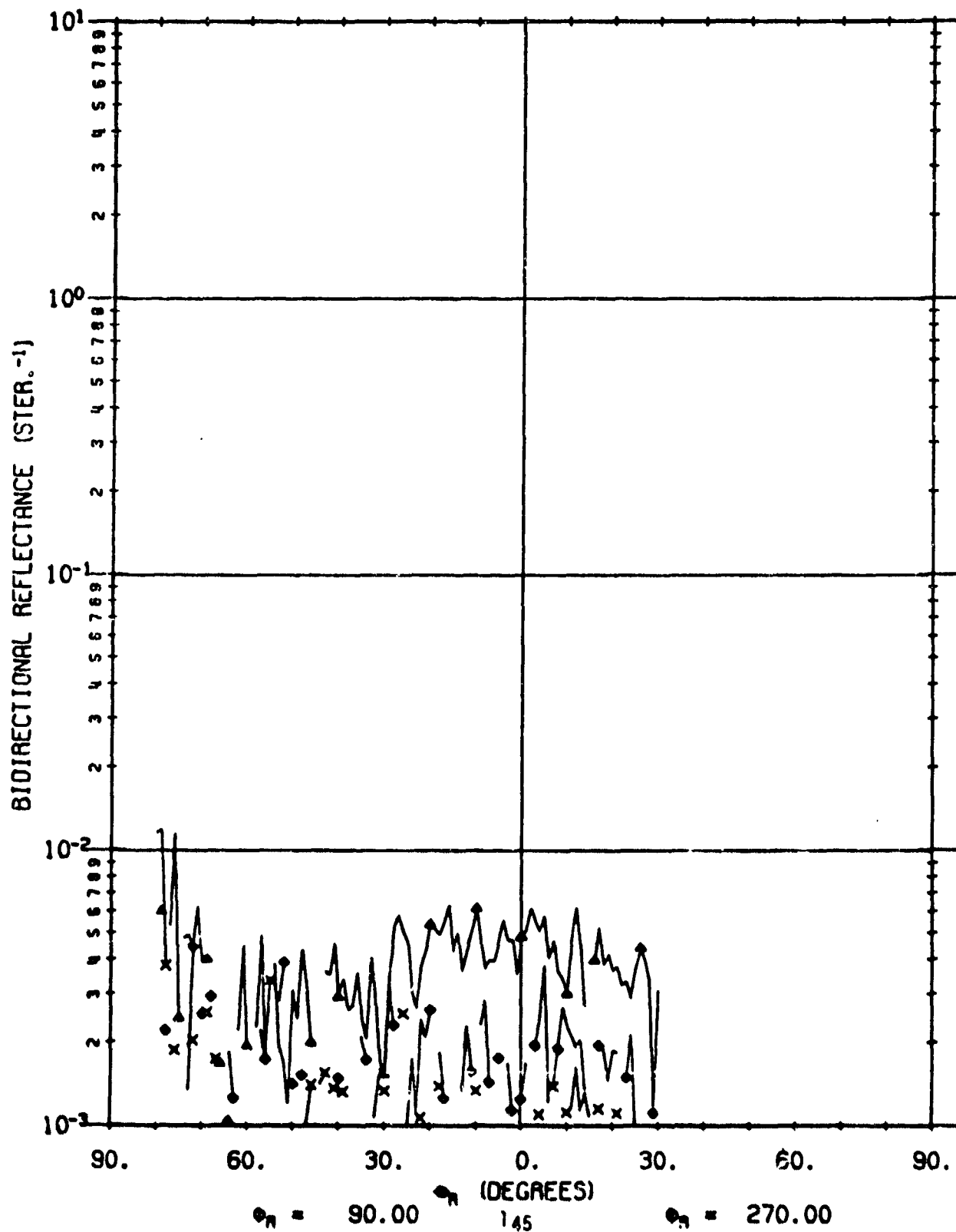
A01610 102

$\lambda = 1.06$   
 $\phi_i = 60.0$   
 $\phi_t = 180.0$



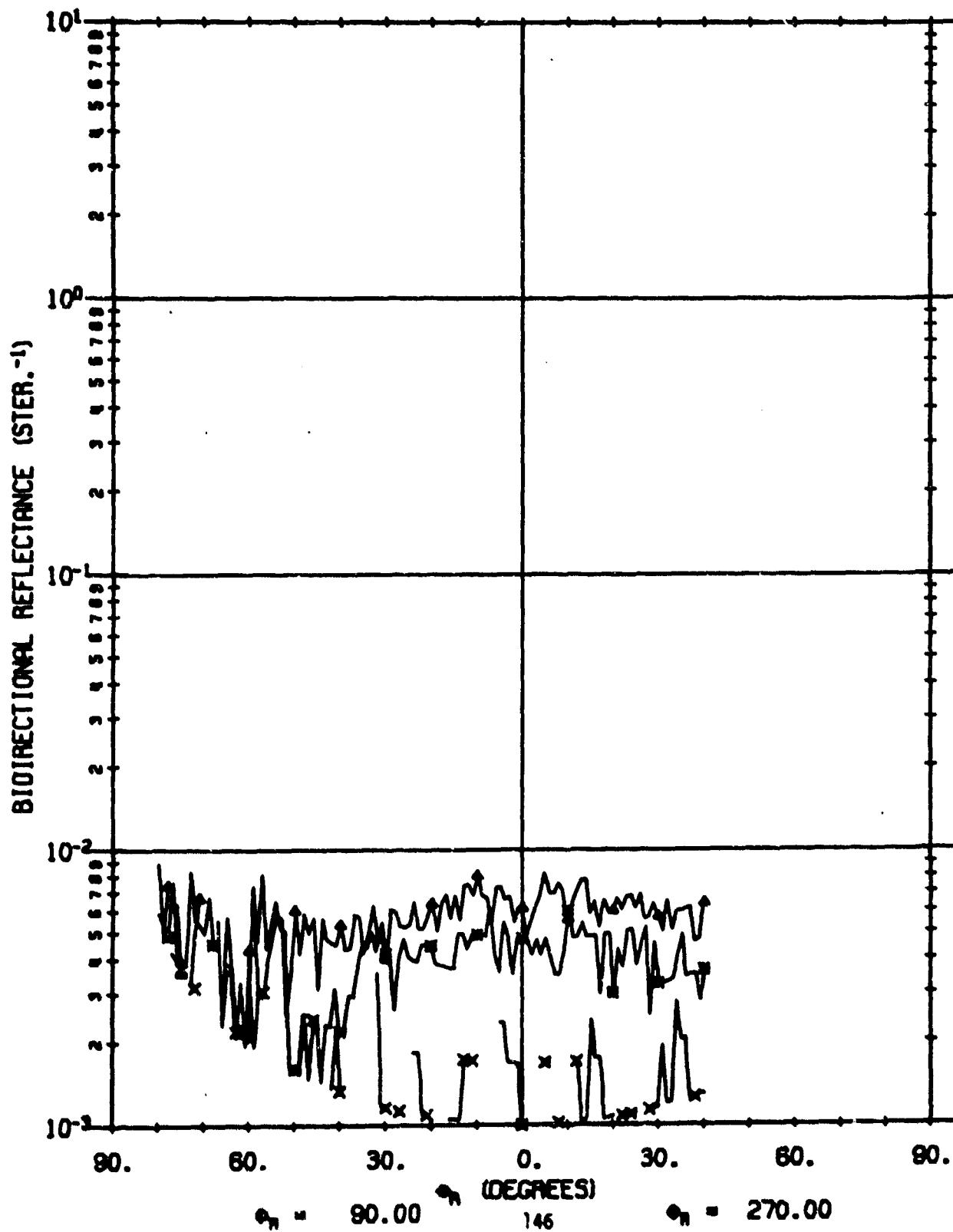
A01610 301

$\lambda = 3.39$   
 $\phi_i = 60.0$   
 $\phi_f = 180.0$



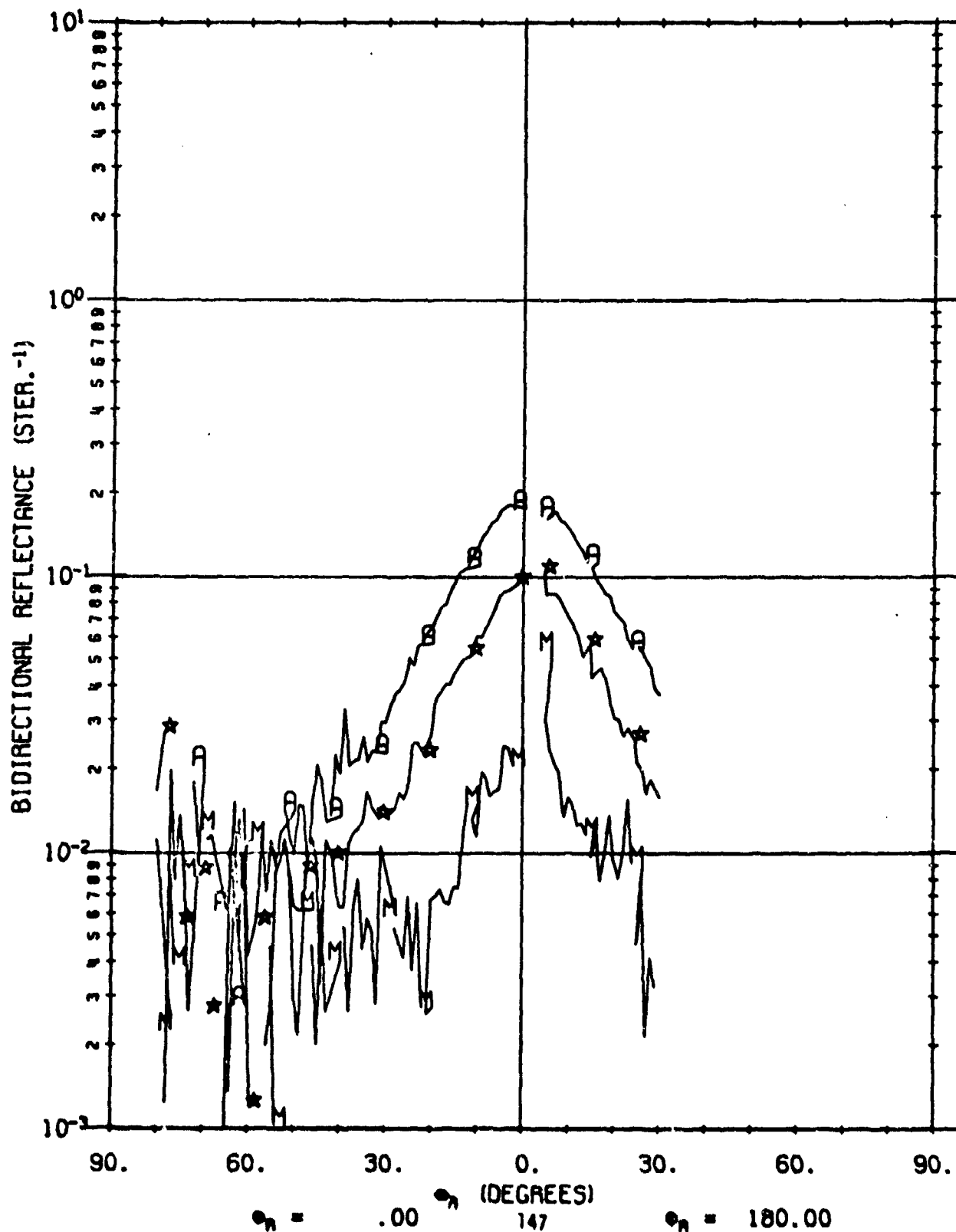
A01610 201

$\lambda = 10.60$   
 $\phi_i = 60.0$   
 $\phi_i = 180.0$



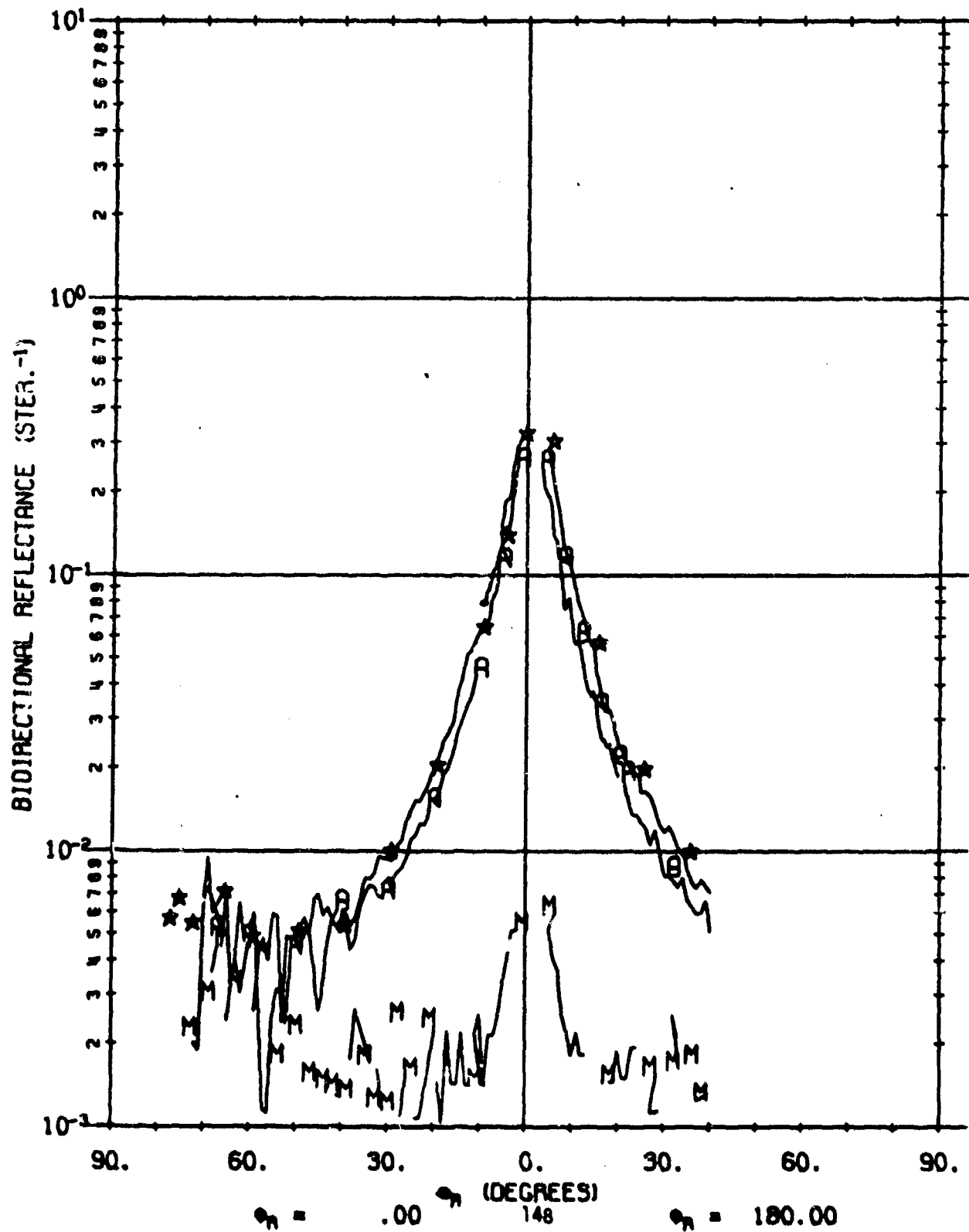
A01610 303

$\lambda = 3.39$   
 $\phi_i = .0$   
 $\phi_f = 180.0$



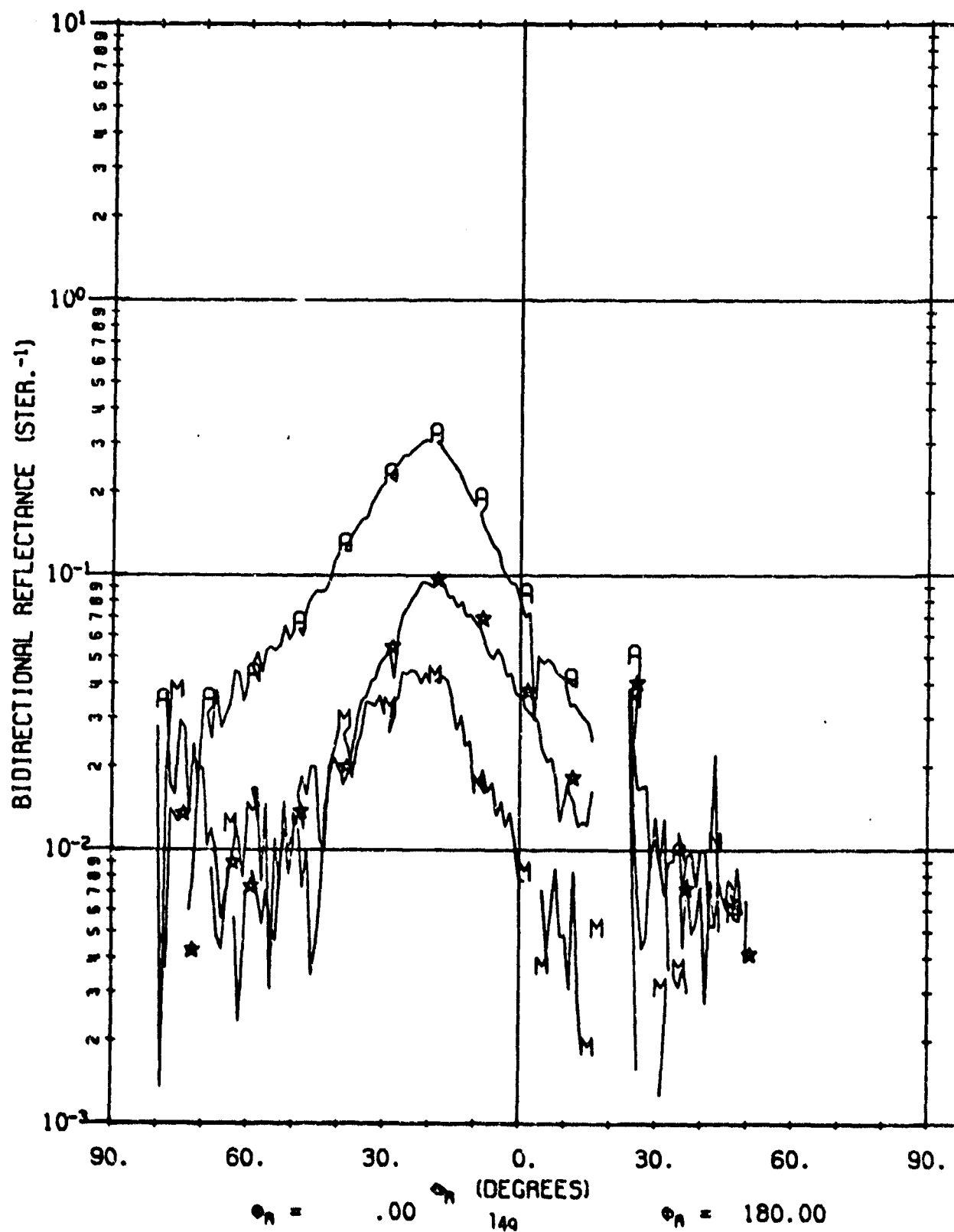
A01610 203

$\lambda = 10.60$   
 $\phi_i = 0.0$   
 $\phi_f = 180.0$



A01610 303

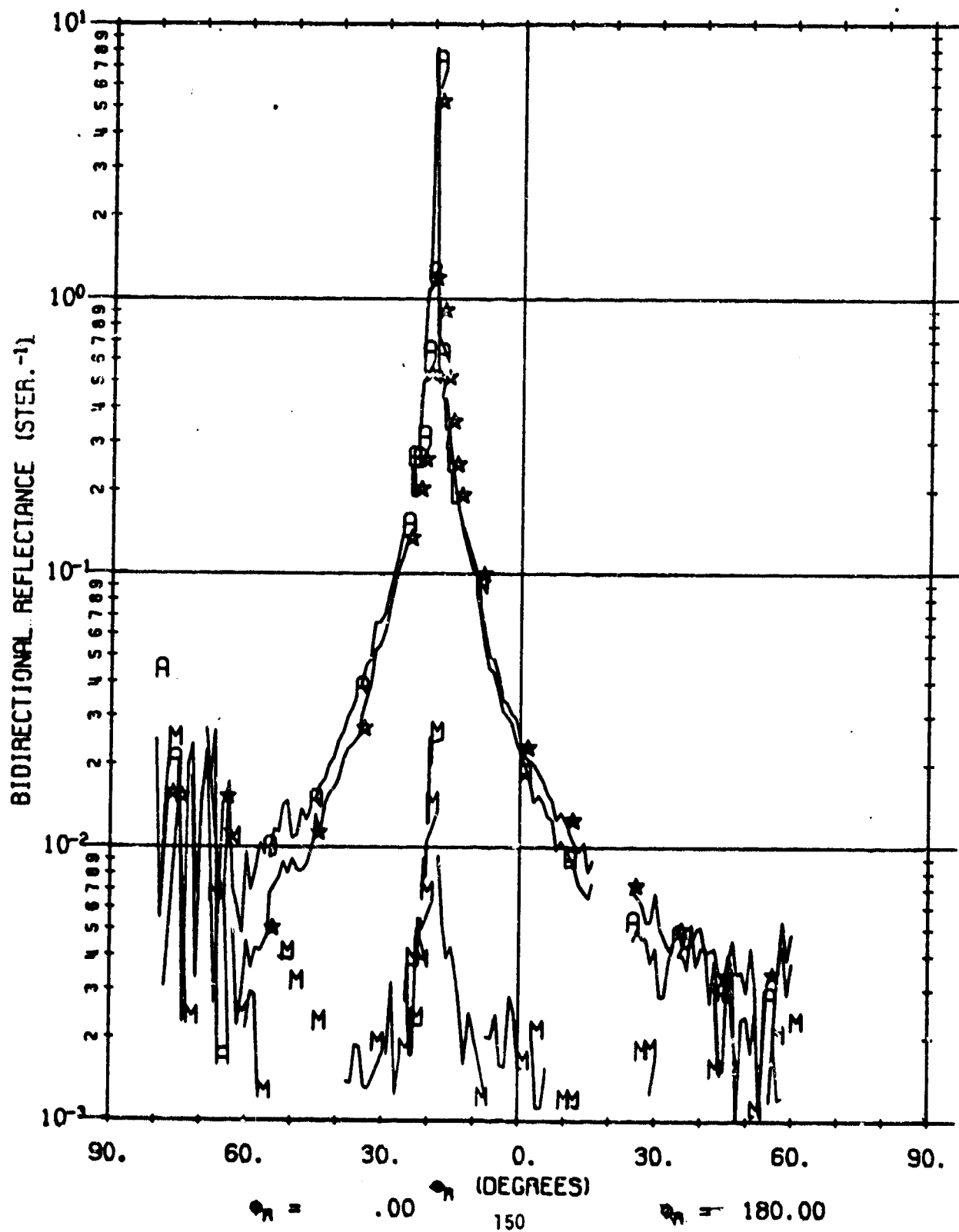
$\lambda = 3.39$   
 $\phi_i = 20.0$   
 $\phi_i = 180.0$





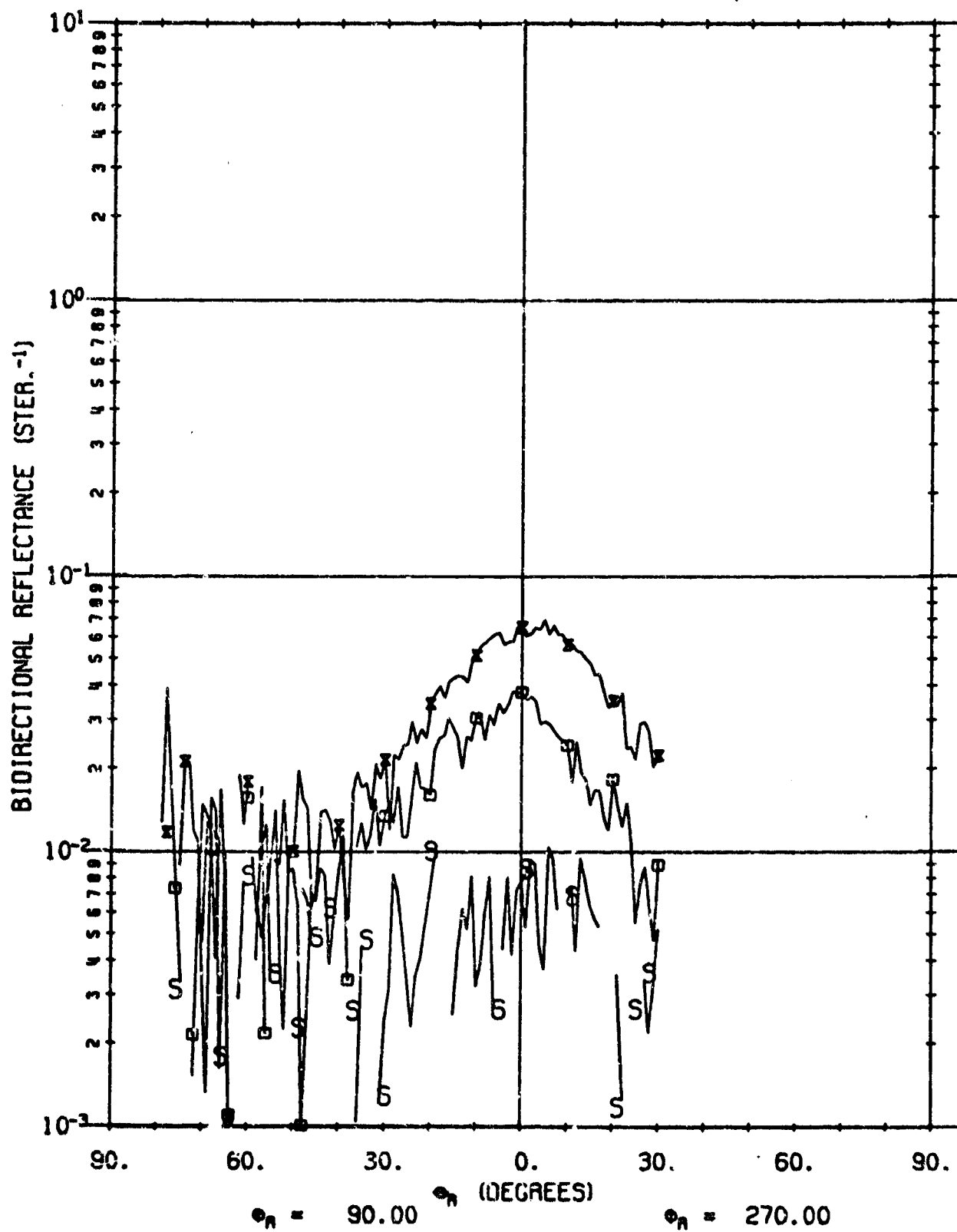
A01610 203

$\lambda = 10.60$   
 $\phi_i = 20.0$   
 $\phi_j = 180.0$



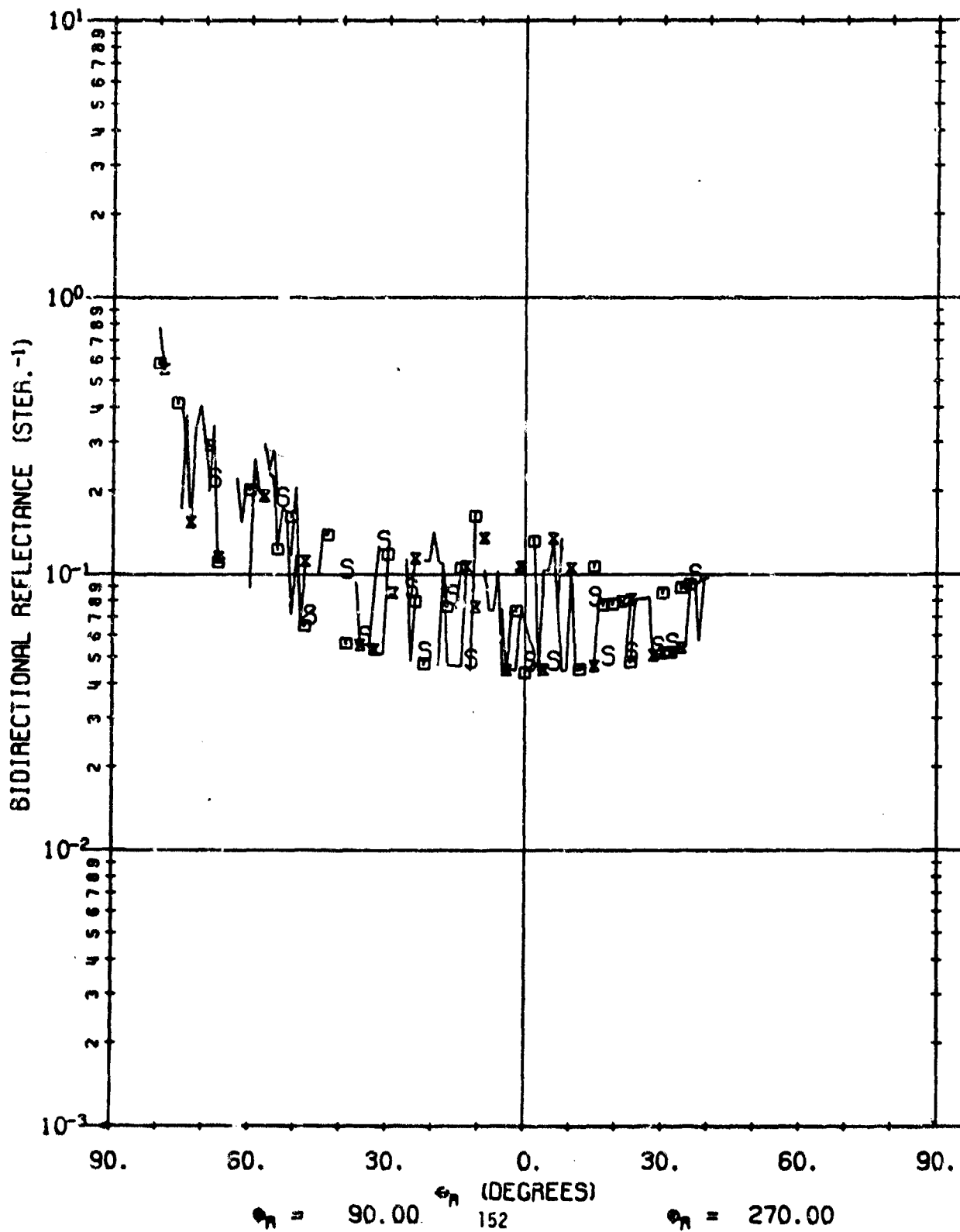
A01610 303

$\lambda = 3.39$   
 $\phi_1 = 20.0$   
 $\phi_2 = 180.0$



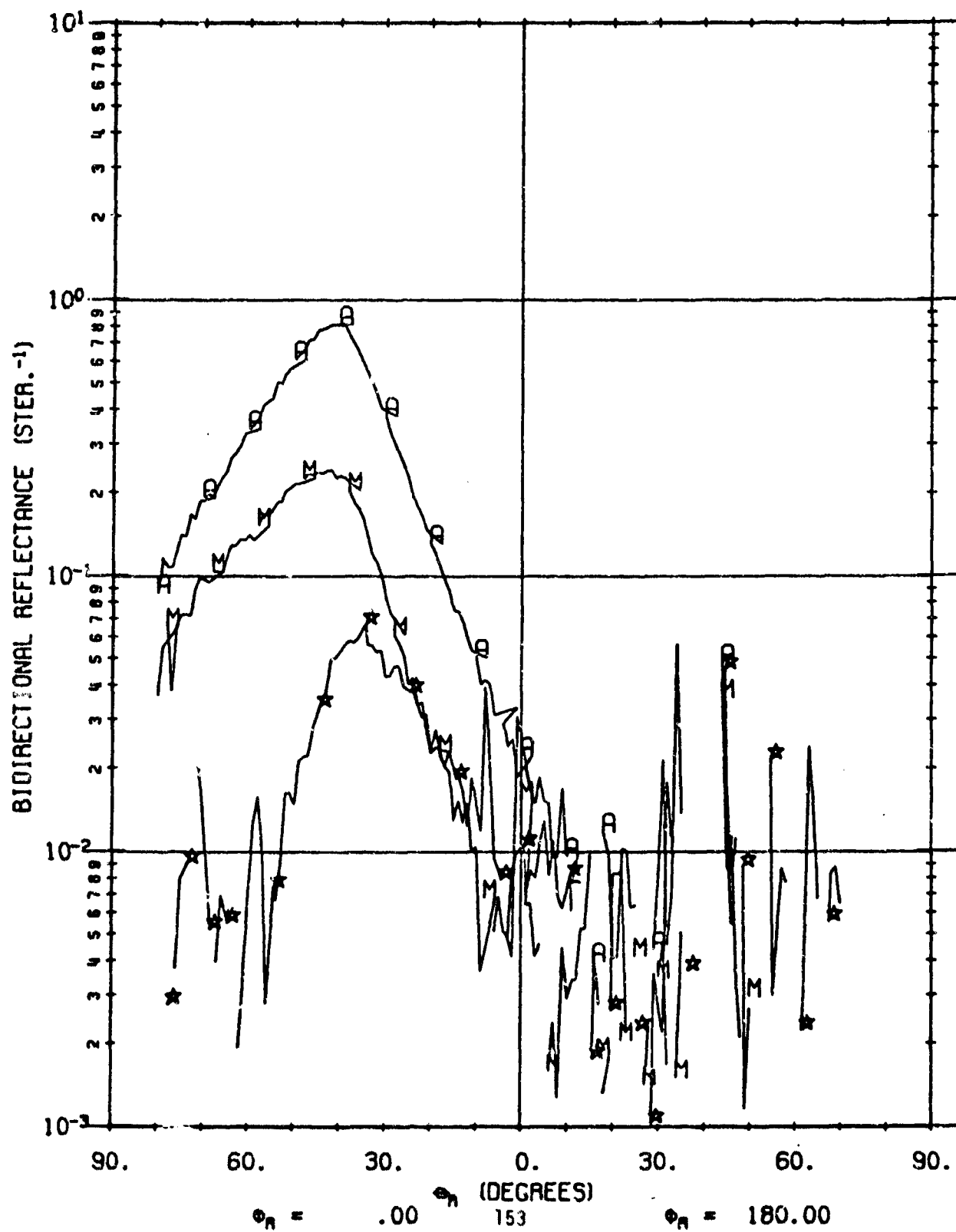
A01610 203

$\lambda = 10.60$   
 $\phi_i = 20.0$   
 $\phi_f = 160.0$



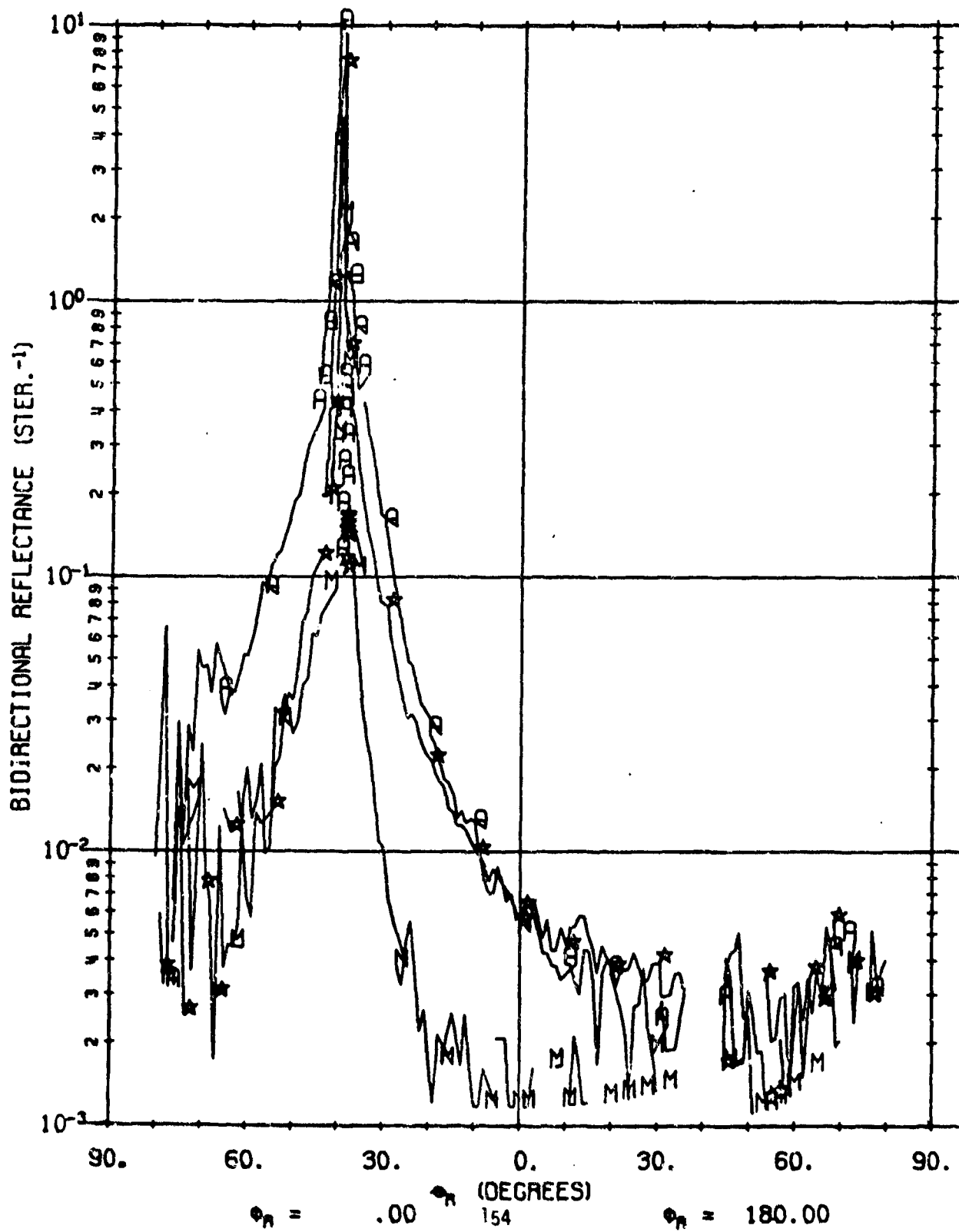
A01610 303

$\lambda = 3.39$   
 $\phi_i = 40.0$   
 $\phi_f = 180.0$



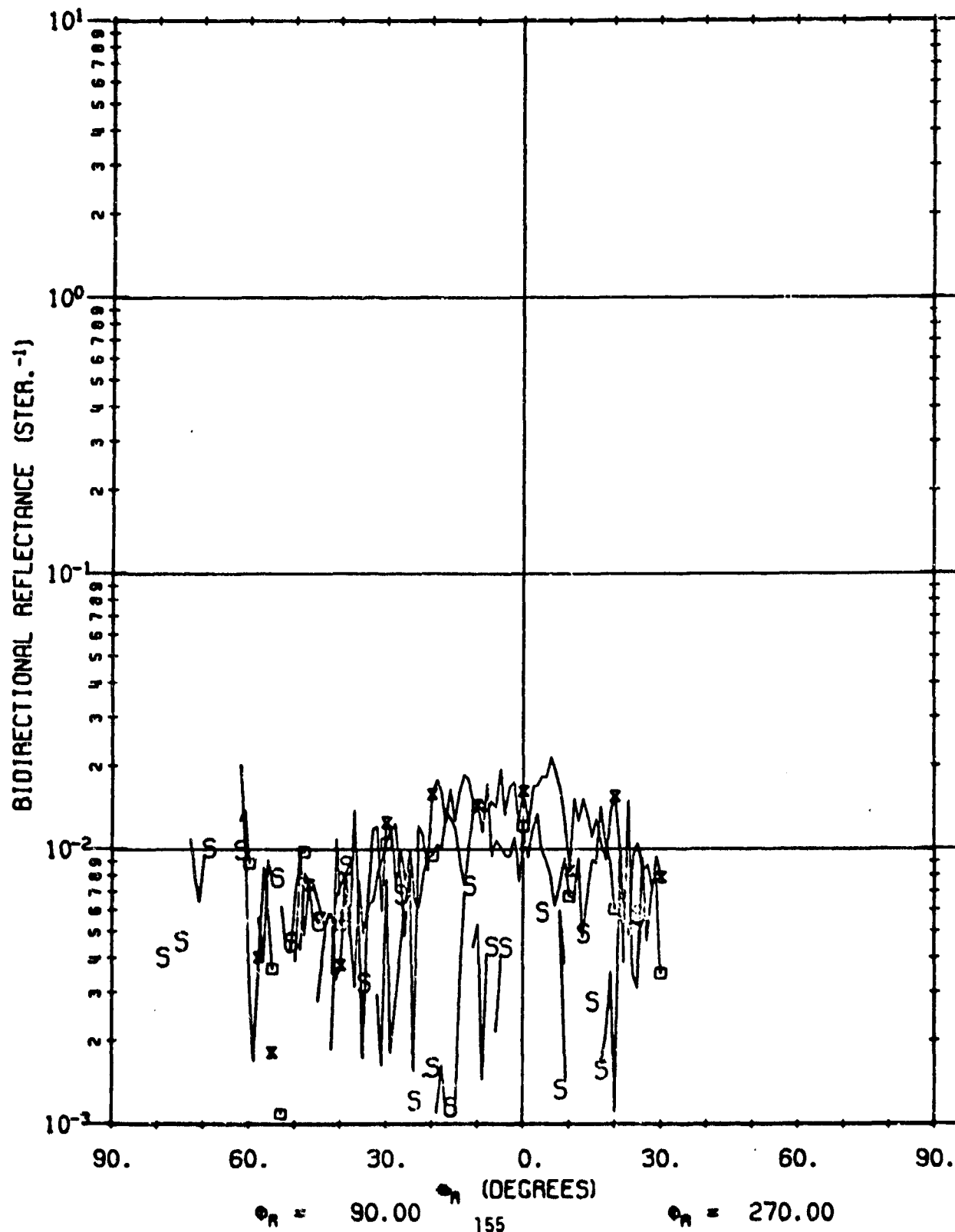
R01610 203

$\lambda = 10.60$   
 $\phi_1 = 40.0$   
 $\phi_2 = 180.0$



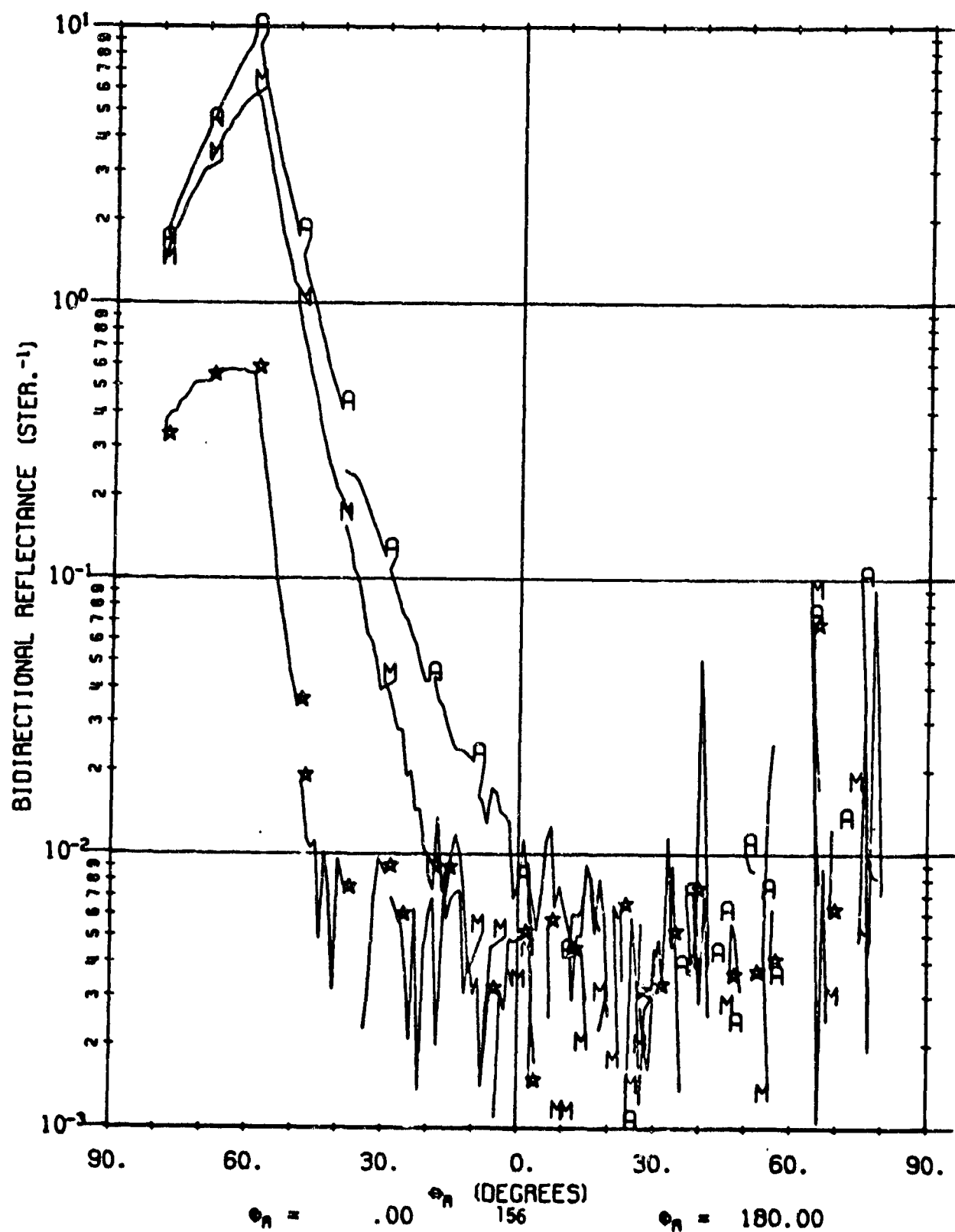
A01610 303

$\lambda = 3.39$   
 $\phi_1 = 40.0$   
 $\phi_i = 180.0$



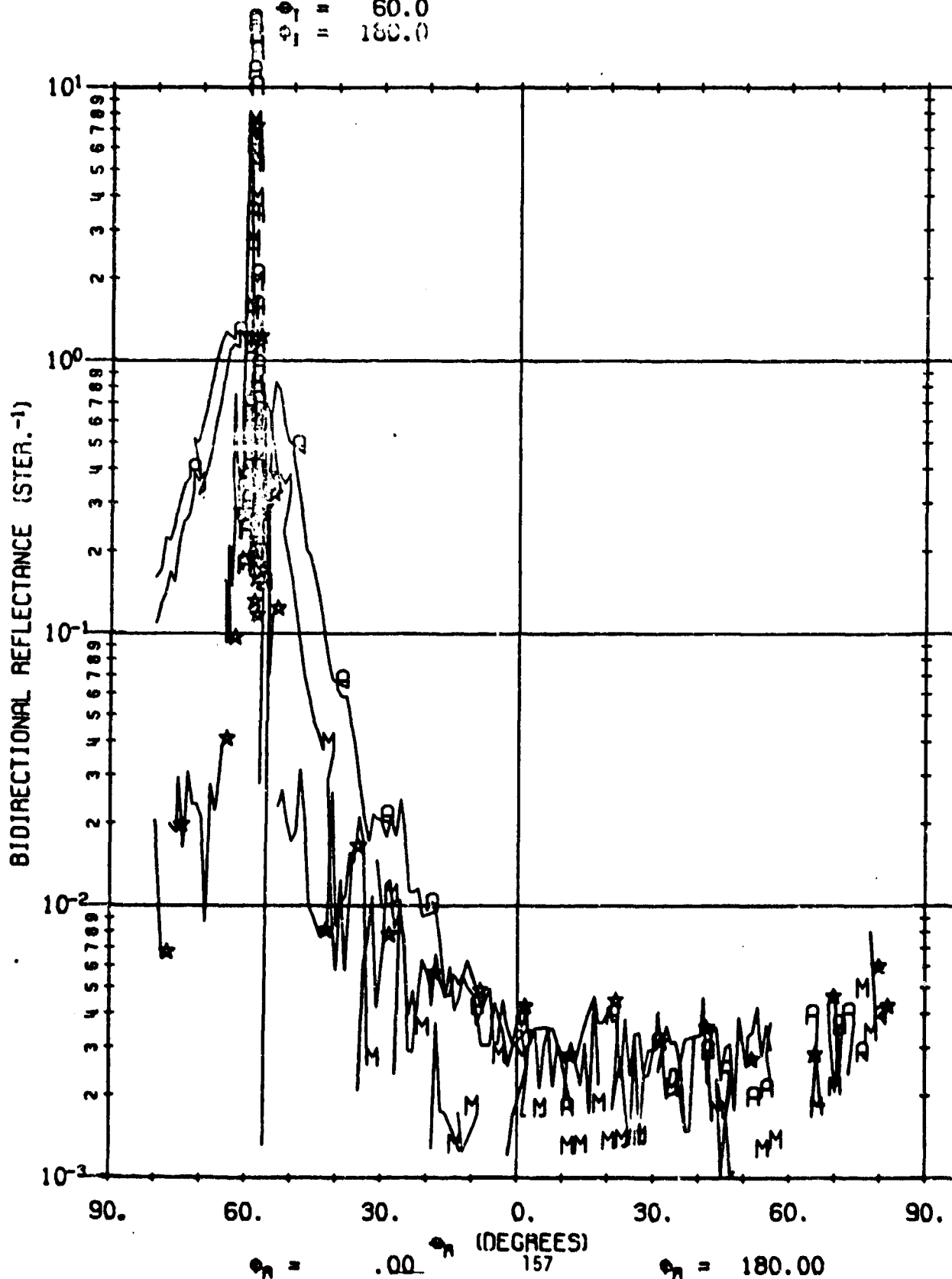
A01610 303

$\lambda = 3.39$   
 $\phi_i = 60.0$   
 $\phi_i = 180.0$



A01610 203

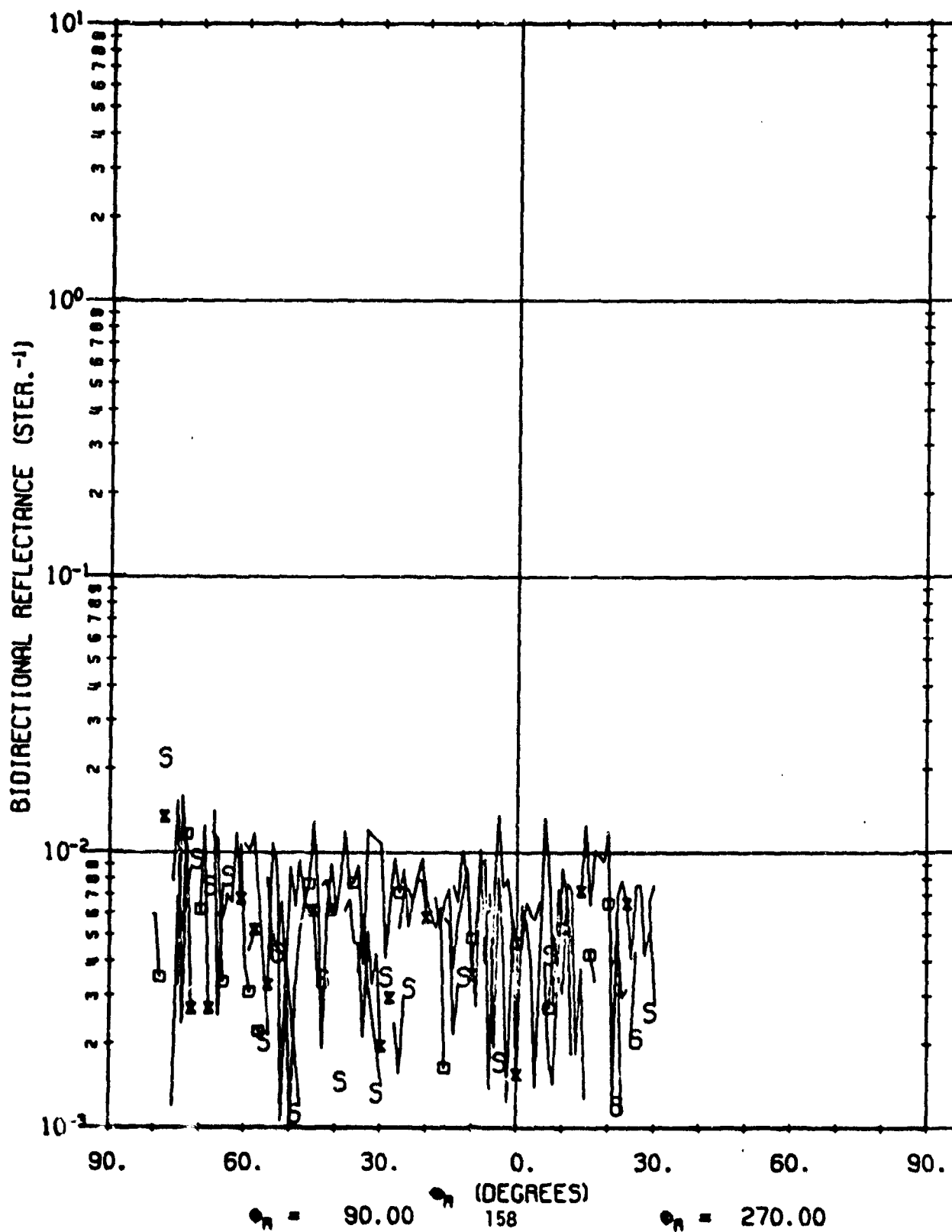
$\lambda = 10.60$   
 $\phi_i = 60.0$   
 $\phi_i = 180.0$





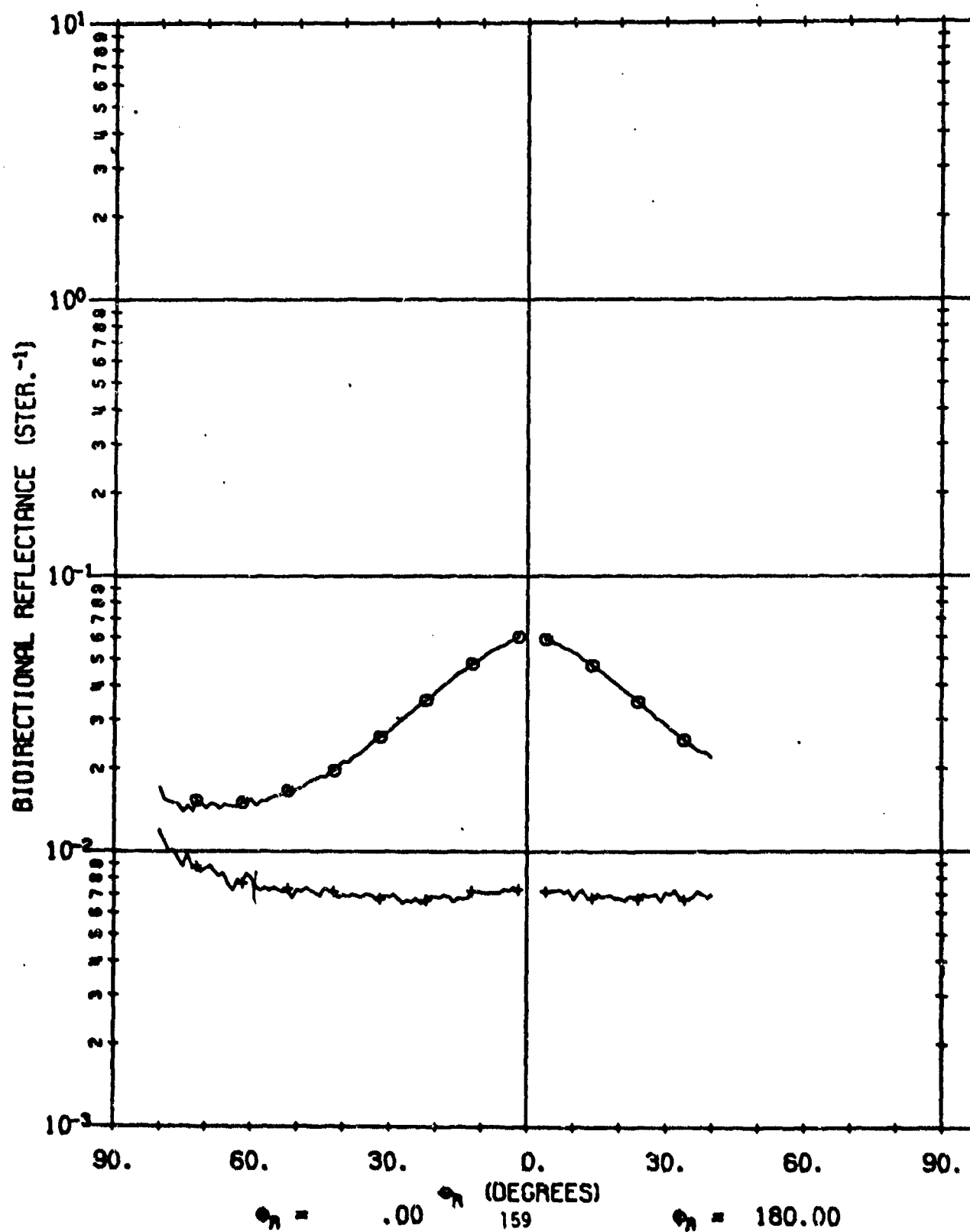
A01610 303

$\lambda = 3.39$   
 $\phi_1 = 60.0$   
 $\phi_2 = 180.0$



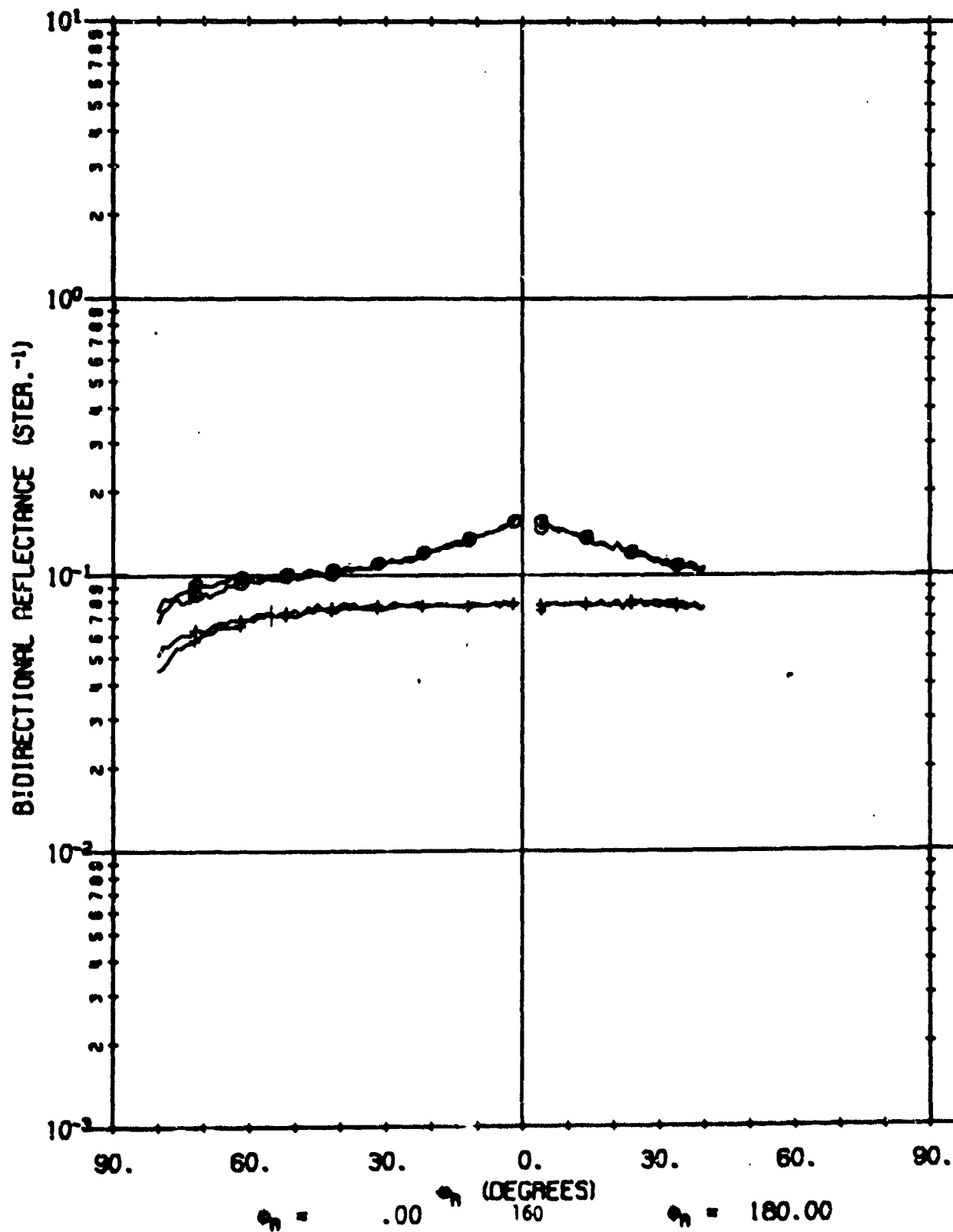
A01610 101

$\lambda = .63$   
 $\phi_j = .0$   
 $\phi_j = 180.0$



A01610 102

$\lambda = 1.06$   
 $\phi_1 = 0.0$   
 $\phi_2 = 180.0$

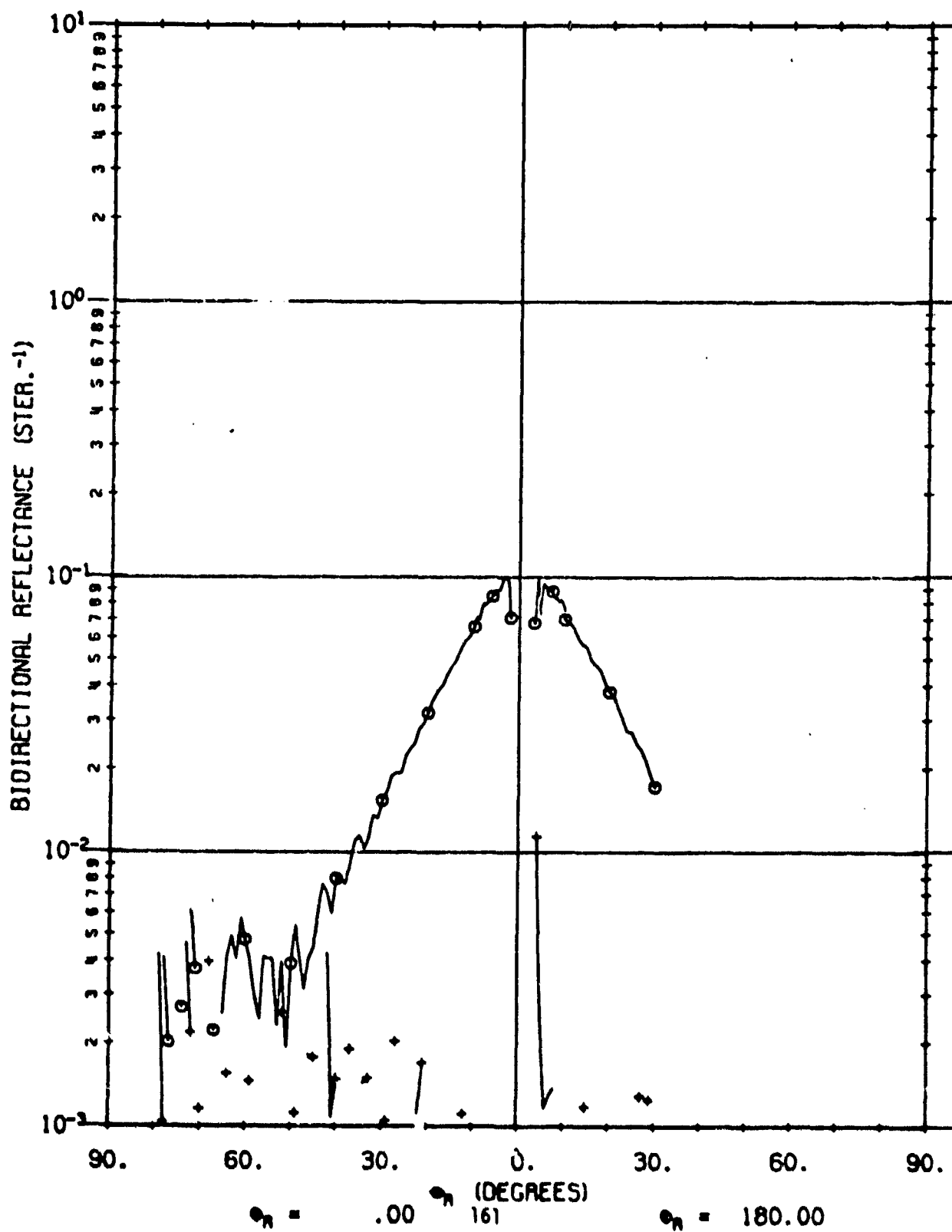


A01610

301

$$\lambda = 3.39$$

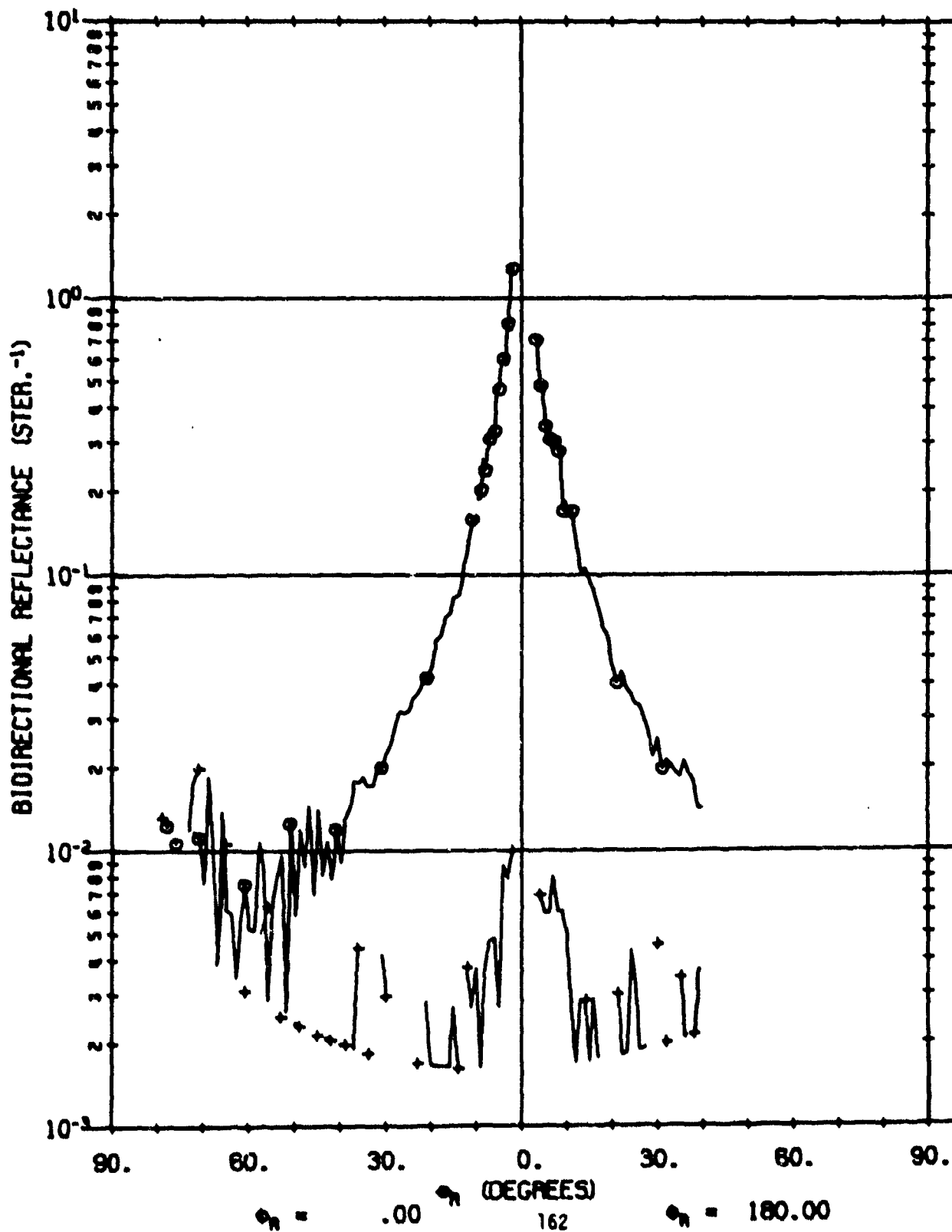
9 = .0

$$\phi_1 = 180.0$$


A01610 204

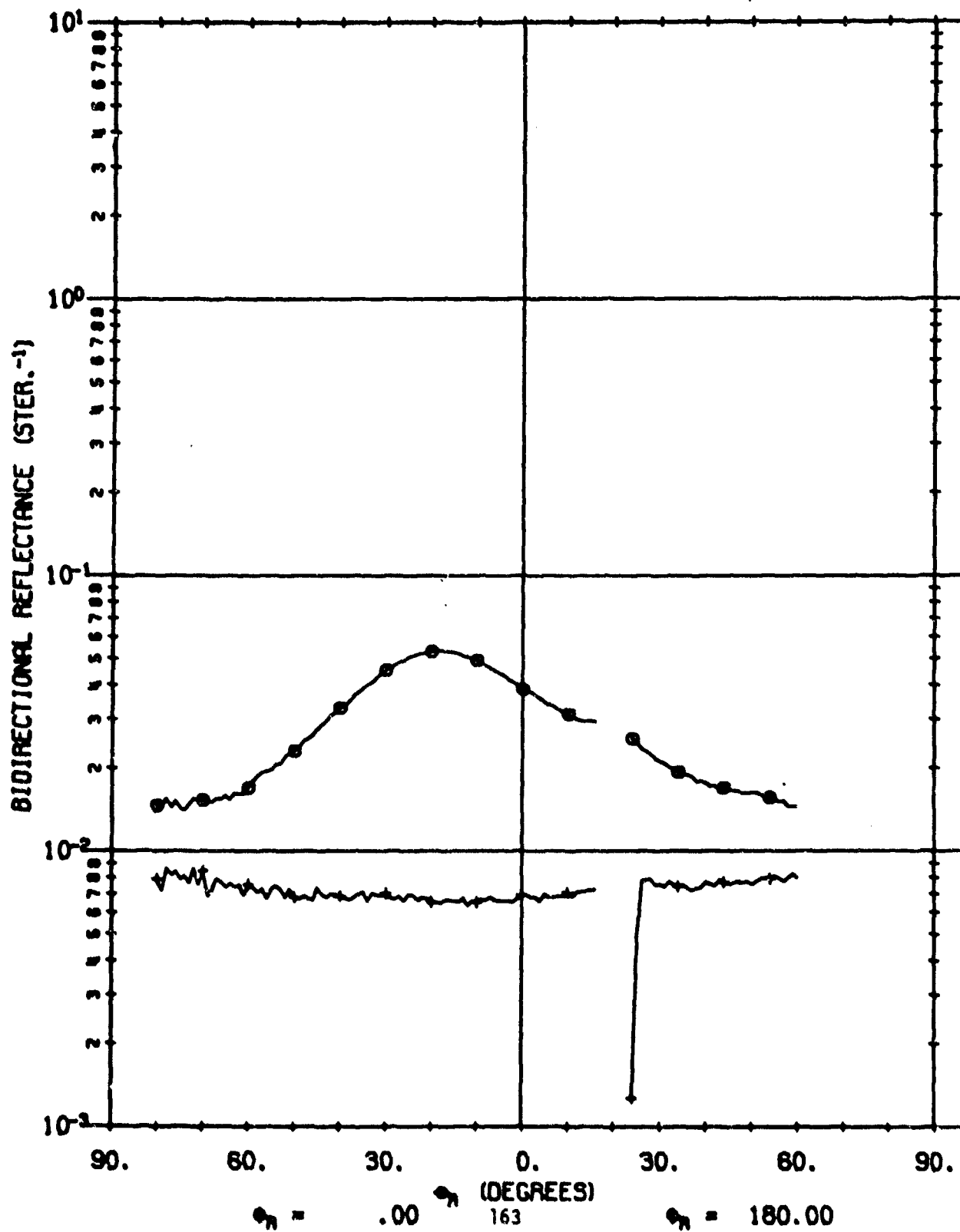
$\lambda = 10.60$

$\phi_i = 180.0$



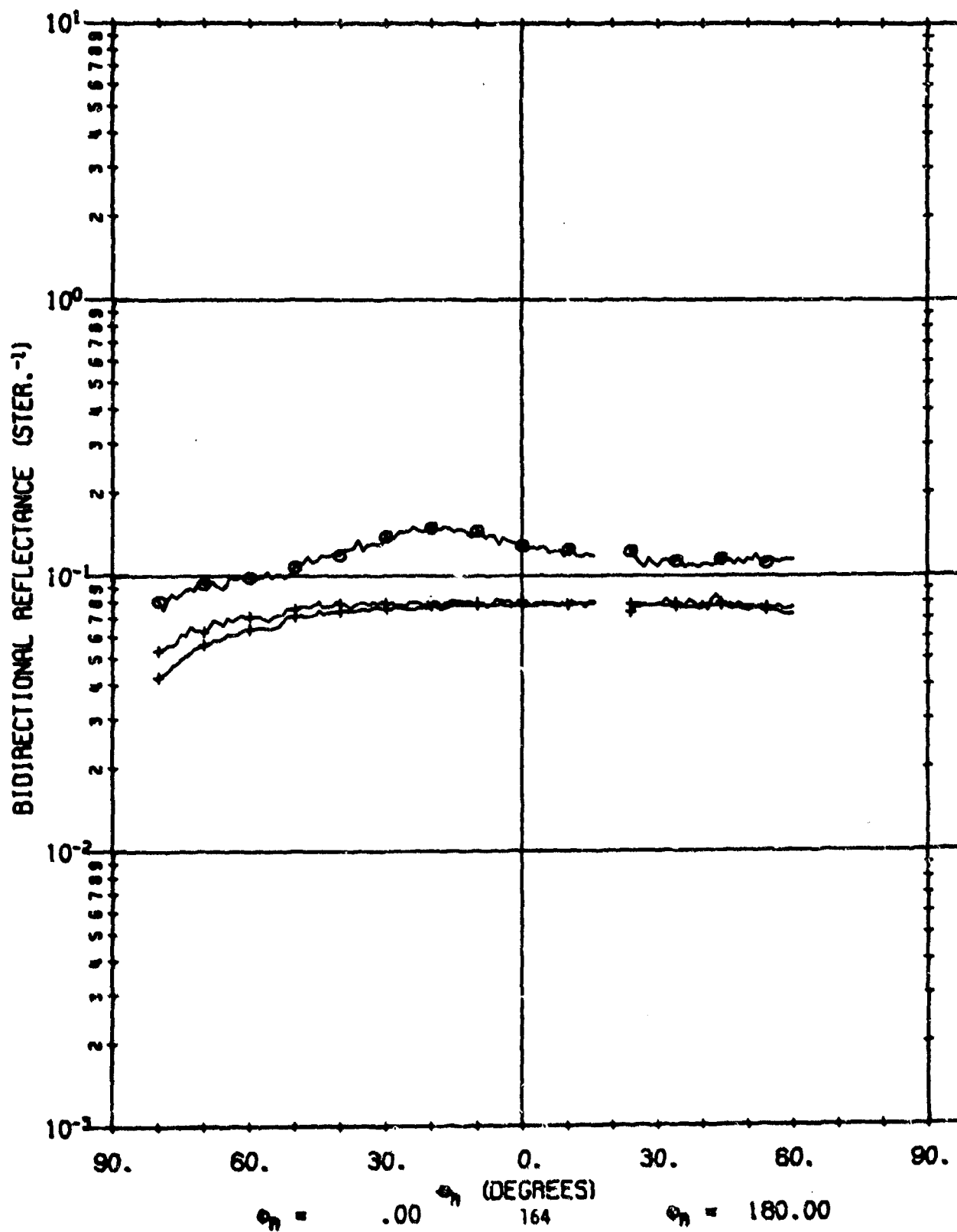
A01610 101

$\lambda = .63$   
 $\theta_1 = 20.0$   
 $\theta_2 = 180.0$



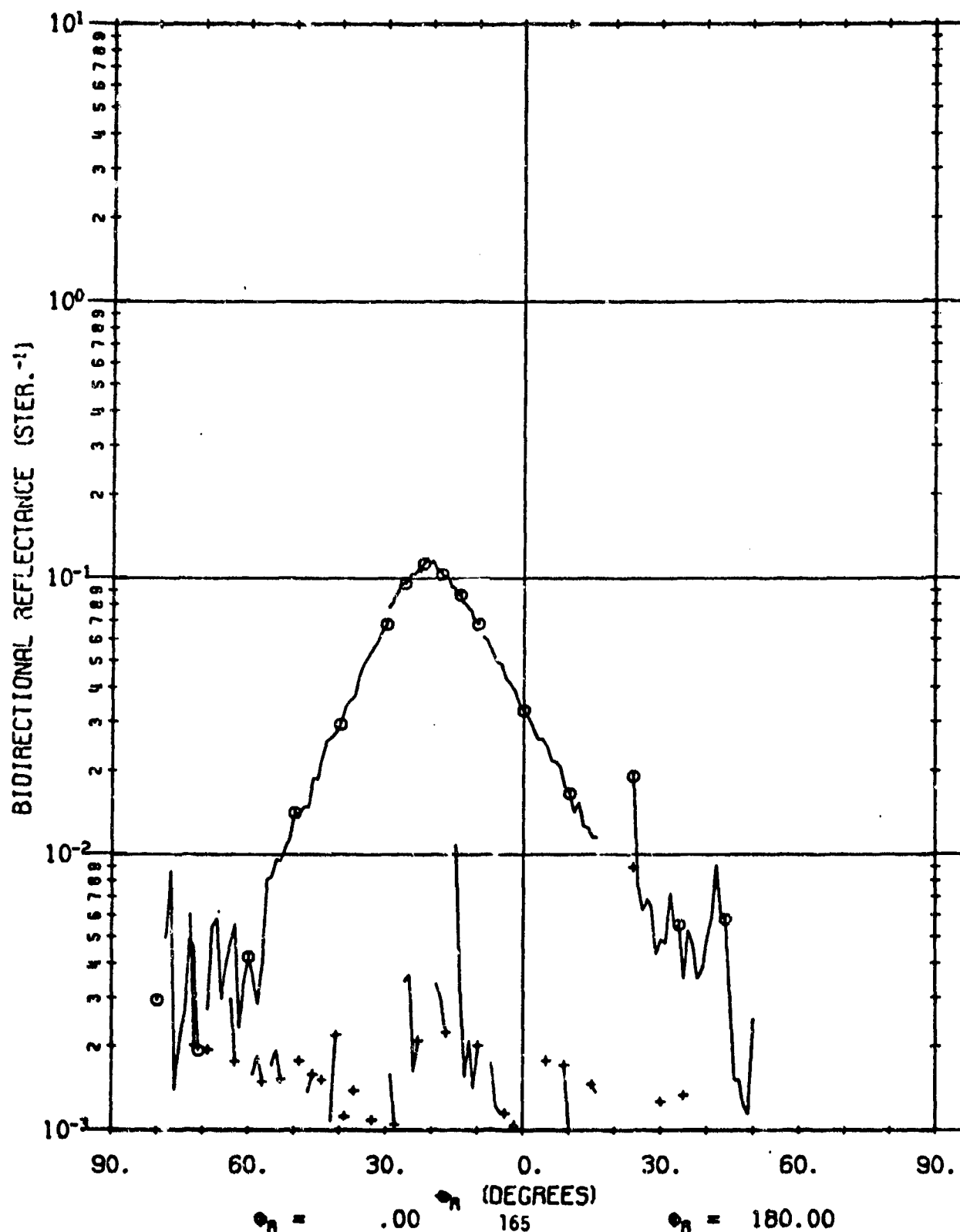
R01610 102

$\lambda = 1.06$   
 $\phi_i = 20.0$   
 $\phi_t = 180.0$



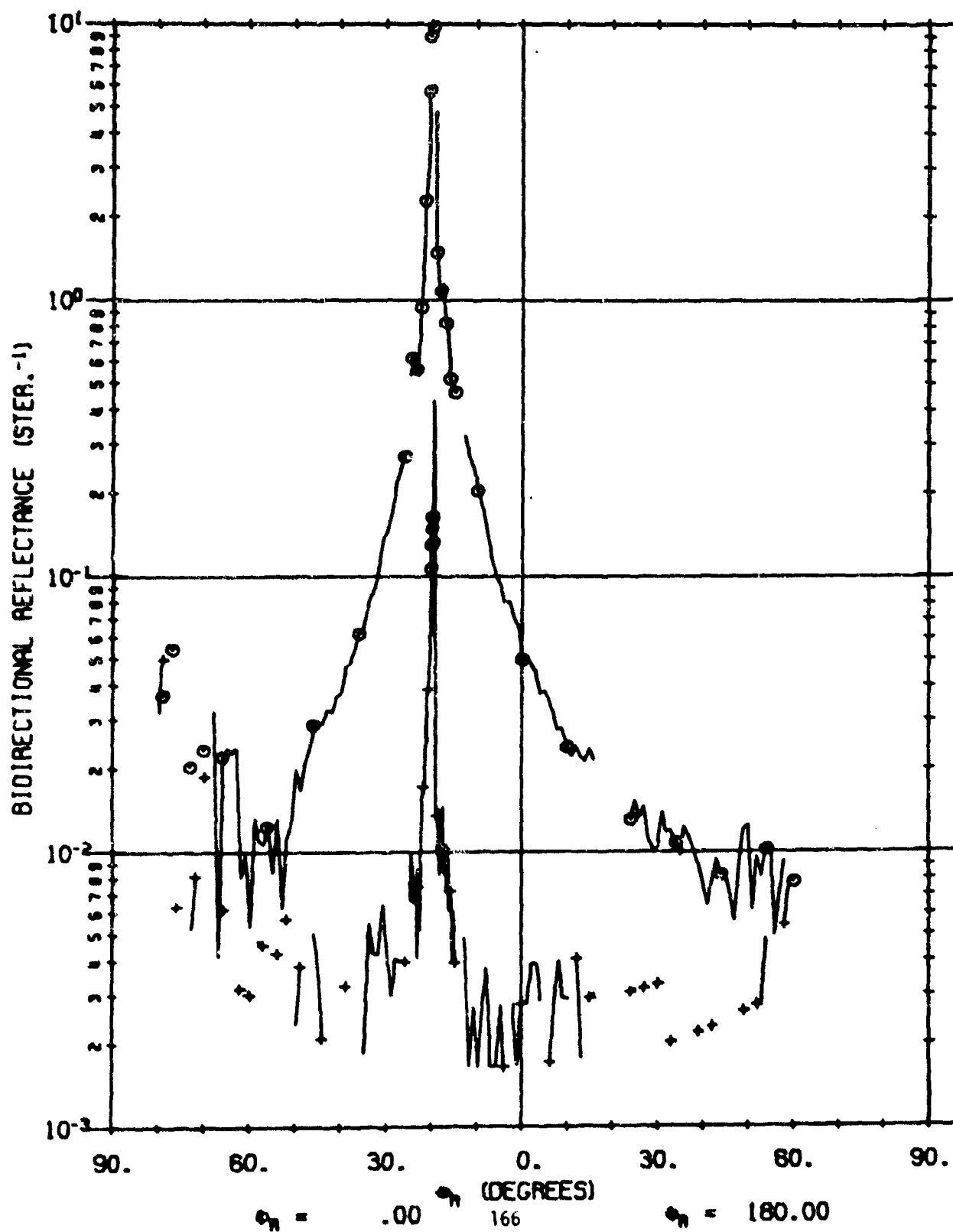
A01610 301

$\lambda = 3.39$   
 $\phi_1 = 20.0$   
 $\phi_2 = 180.0$



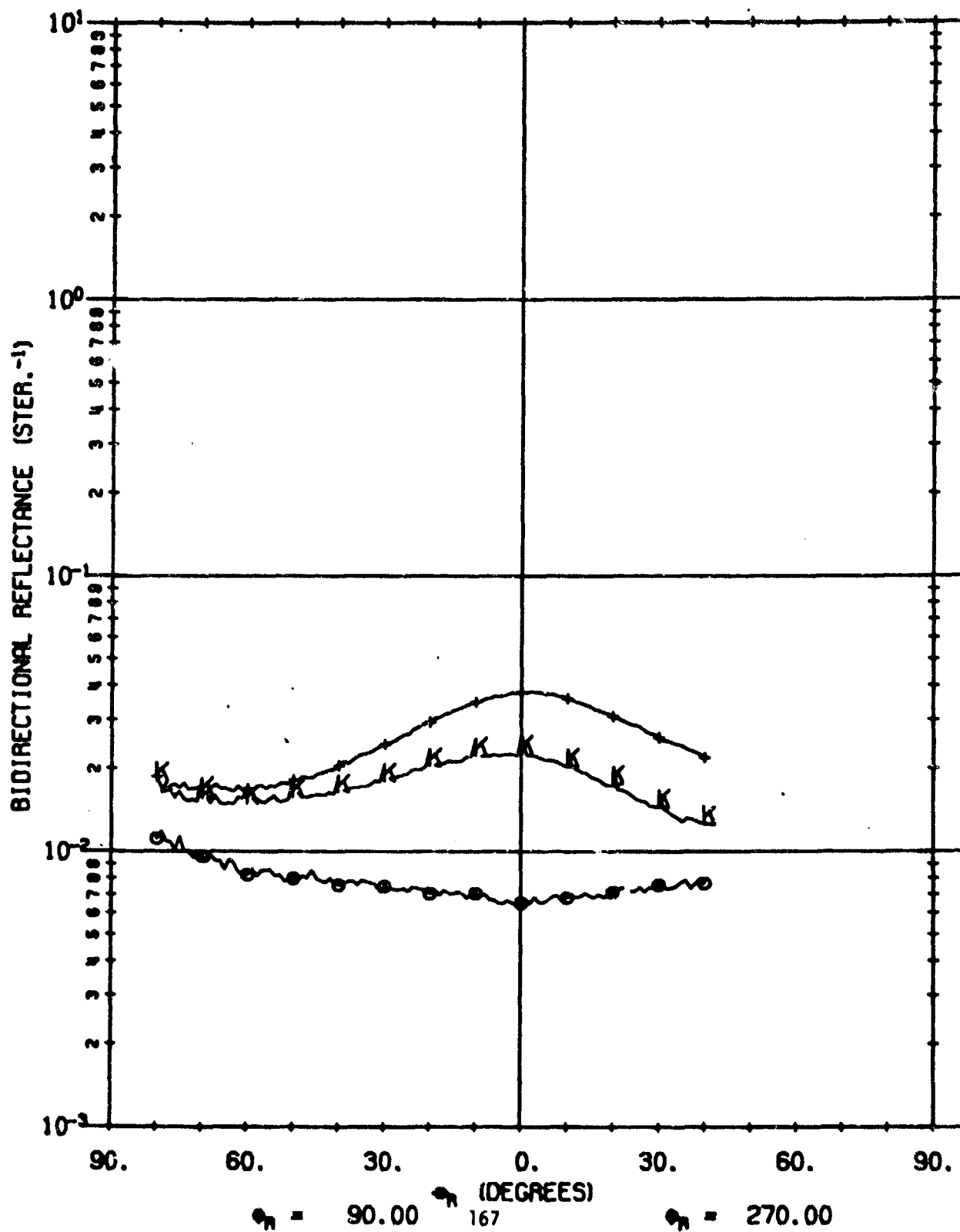


$\lambda = 10.60$   
 $\phi_I = 20.0$   
 $\phi_I = 180.0$



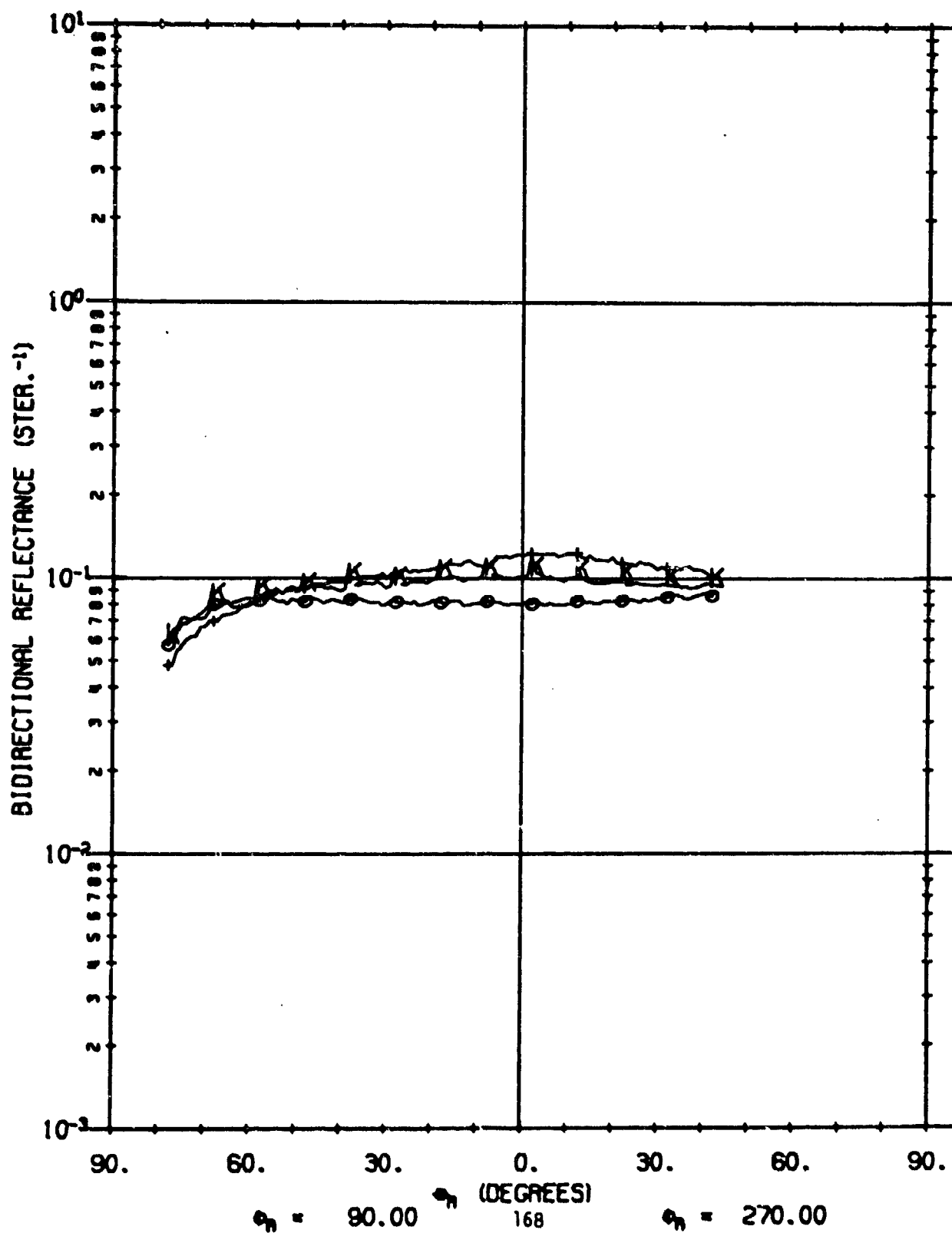
A01610 101

$\lambda = .63$   
 $\phi_1 = 20.0$   
 $\phi_2 = 180.0$



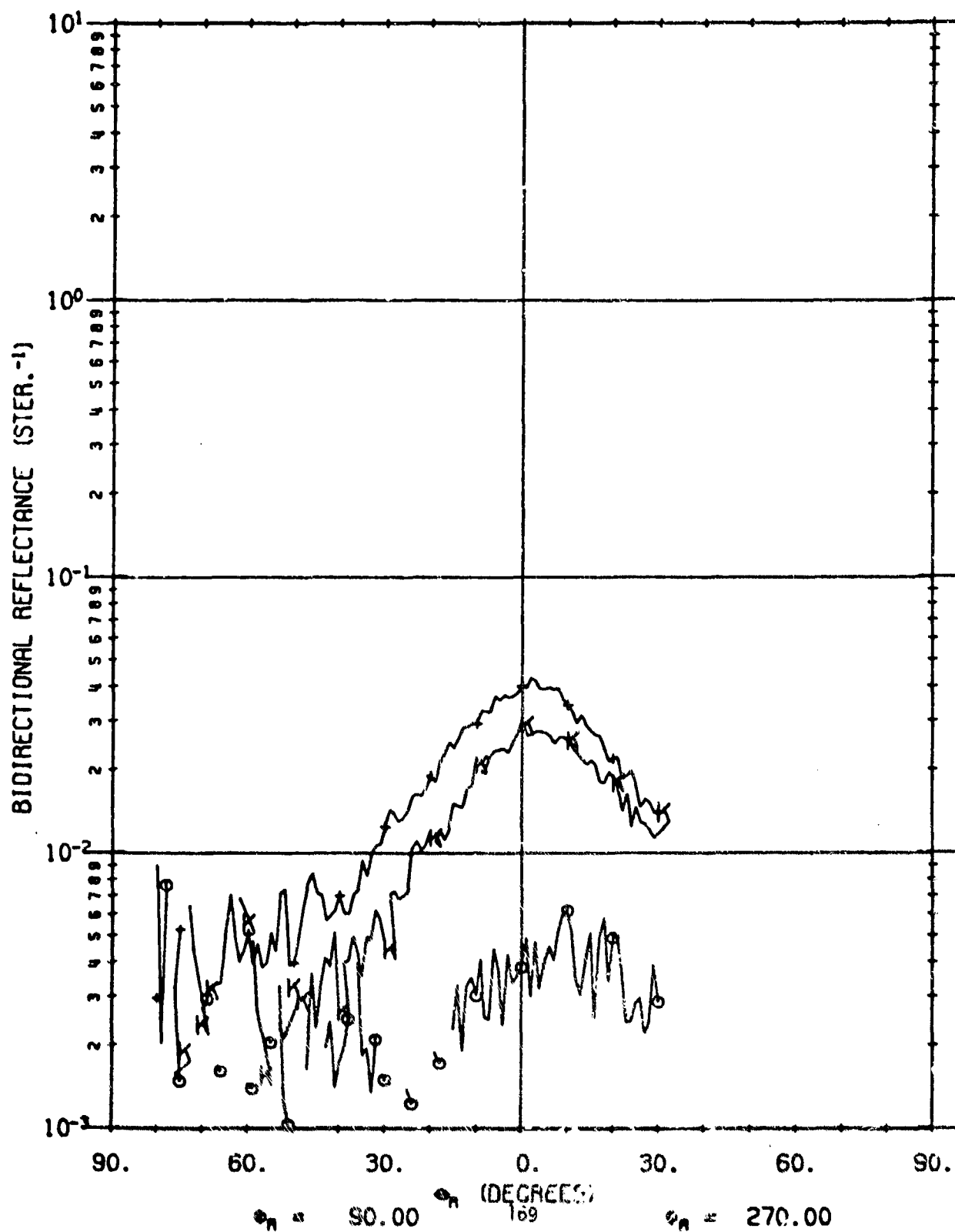
A01610 102

$\lambda = 1.06$   
 $\phi_i = 20.0$   
 $\phi_t = .0$



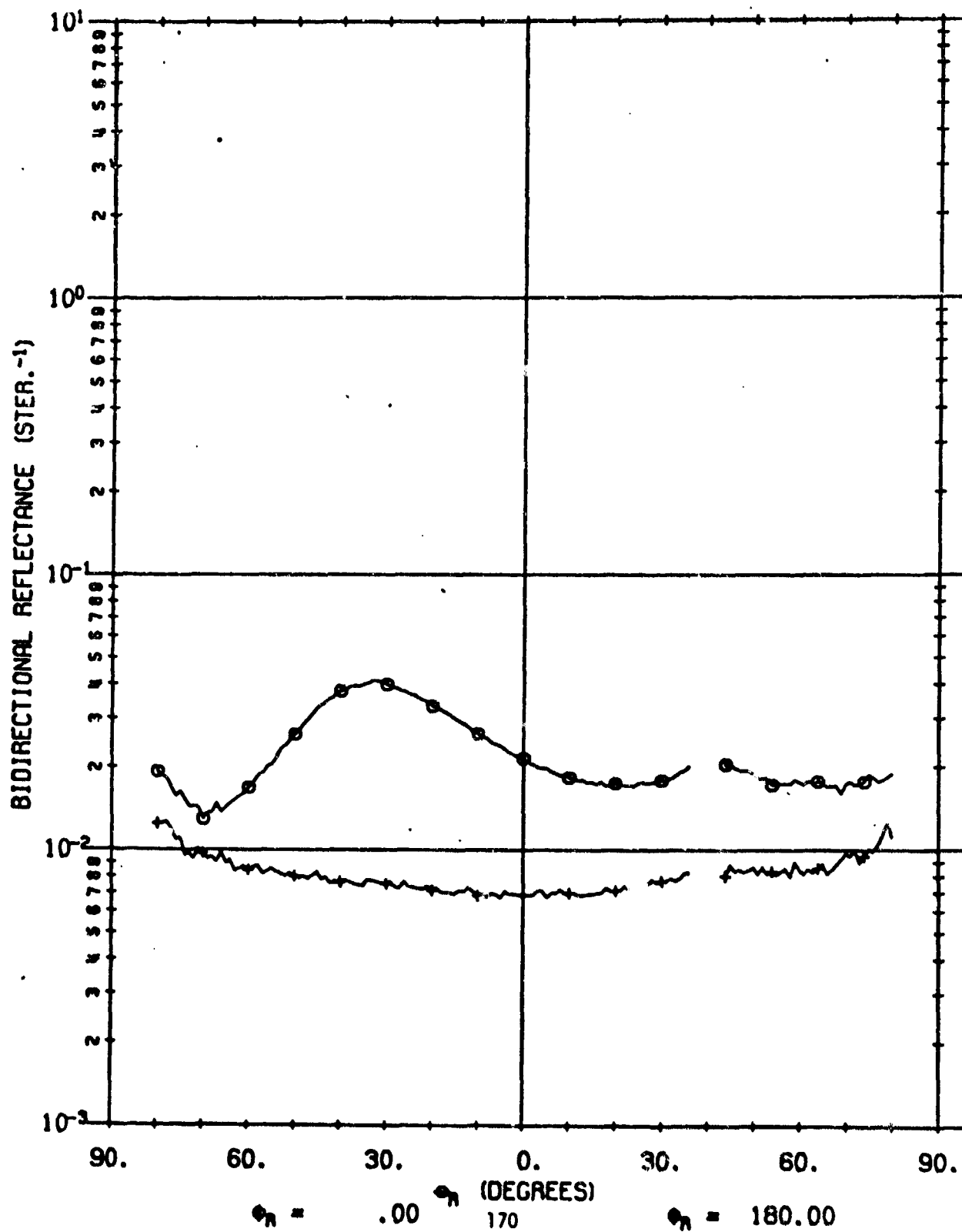
A01610 302

$\lambda = 3.39$   
 $\phi_i = 20.0$   
 $\phi_f = 180.0$



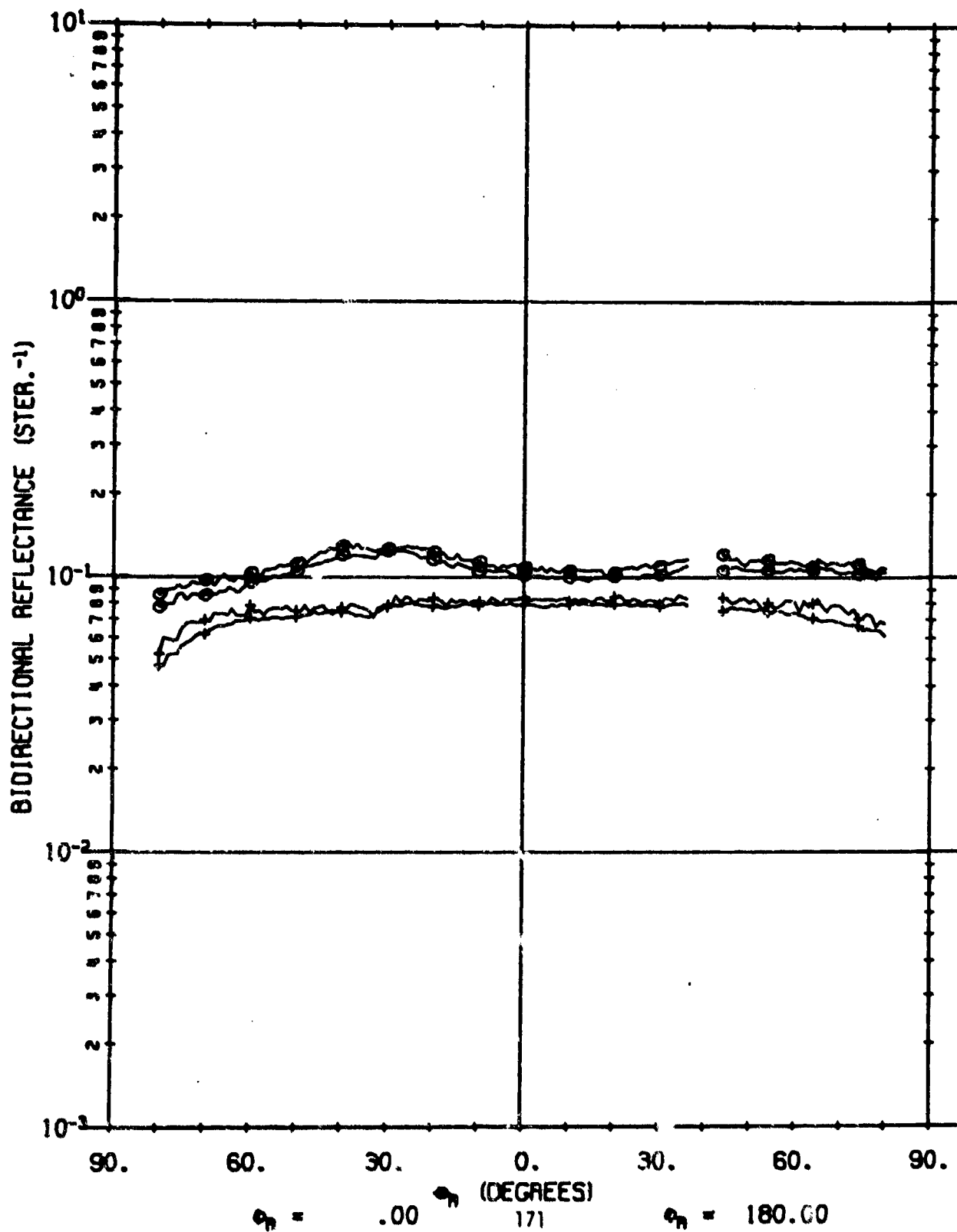
H01610 101

$\lambda = .63$   
 $\phi_i = 40.0$   
 $\phi_j = 180.0$



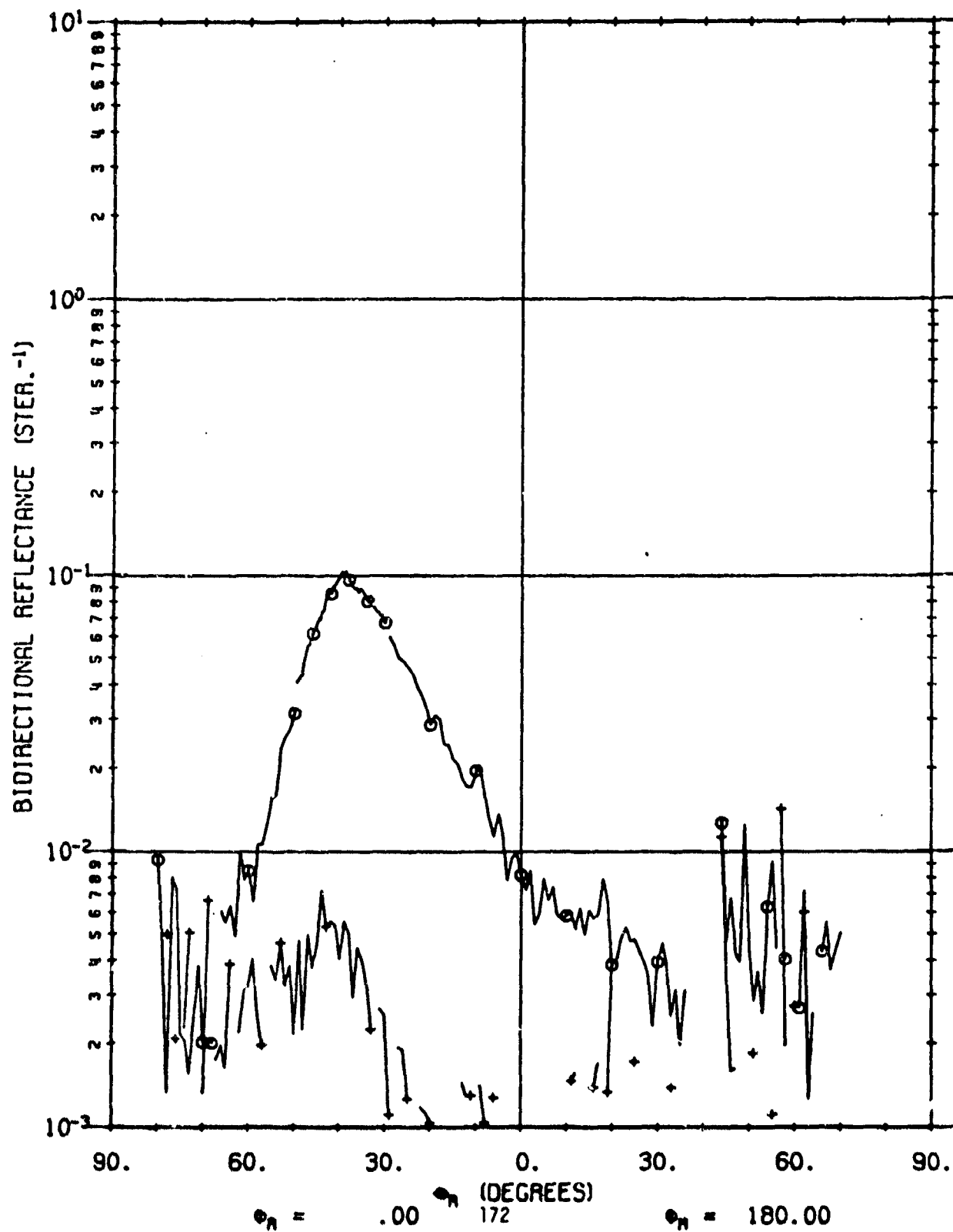
A01610 102

$\lambda = 1.06$   
 $\phi_i = 40.0$   
 $\phi_f = 180.0$



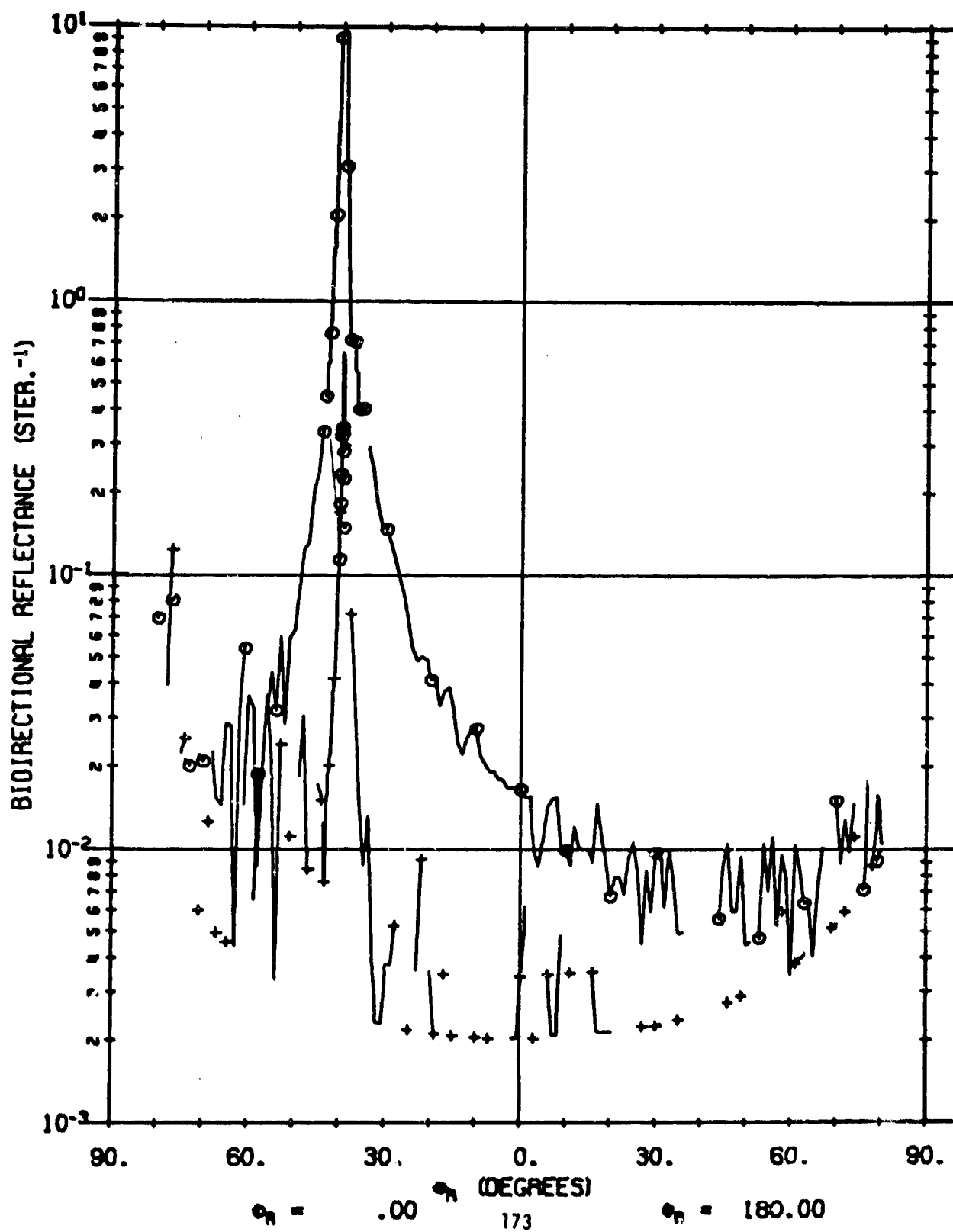
A01610 301

$\lambda = 3.39$   
 $\phi_1 = 40.0$   
 $\phi_2 = 180.0$



A01610 204

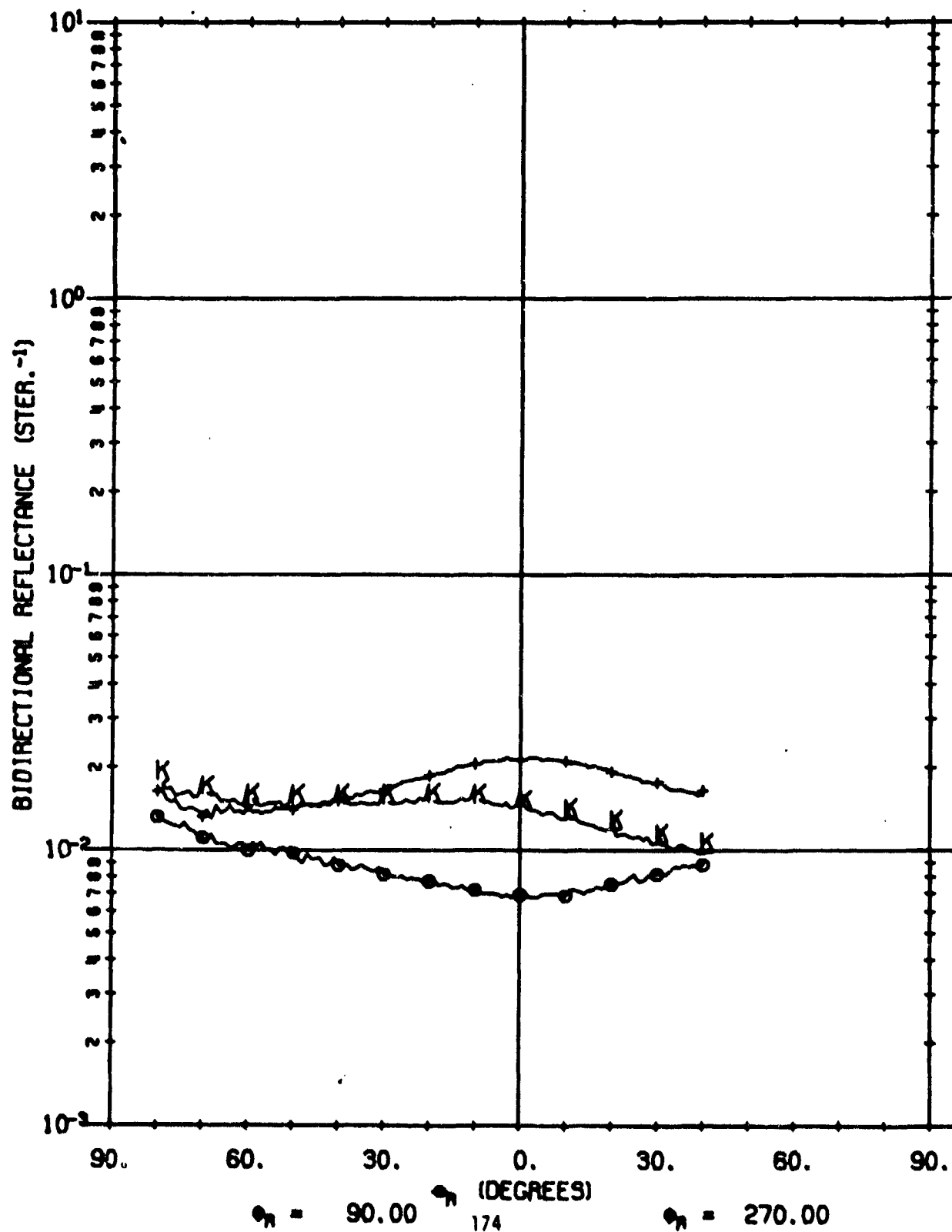
$\lambda = 10.60$   
 $\phi_i = 40.0$   
 $\phi_f = 180.0$





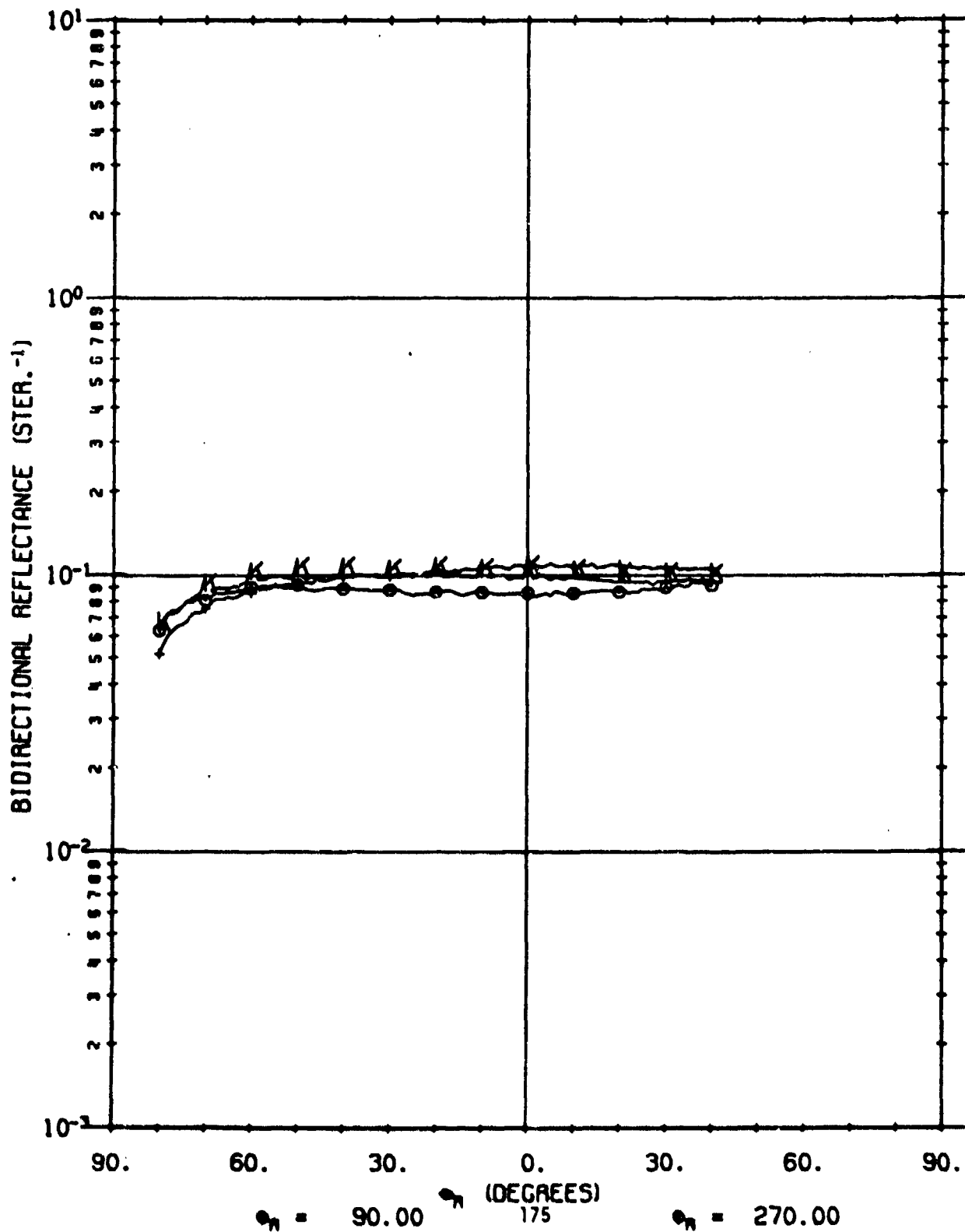
A01610 101

$\lambda = .63$   
 $\phi_1 = 40.0$   
 $\phi_2 = 180.0$



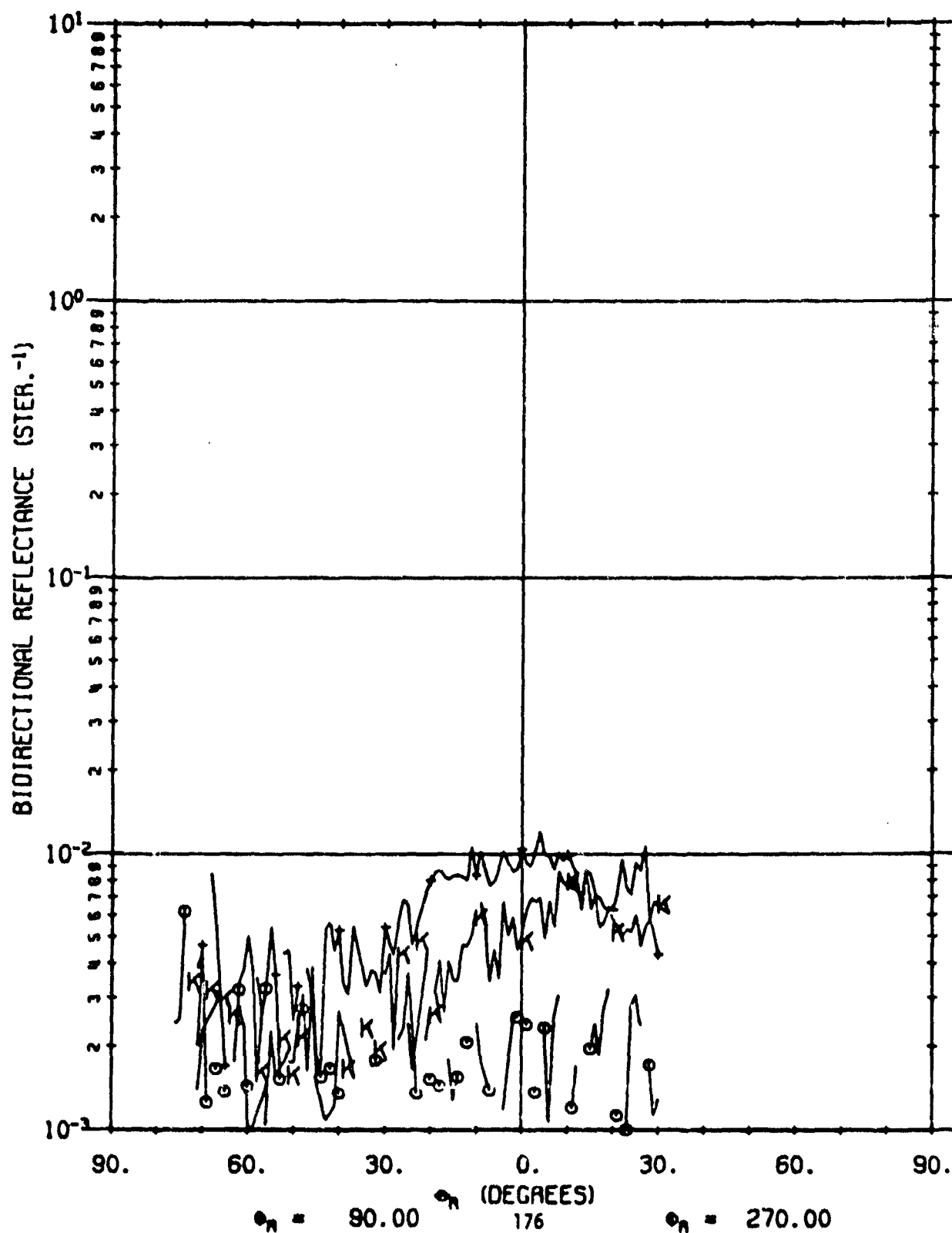
A01610 102

$\lambda = 1.06$   
 $\phi_i = 40.0$   
 $\phi_f = .0$



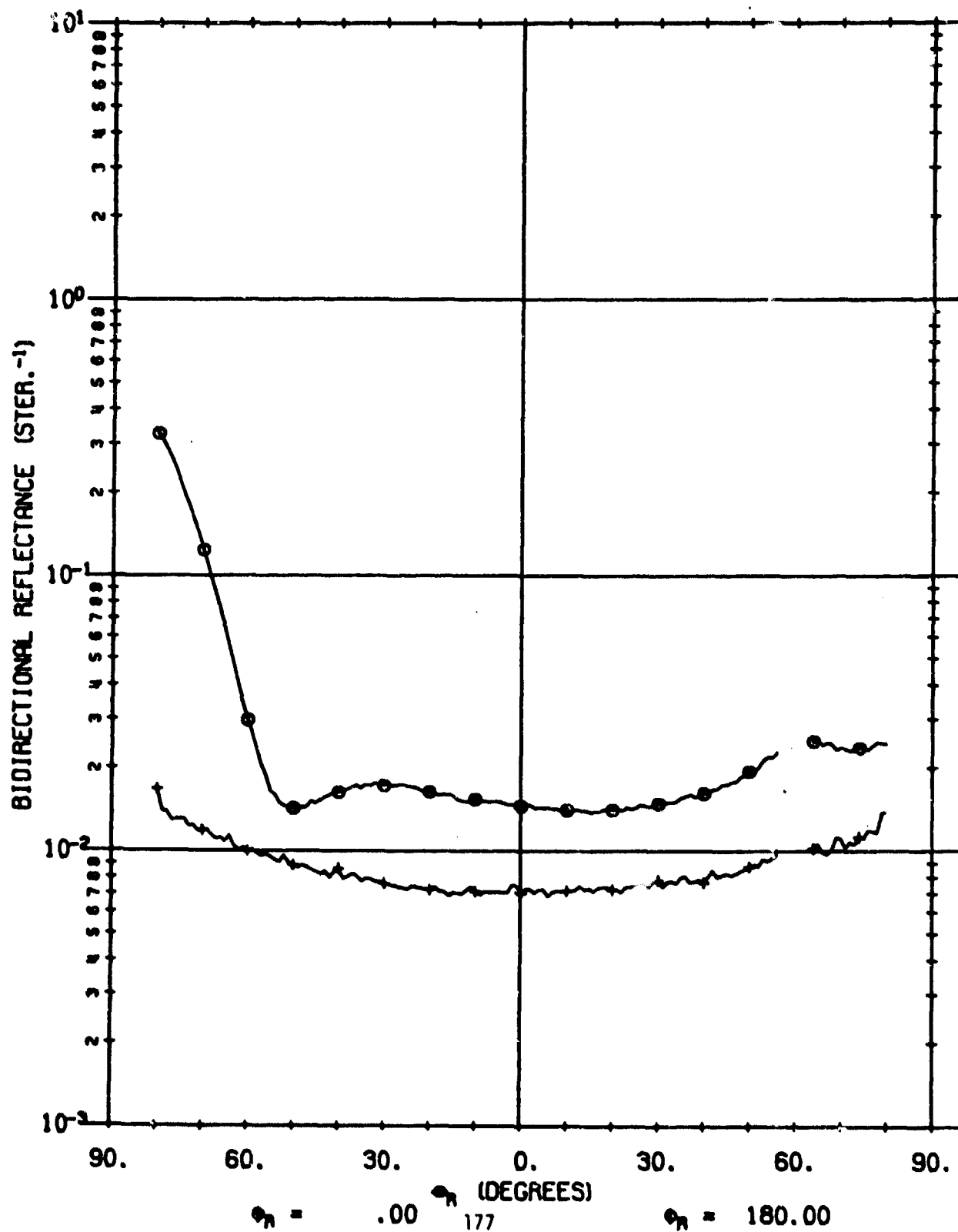
A01610 302

$\lambda = 3.39$   
 $\phi_i = 40.0$   
 $\phi_i = 180.0$



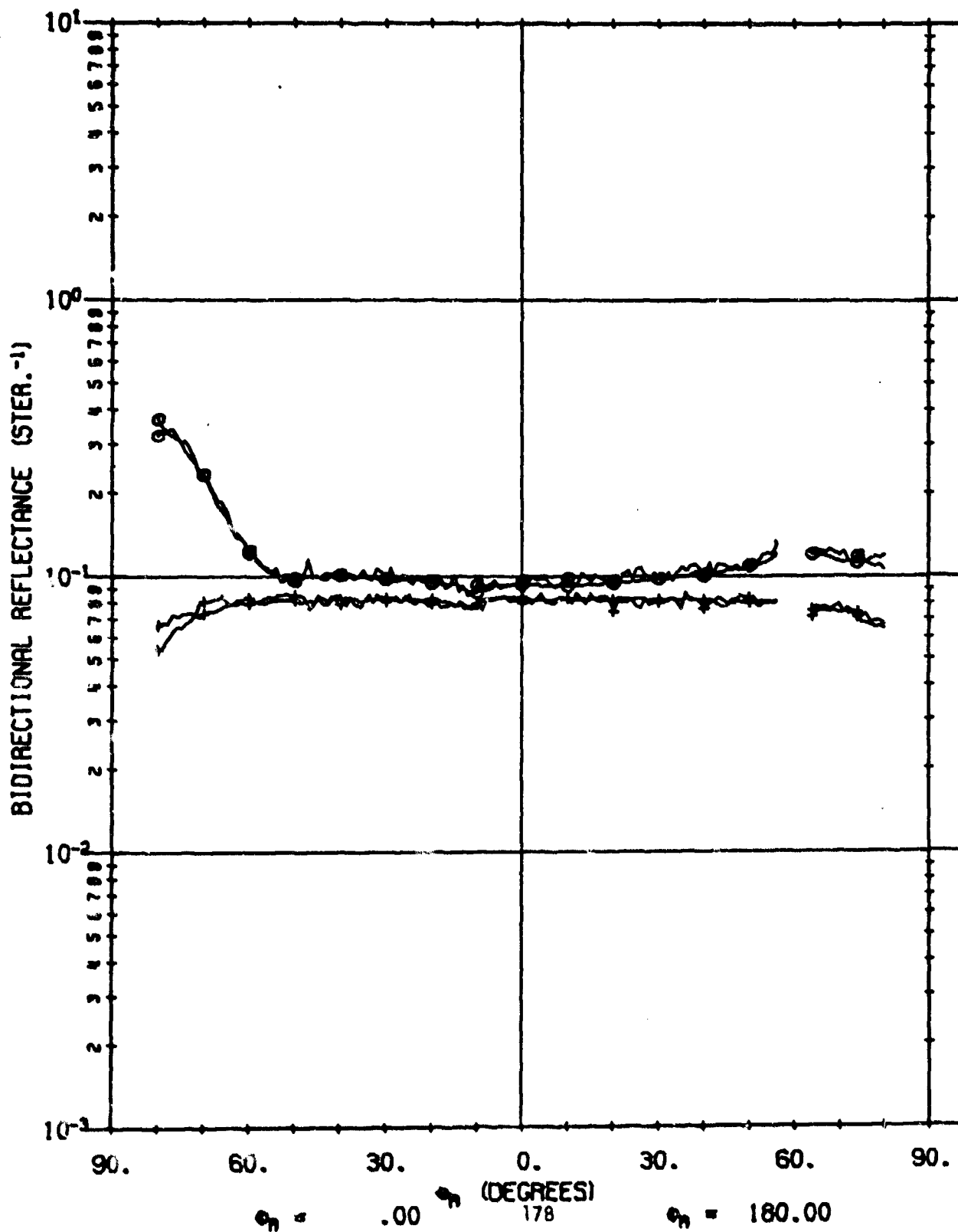
A01610 101

$\lambda = .63$   
 $\phi_i = 60.0$   
 $\phi_i = 180.0$



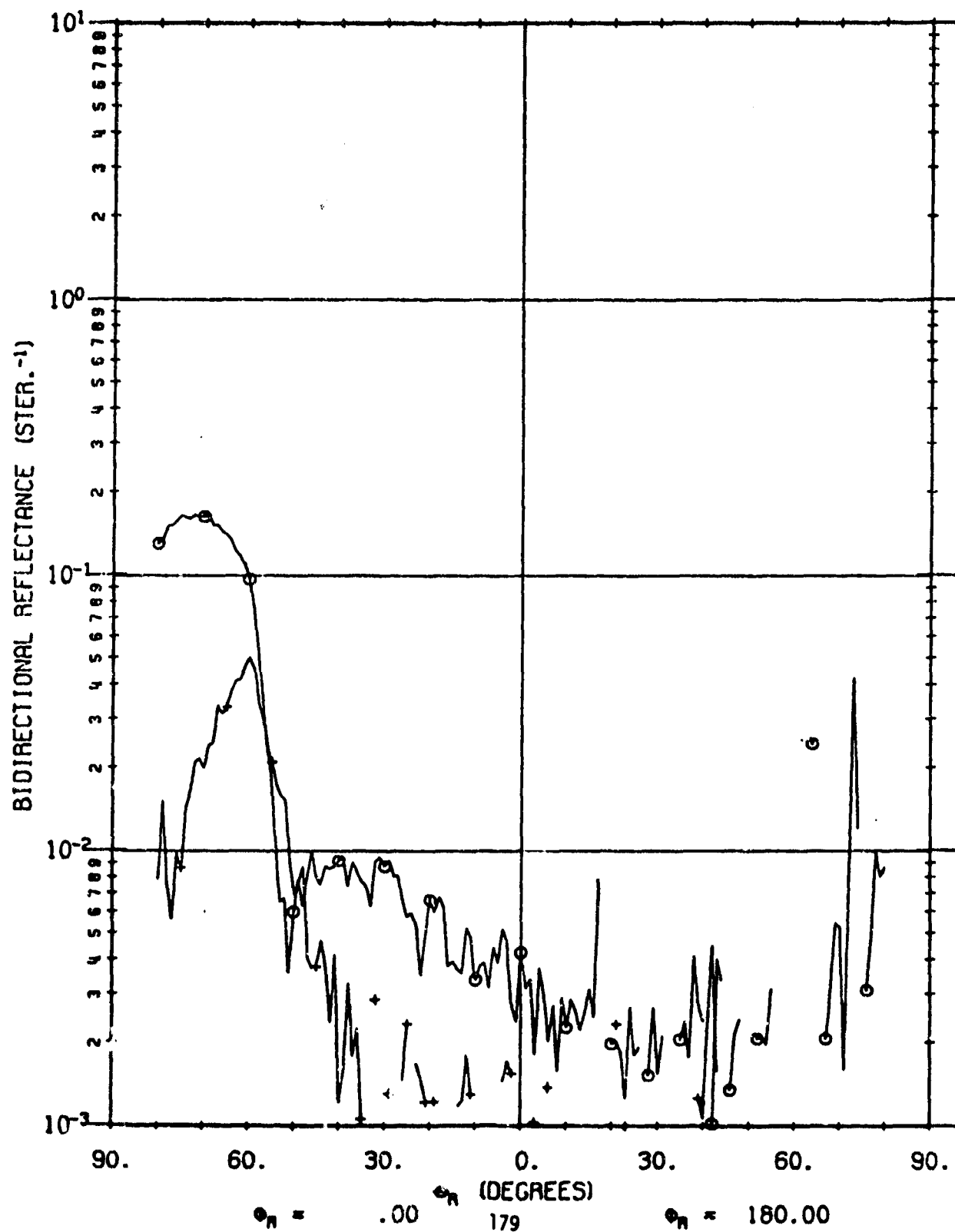
A01610 102

$\lambda = 1.06$   
 $\theta_i = 60.0$   
 $\theta_f = 180.0$



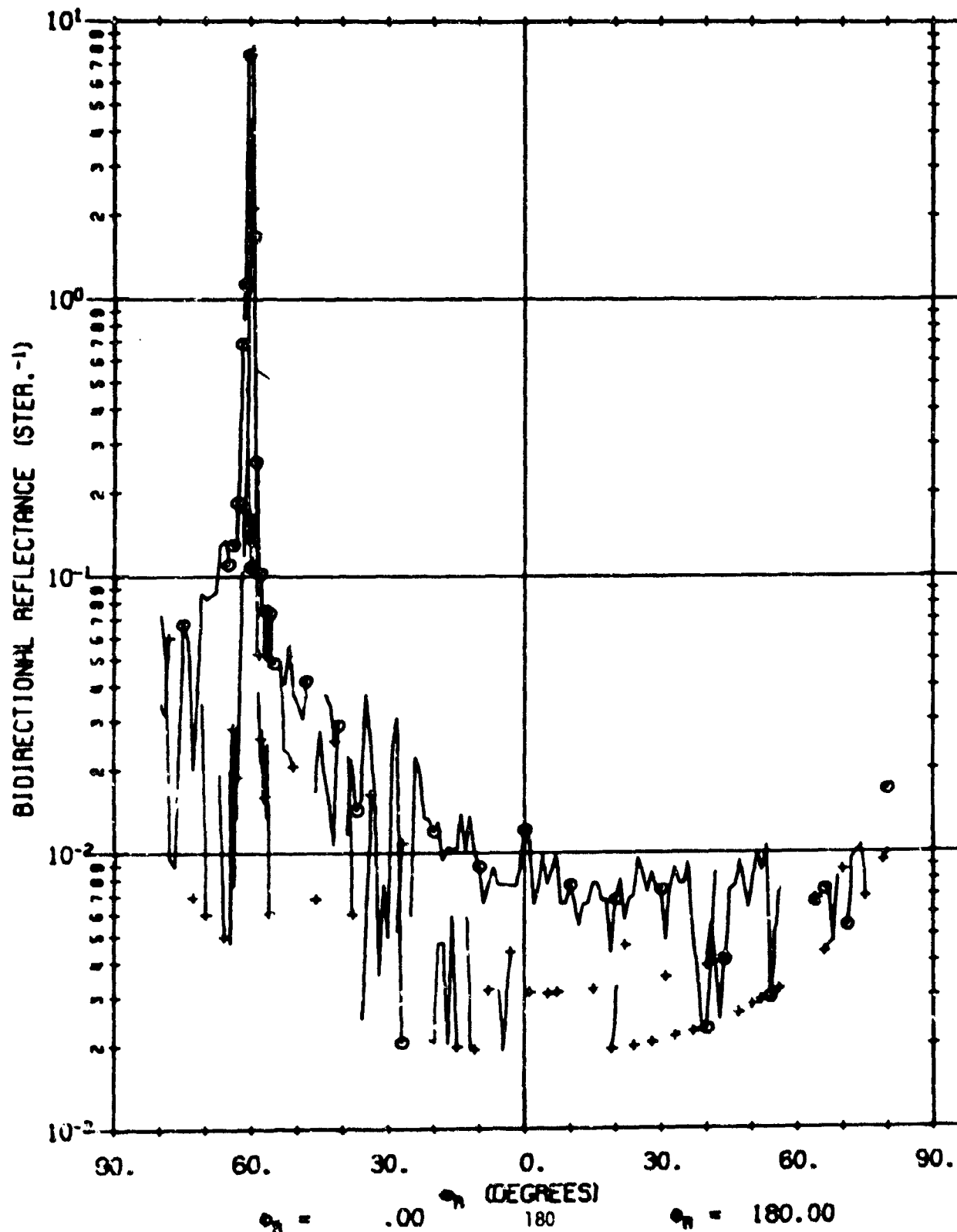
A01610 301

$\lambda = 3.39$   
 $\phi_i = 60.0$   
 $\phi_j = 180.0$



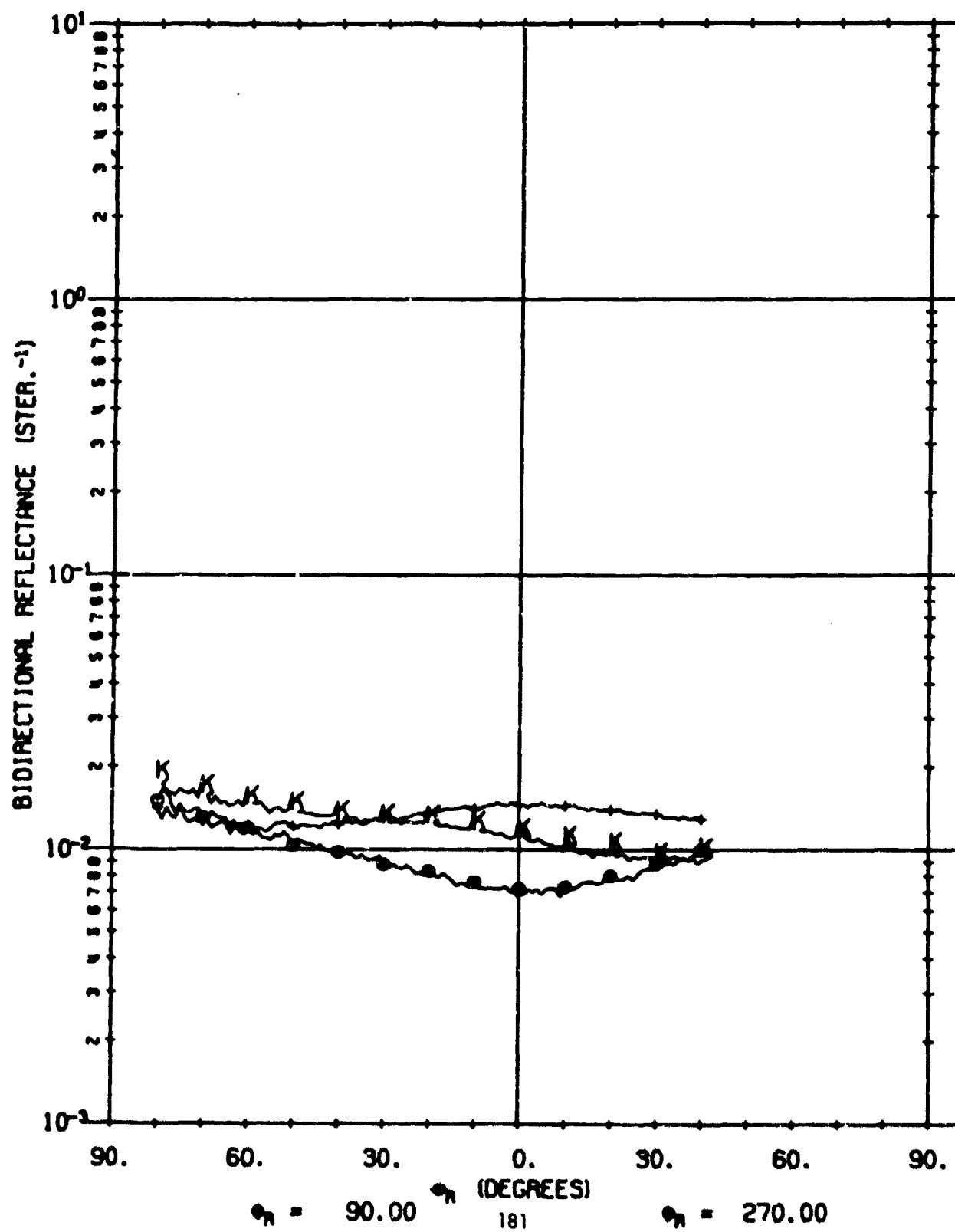
A01610 204

$\lambda = 10.60$   
 $\phi_i = 60.0$   
 $\phi_f = 180.0$



A01610 101

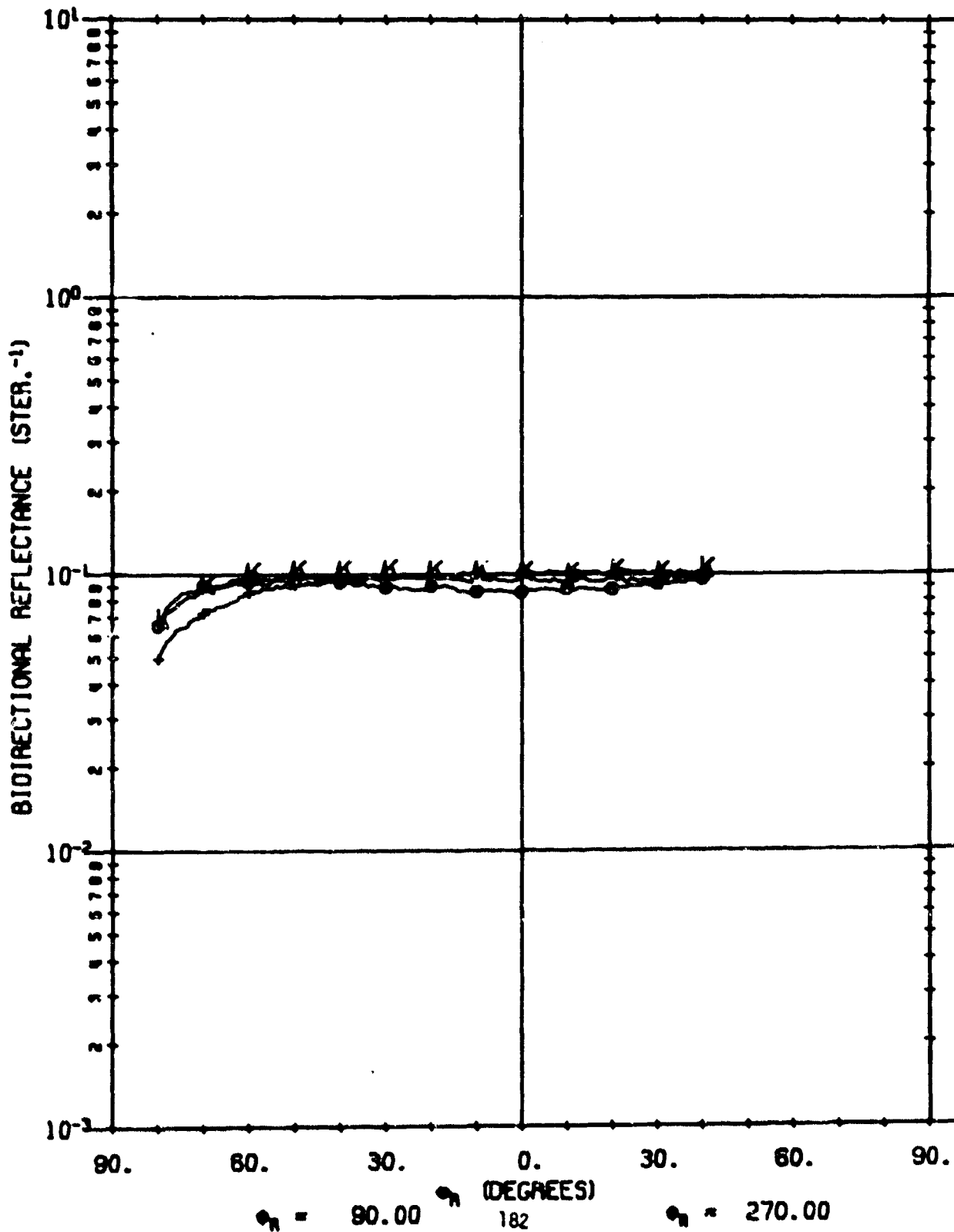
$\lambda = .63$   
 $\phi_i = 60.0$   
 $\phi_i = 180.0$





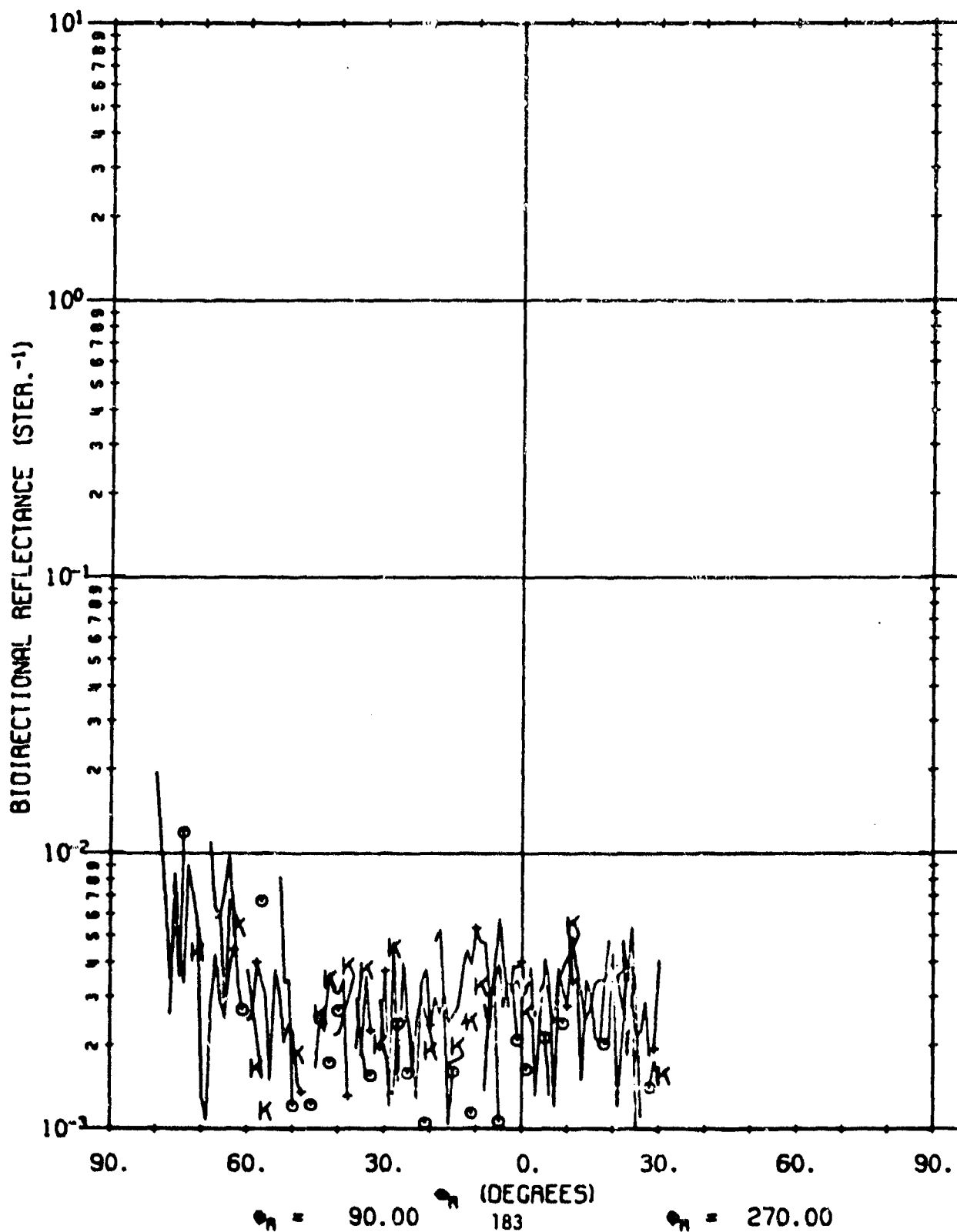
A01610 102

$\lambda = 1.06$   
 $\theta_i = 60.0$   
 $\phi_i = .0$



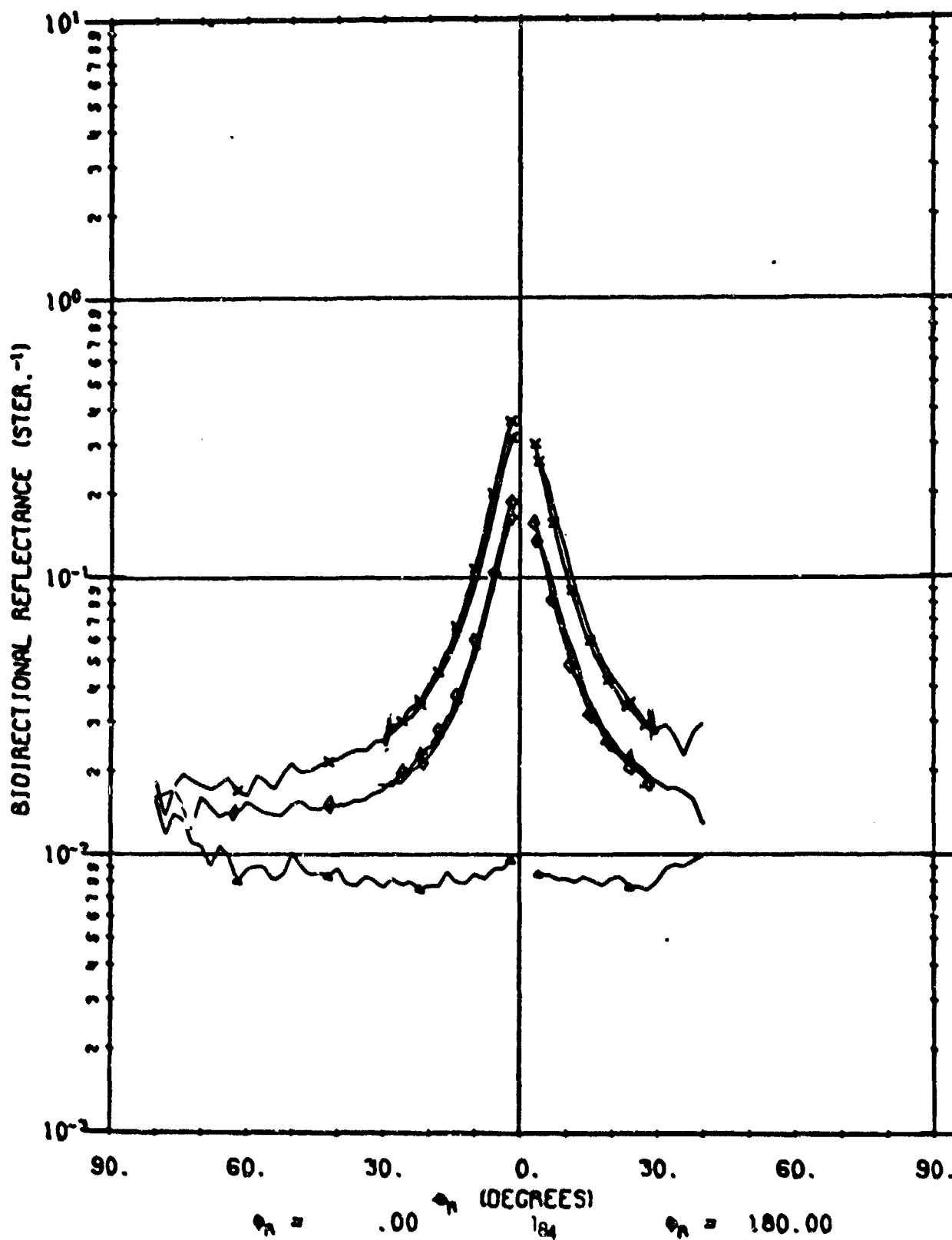
A01610 302

$\lambda = 3.39$   
 $\phi_1 = 60.0$   
 $\phi_2 = 180.0$



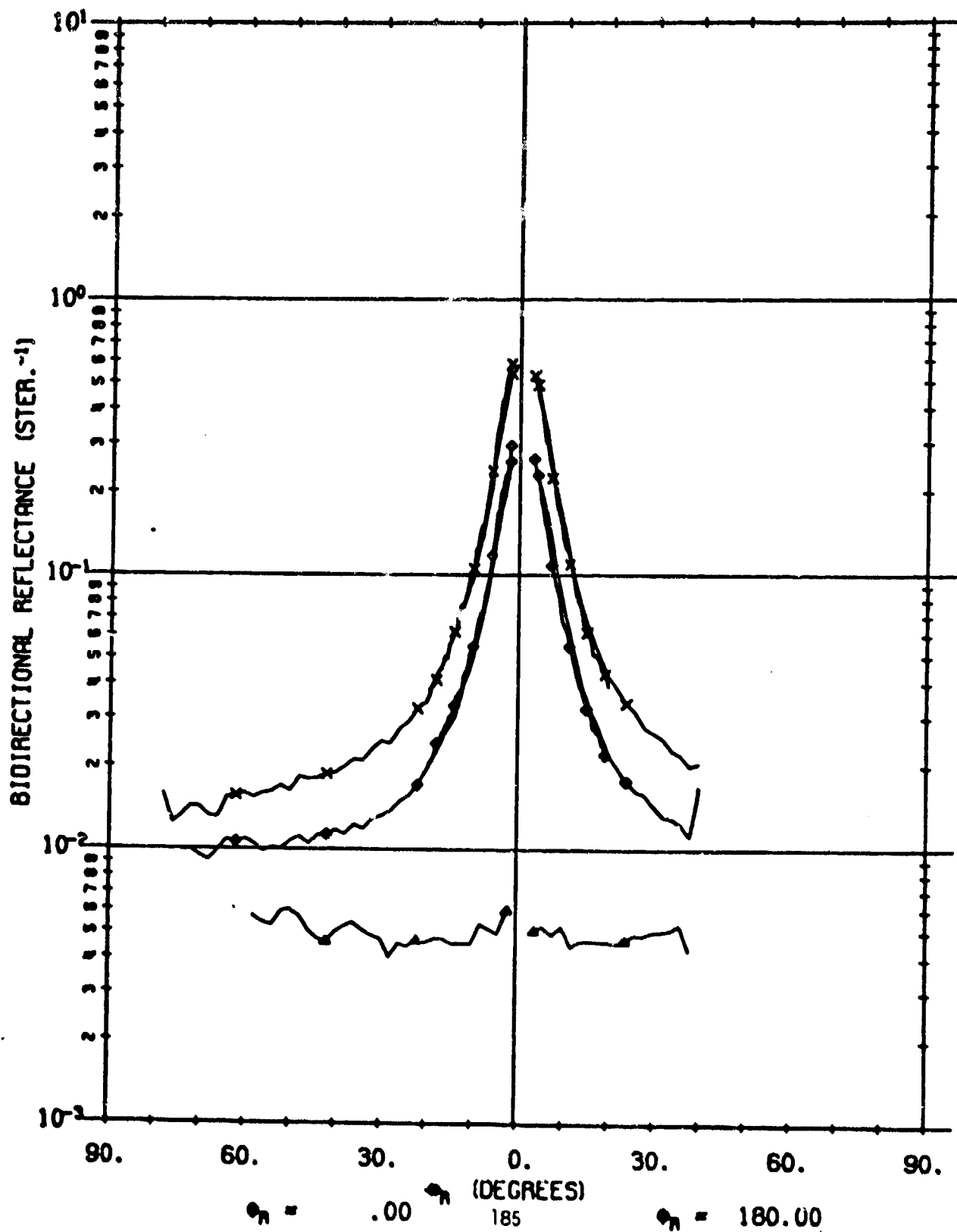
A02022 202

$\lambda = .63$   
 $\phi_1 = 0$   
 $\phi_2 = 180.0$



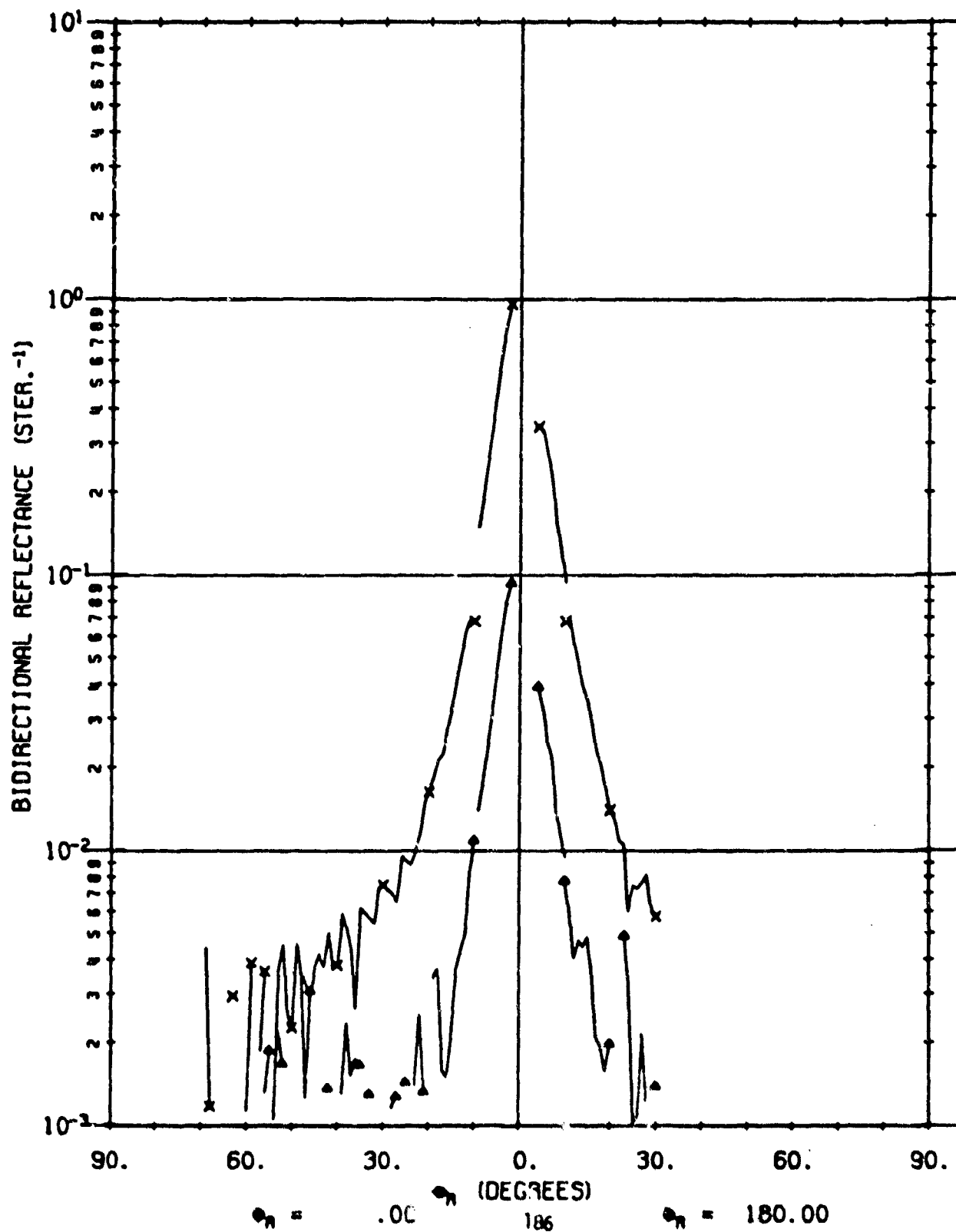
A02022 201

$\lambda = 1.06$   
 $\phi_1 = .0$   
 $\phi_2 = 180.0$



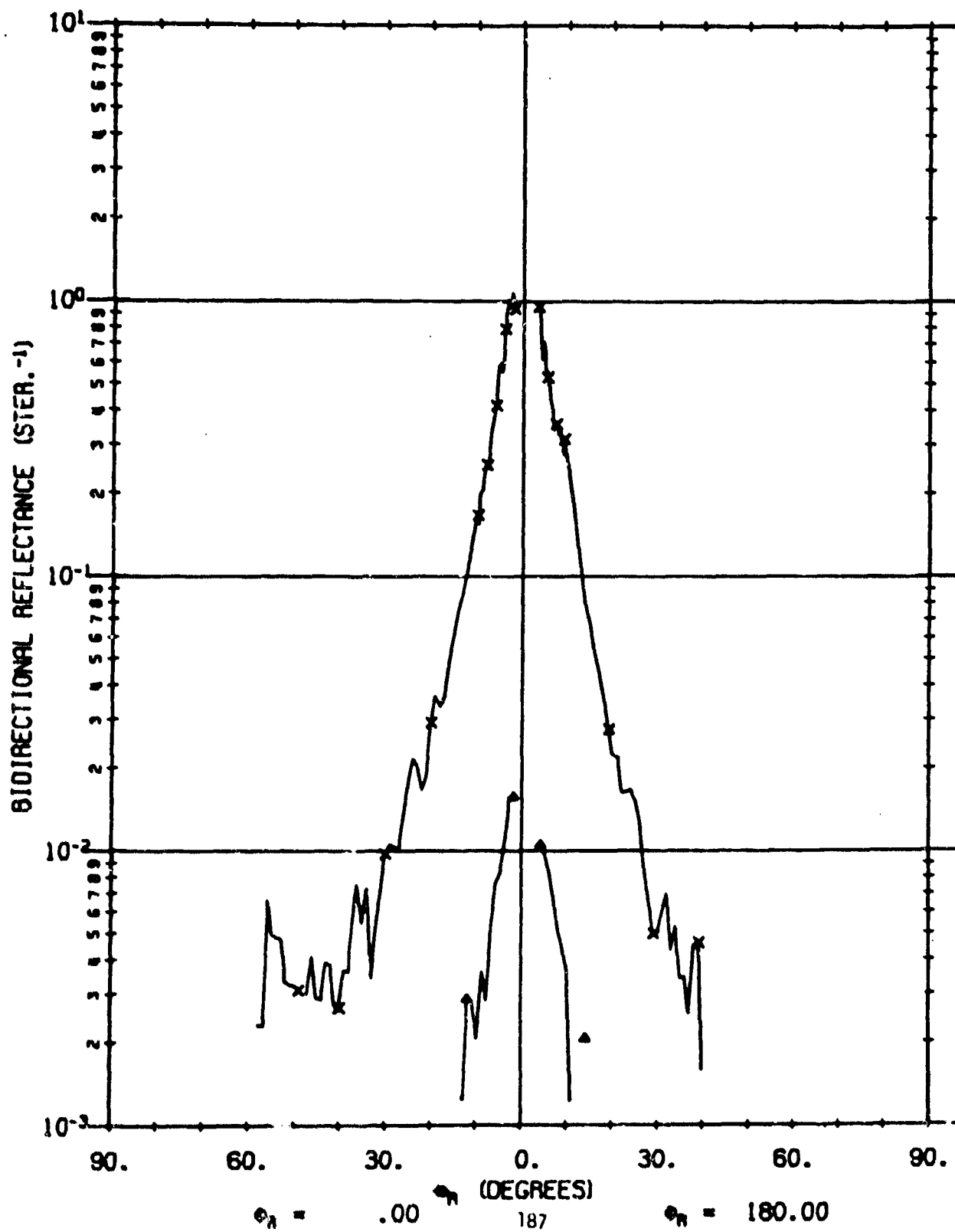
A02022 702

$\lambda = 3.39$   
 $\phi_1 = 0$   
 $\phi_2 = 180.0$



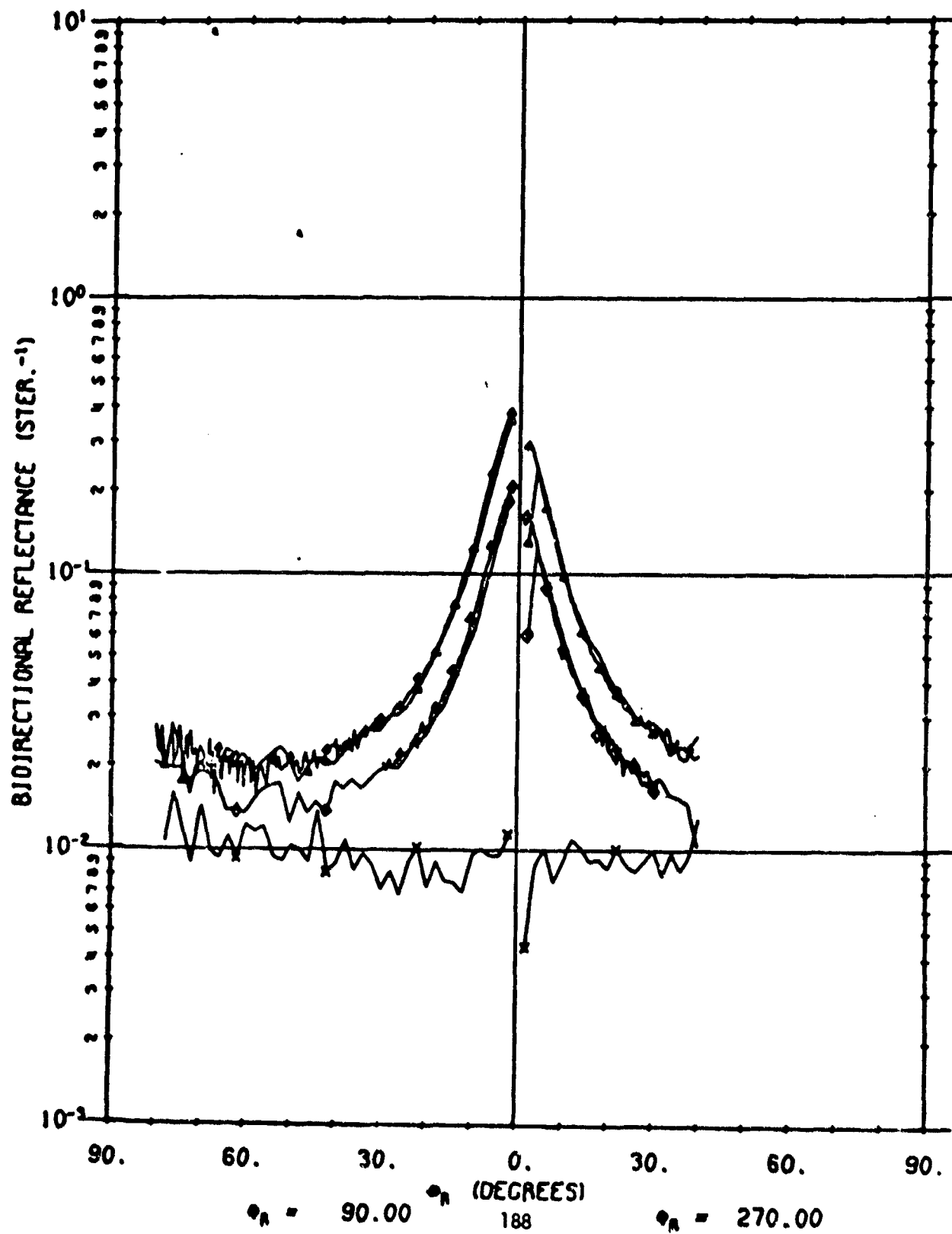
A02022 602

$\lambda = 10.60$   
 $\phi_i = 0.0$   
 $\phi_f = 180.0$



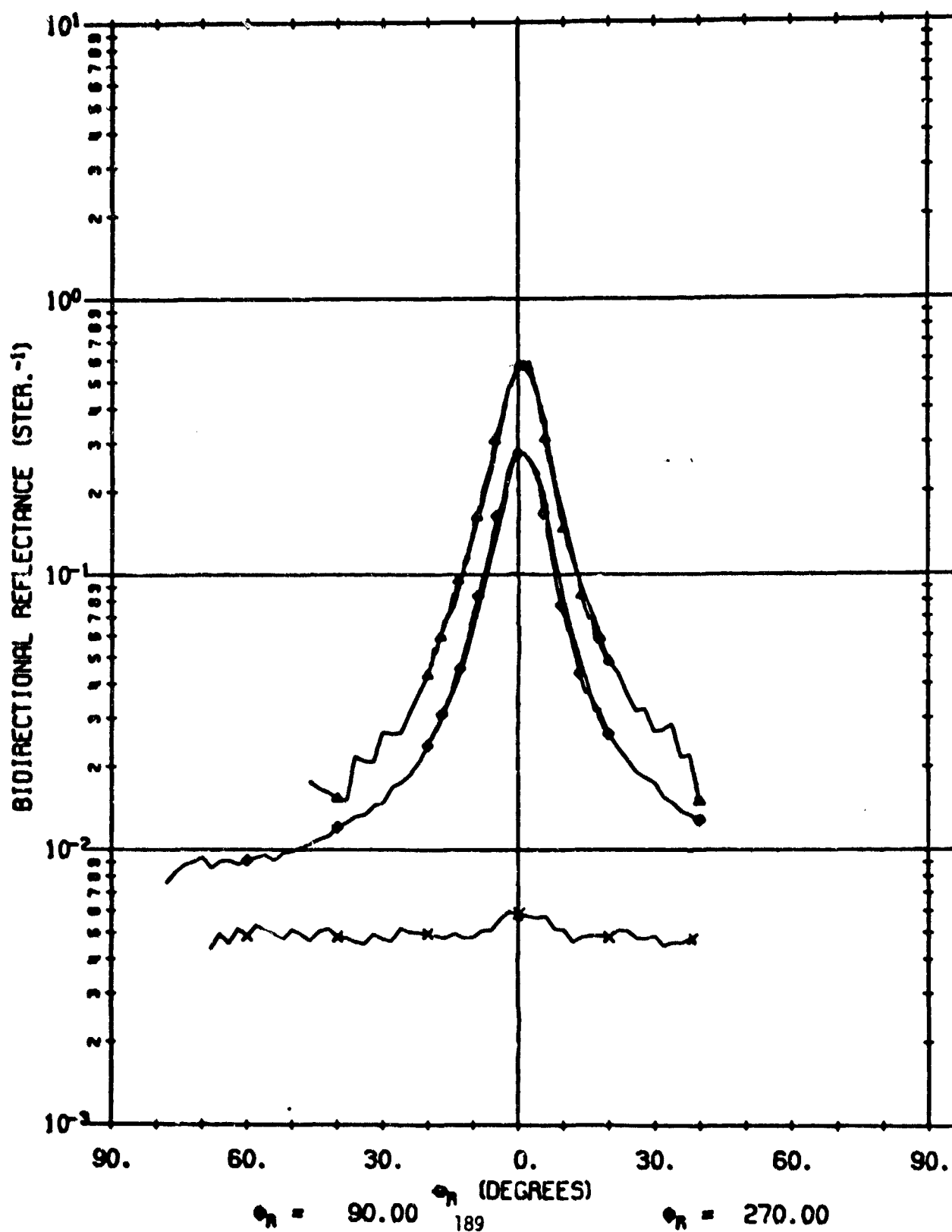
A02022 202

$\lambda = .63$   
 $\phi_i = .0$   
 $\phi_i = 180.0$



A02022 201

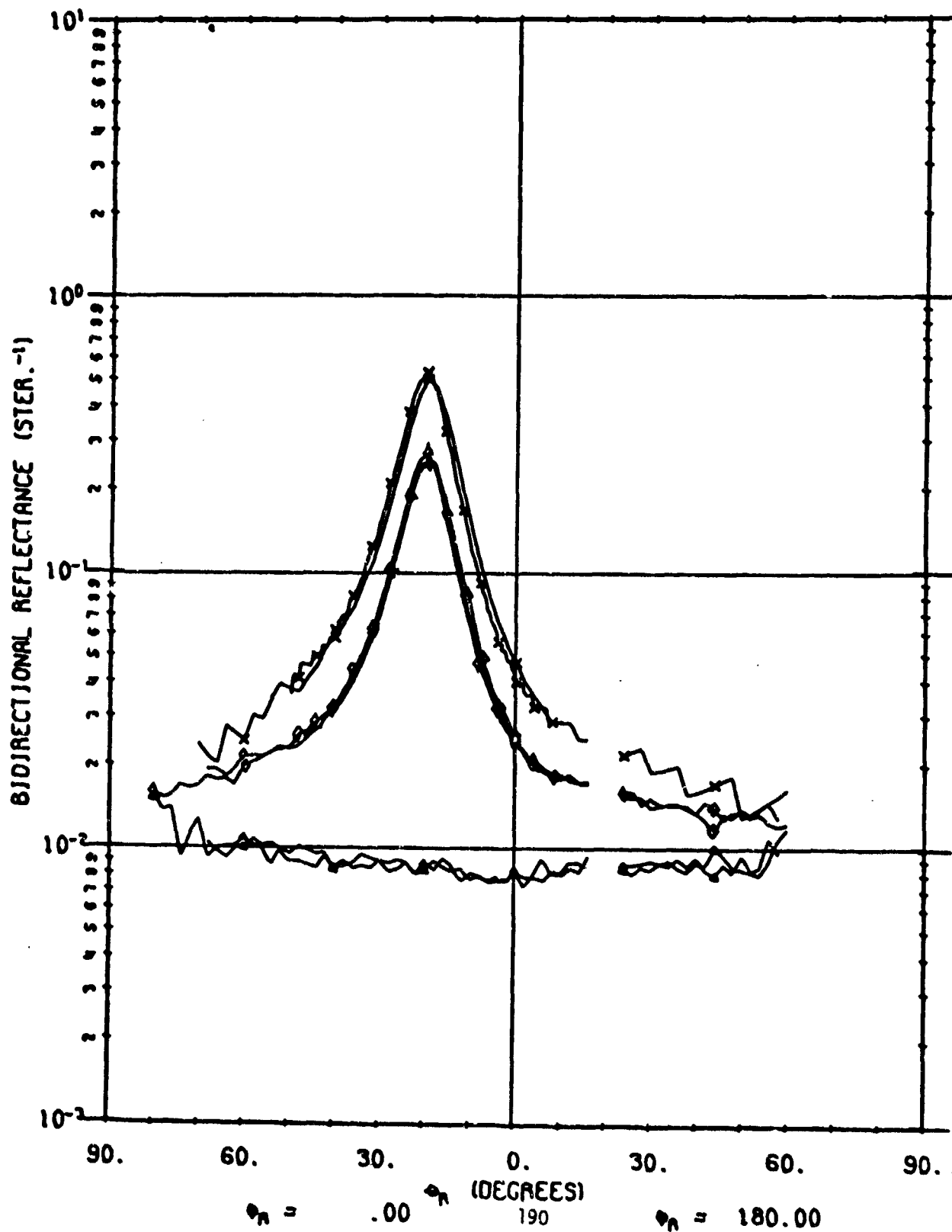
$\lambda = 1.06$   
 $\phi_1 = 0$   
 $\phi_2 = 180.0$





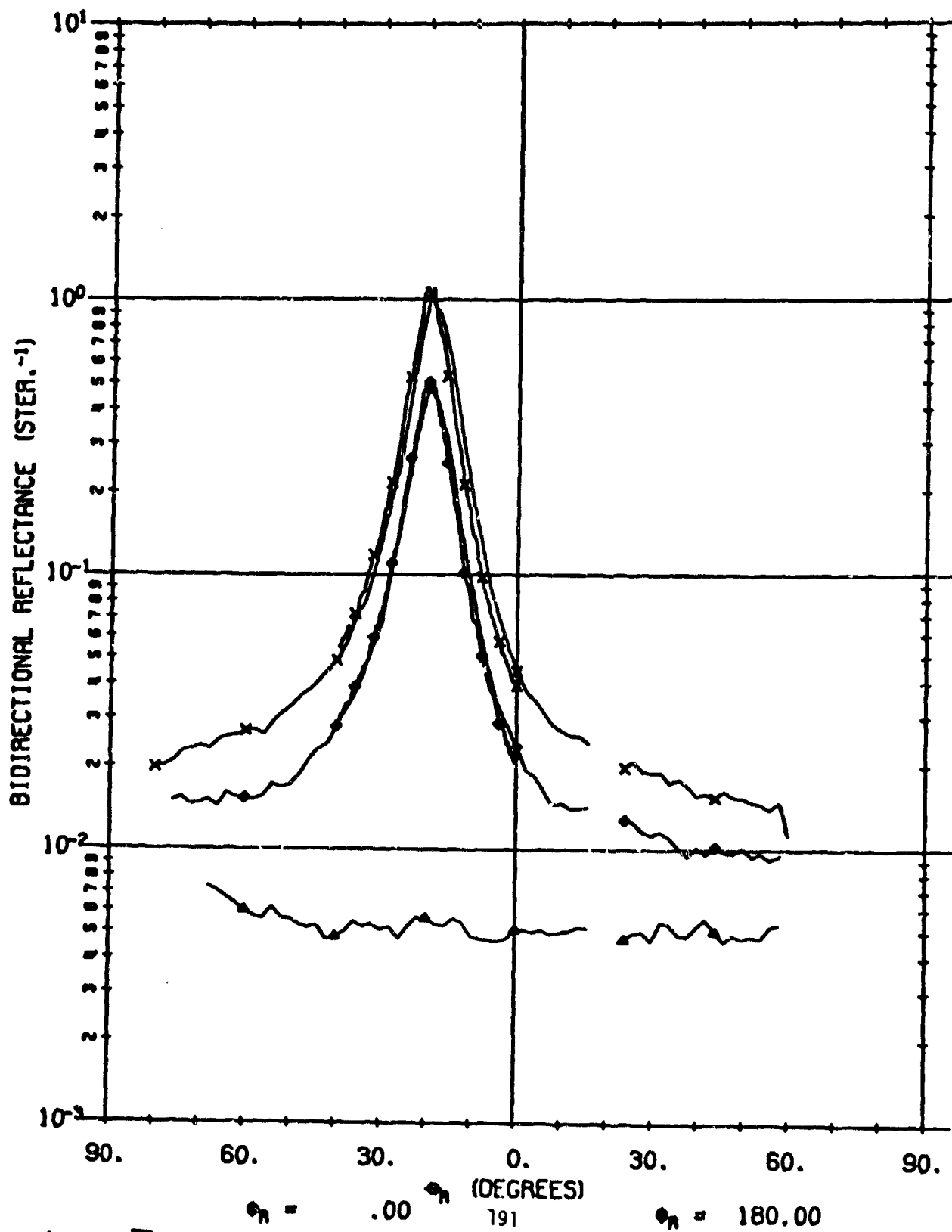
A02022 202

$\lambda = .63$   
 $\phi_i = 20.0$   
 $\phi_f = 180.0$



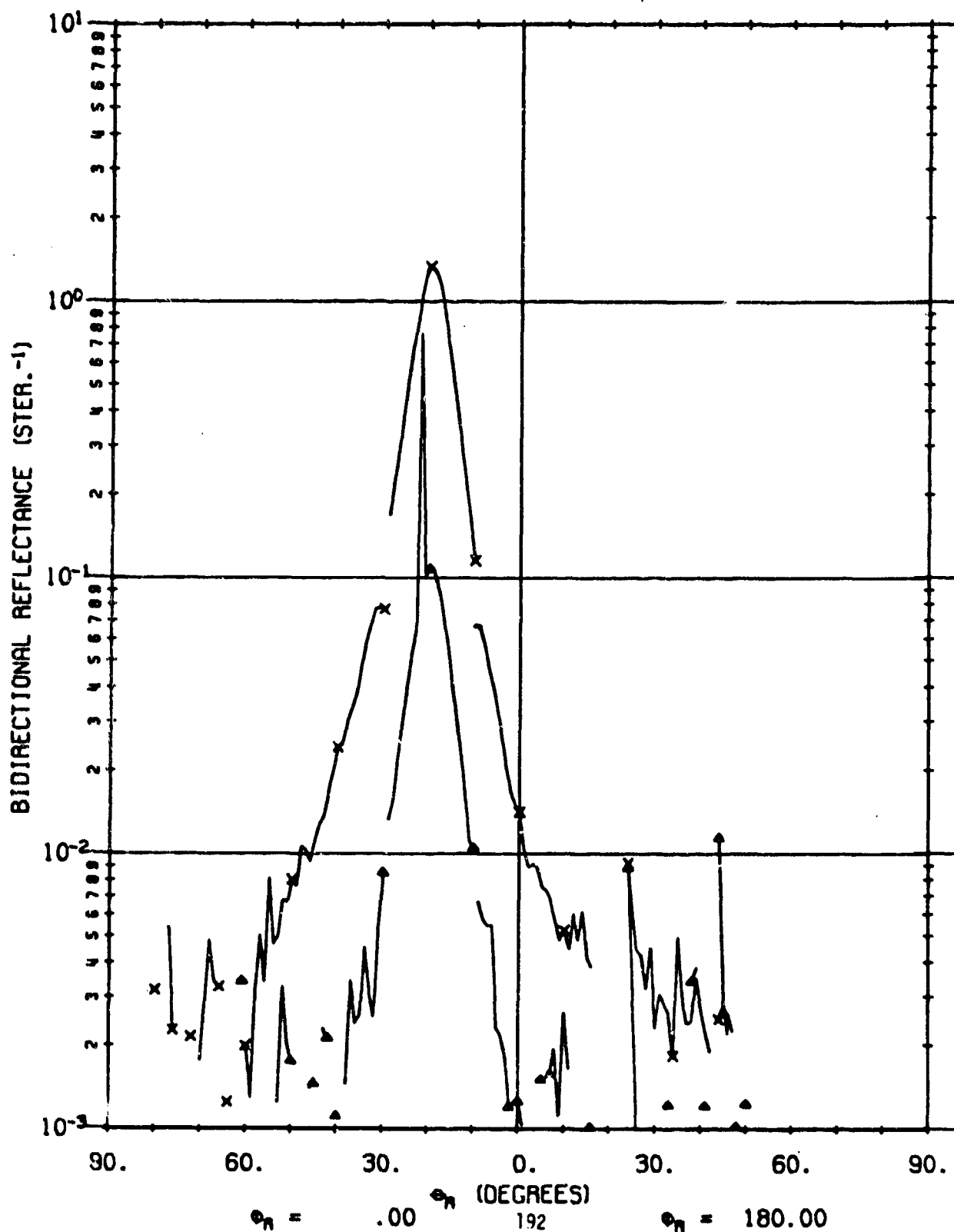
A02022 201

$\lambda = 1.06$   
 $\phi_i = 20.0$   
 $\phi_j = 180.0$



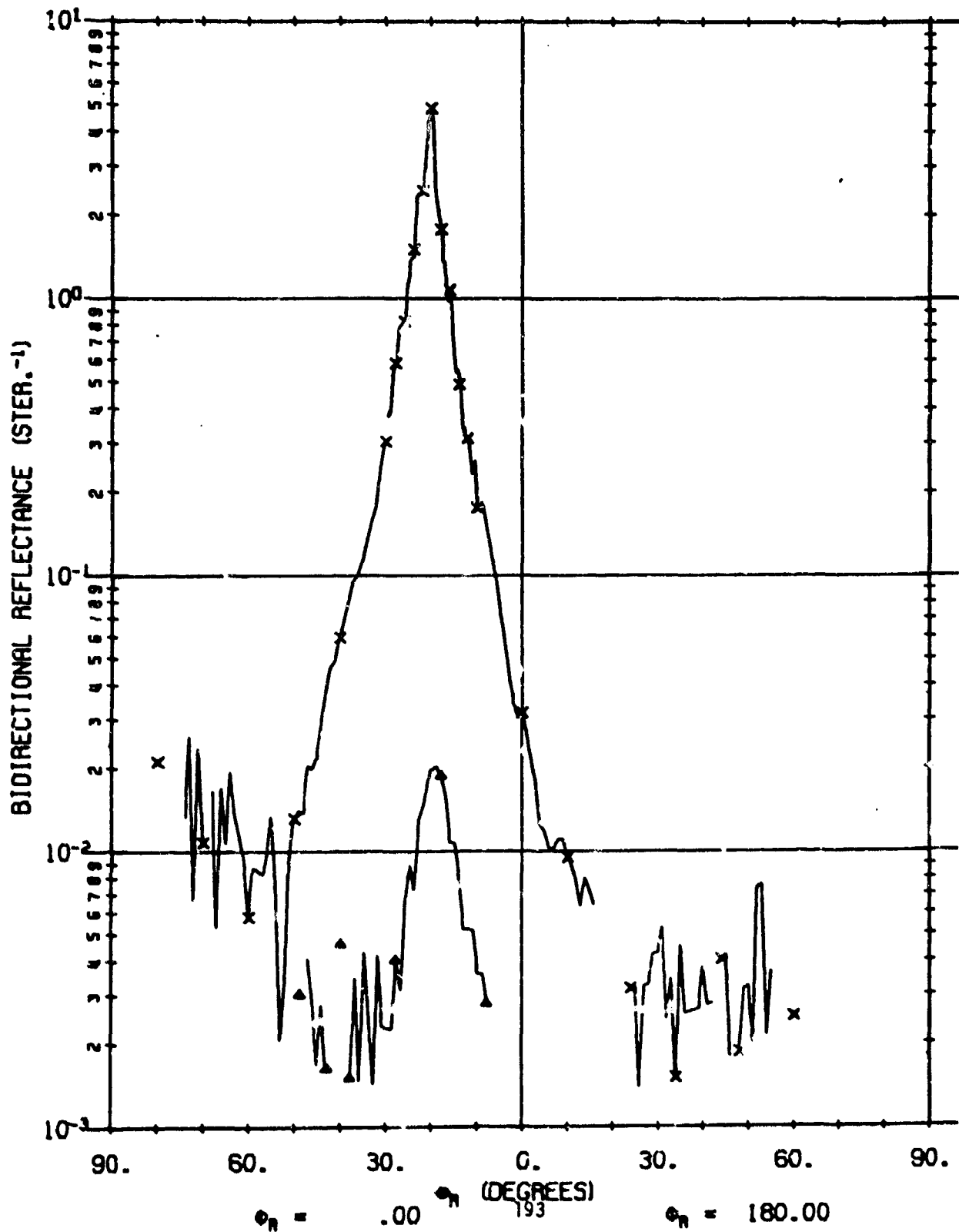
A02022 702

$\lambda = 3.39$   
 $\phi_i = 20.0$   
 $\phi_f = 180.0$

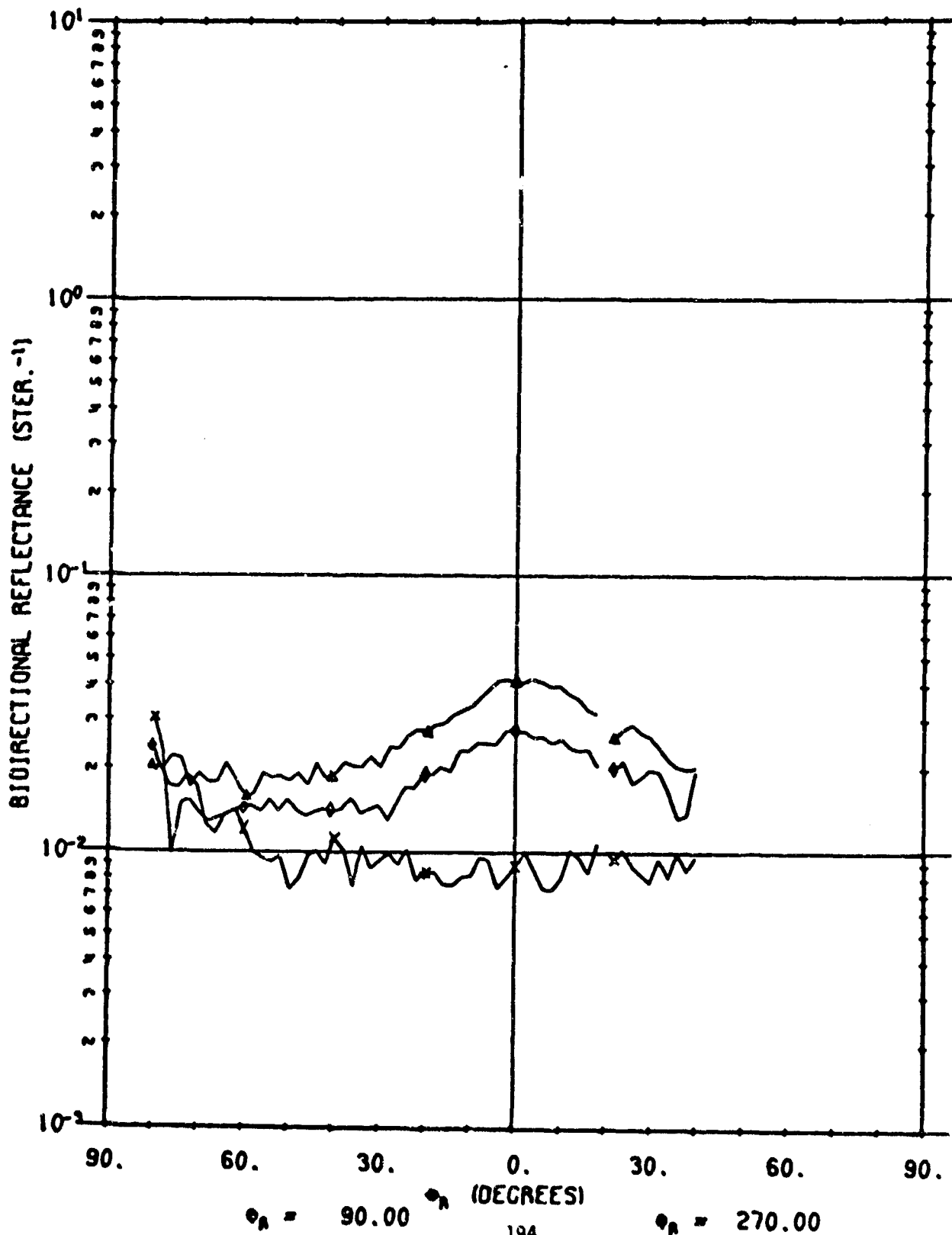


A02022 602

$\lambda = 10.60$   
 $\phi_i = 20.0$   
 $\phi_f = 180.0$

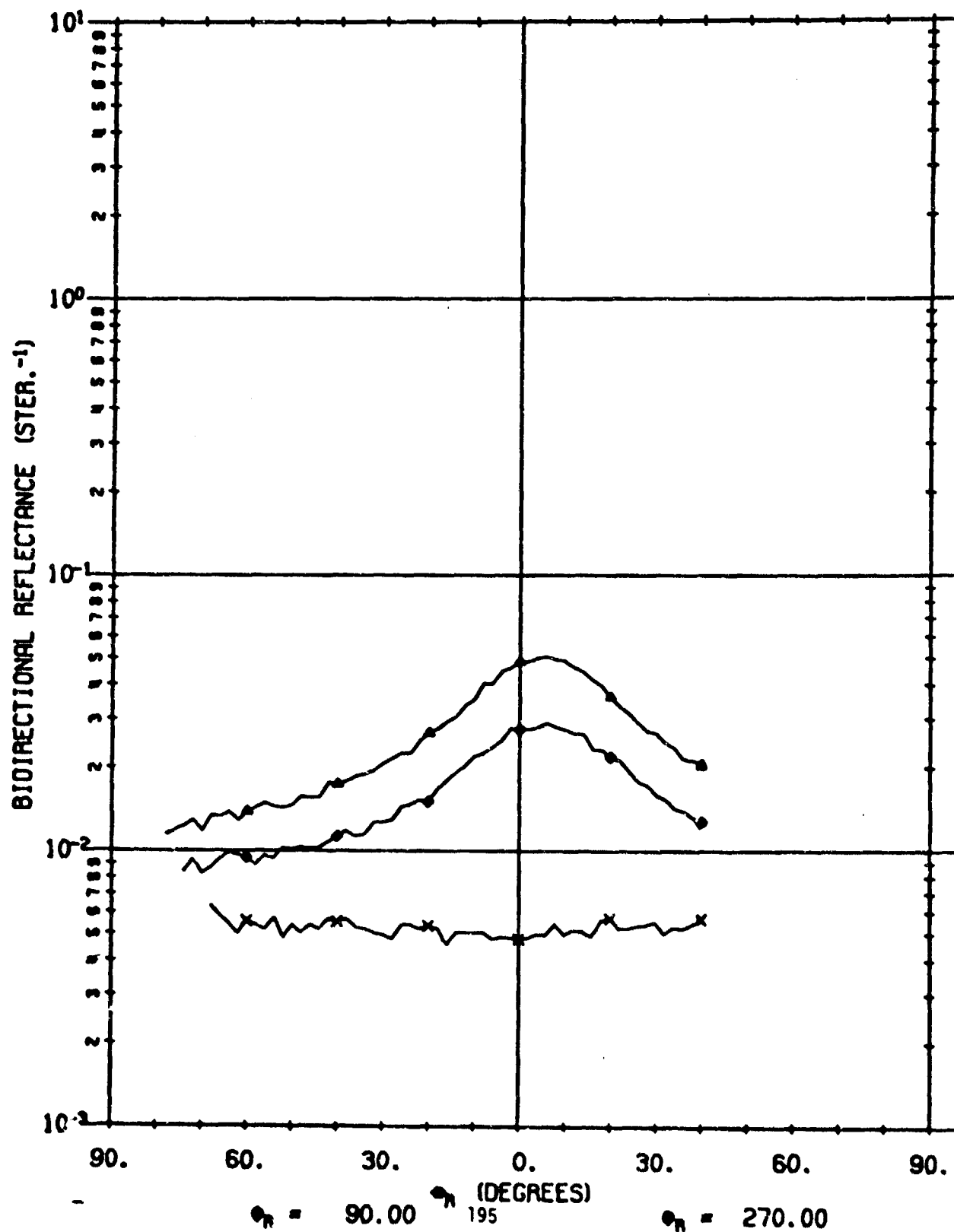


$\lambda = .63$   
 $\phi_i = 20.0$   
 $\phi_j = 180.0$



A02022 201

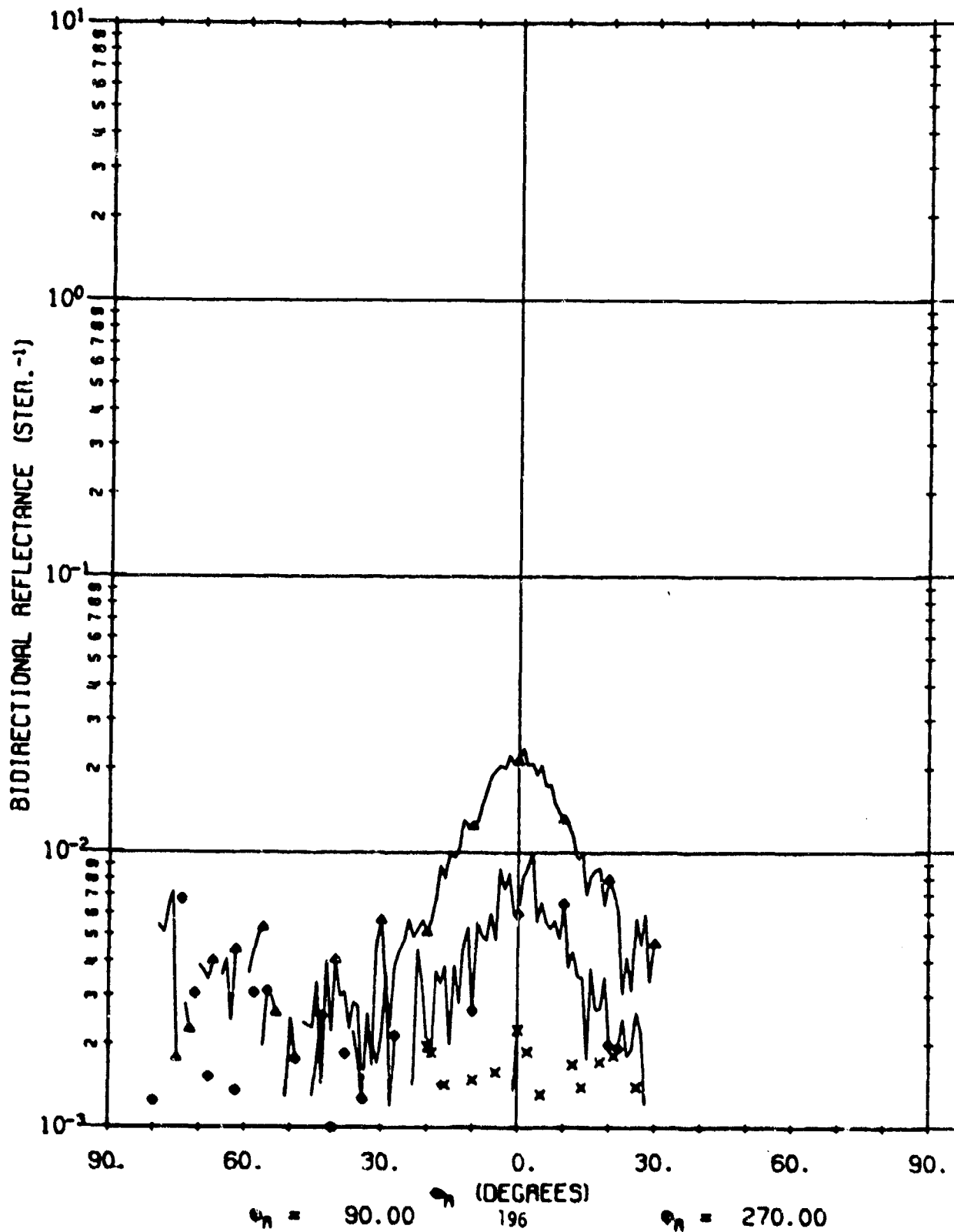
$\lambda = 1.06$   
 $\phi_1 = 20.0$   
 $\phi_2 = 180.0$



A02022 701

$\lambda = 3.39$   
 $\theta_i = 20.0$   
 $\phi_i = 180.0$

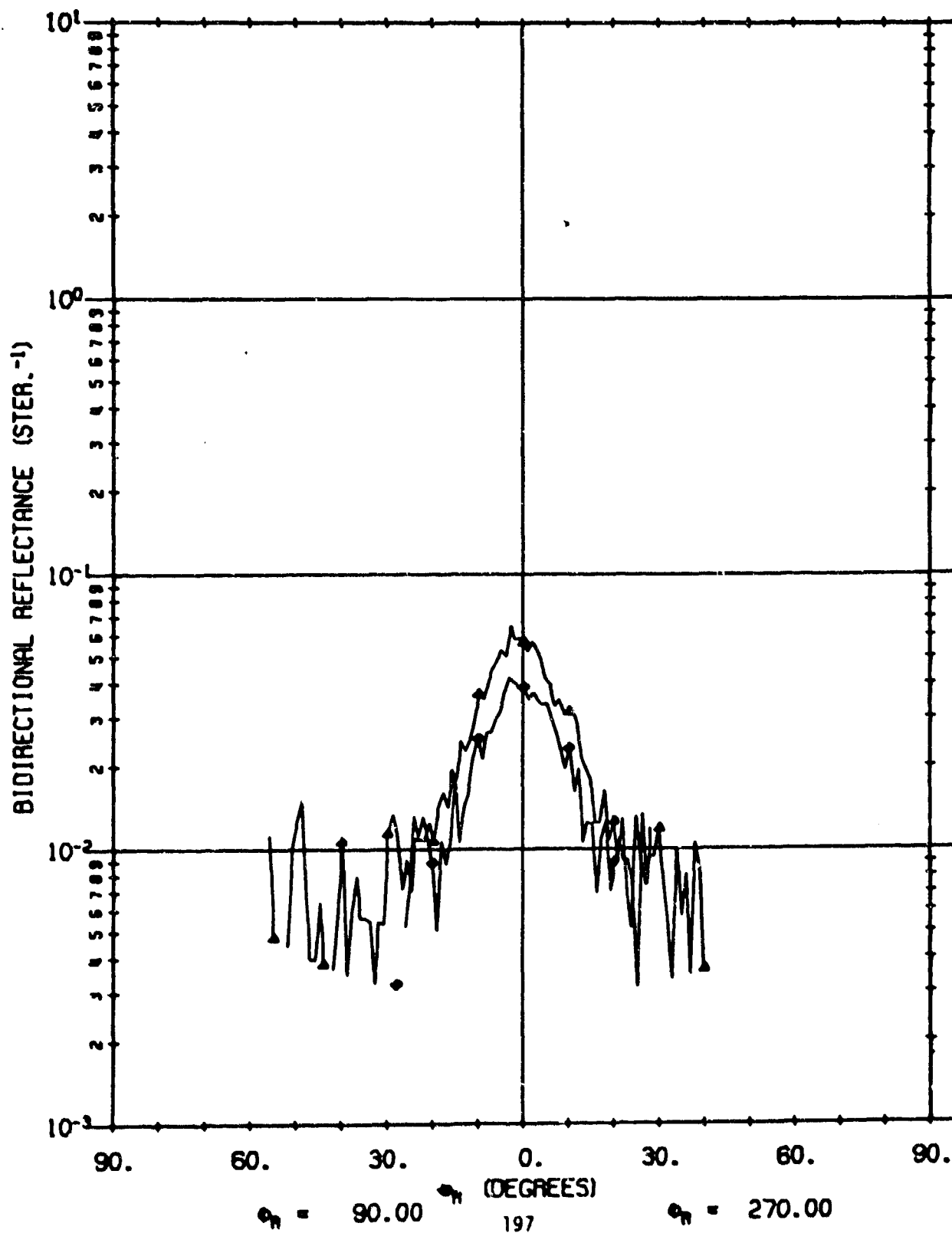
77



A02022

604

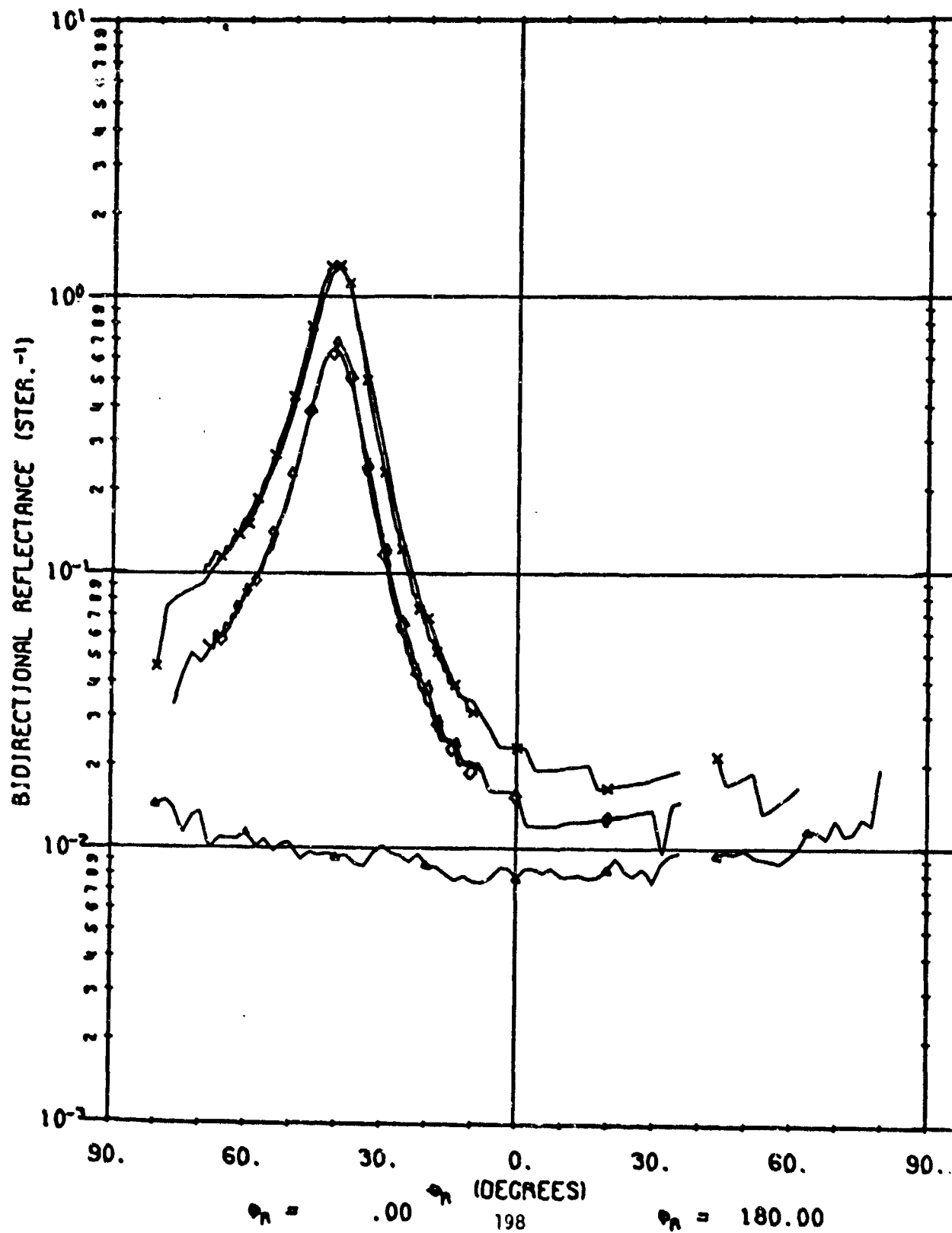
$\lambda = 10.60$   
 $\phi_i = 20.0$   
 $\phi_f = 180.0$





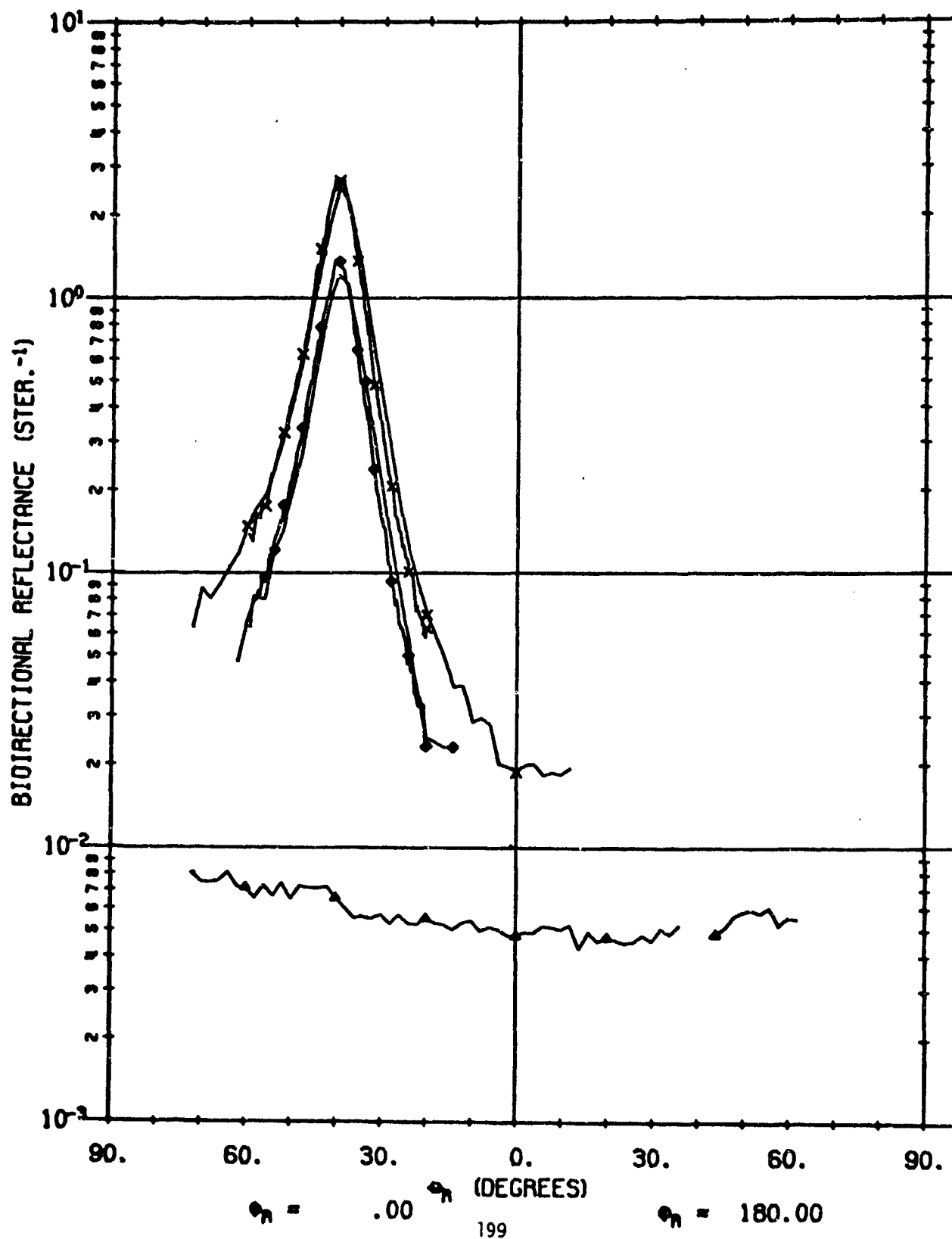
A02022 202

$\lambda = .63$   
 $\phi_i = 40.0$   
 $\phi_f = 180.0$



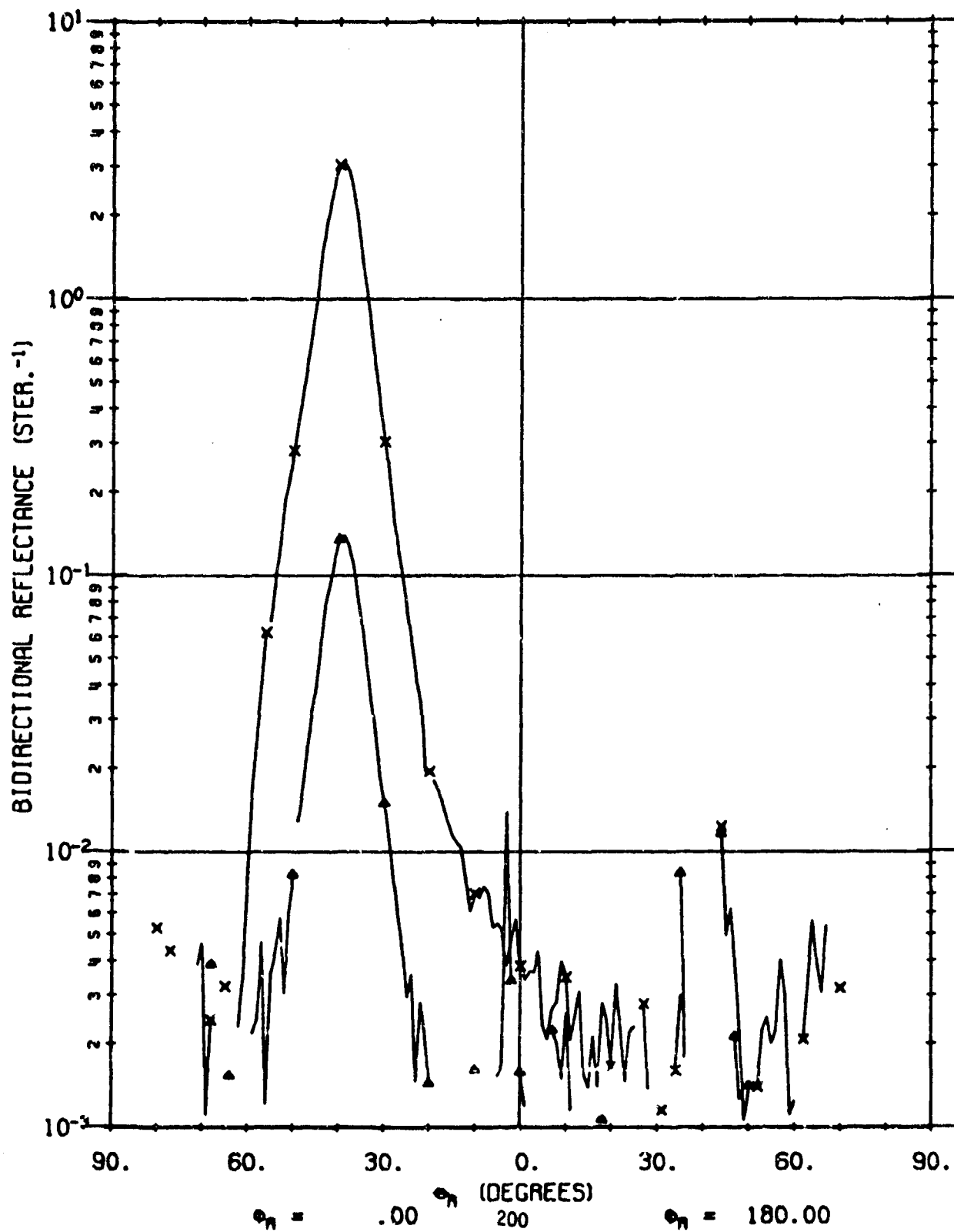
A02022 201

$\lambda = 1.06$   
 $\phi_i = 40.0$   
 $\phi_i = 180.0$



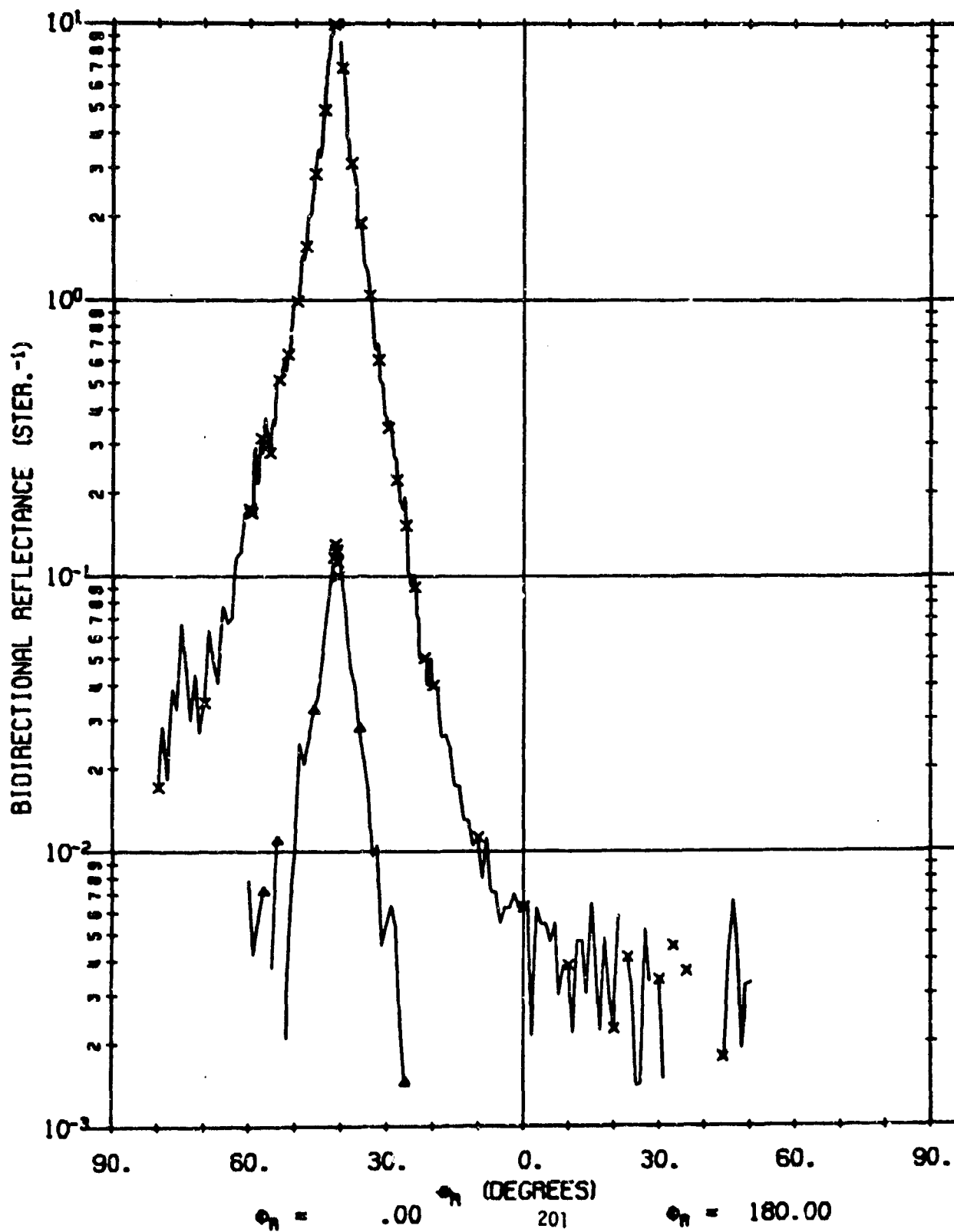
A02022 702

$\lambda = 3.39$   
 $\phi_i = 40.0$   
 $\phi_i = 180.0$



A02022 602

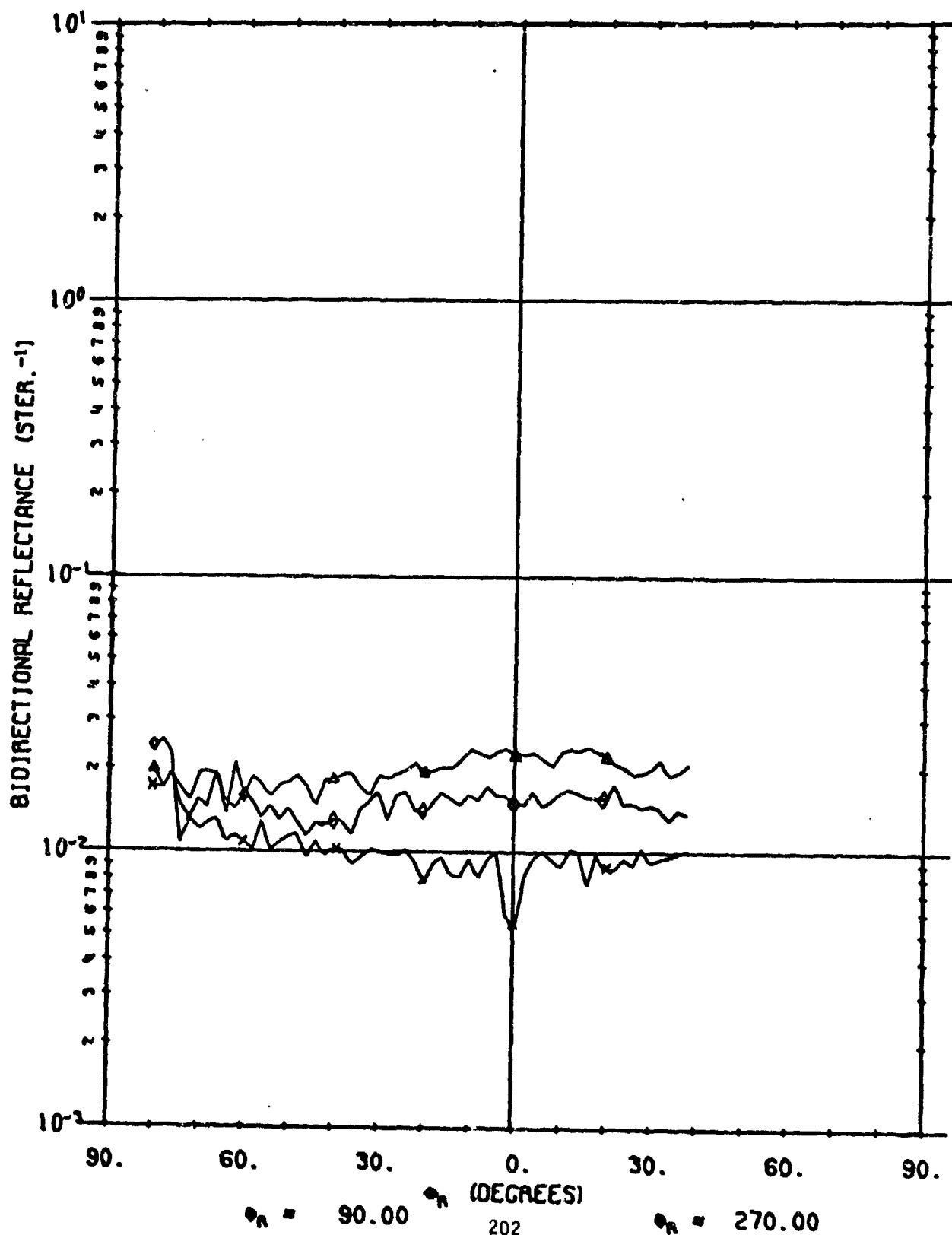
$\lambda = 10.60$   
 $\phi_i = 40.0$   
 $\phi_f = 180.0$



MUCVCC

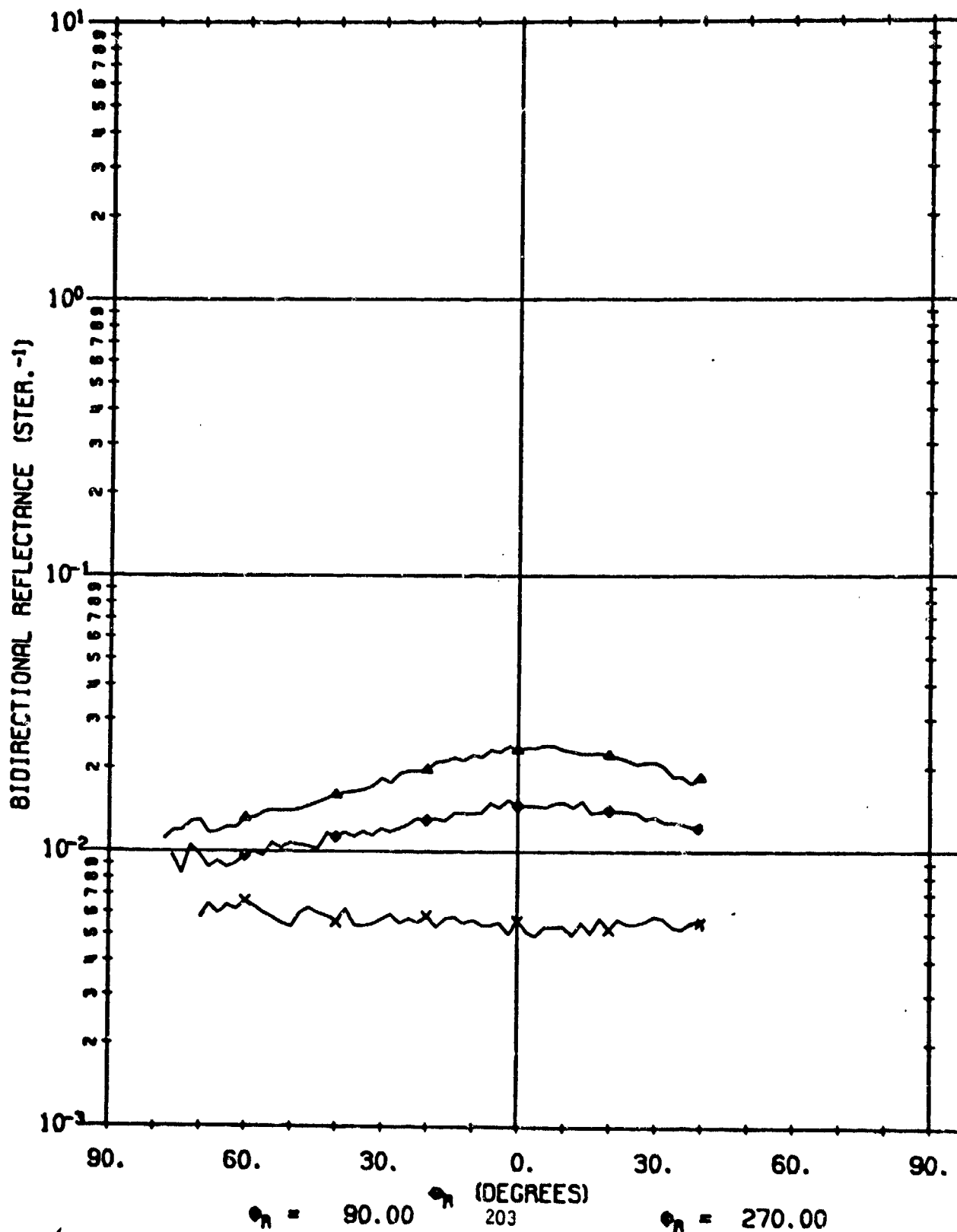
CVC

$\lambda = .63$   
 $\phi_1 = 40.0$   
 $\phi_2 = 180.0$



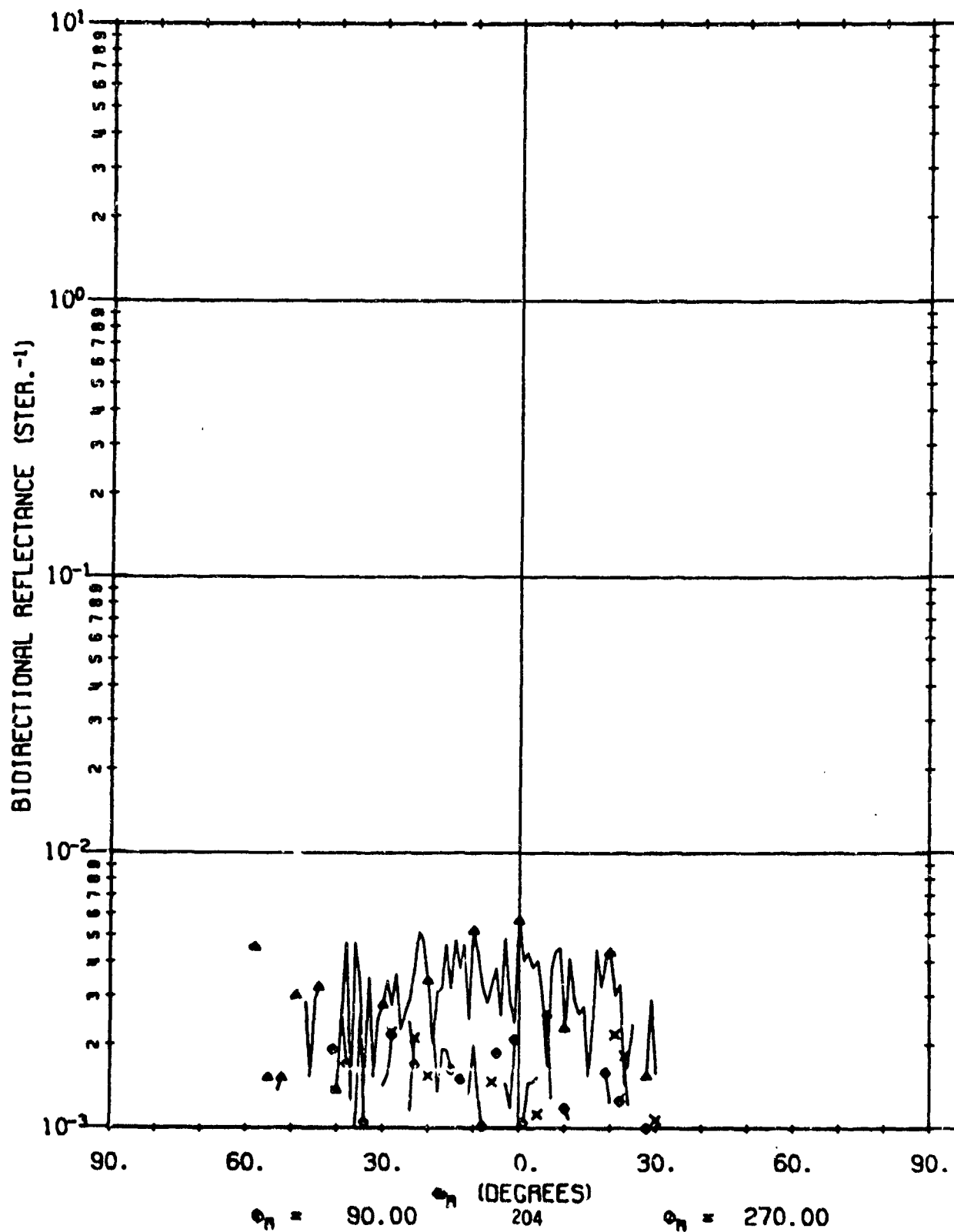
A02022 201

$\lambda = 1.06$   
 $\phi_i = 40.0$   
 $\phi_j = 180.0$



A02022 701

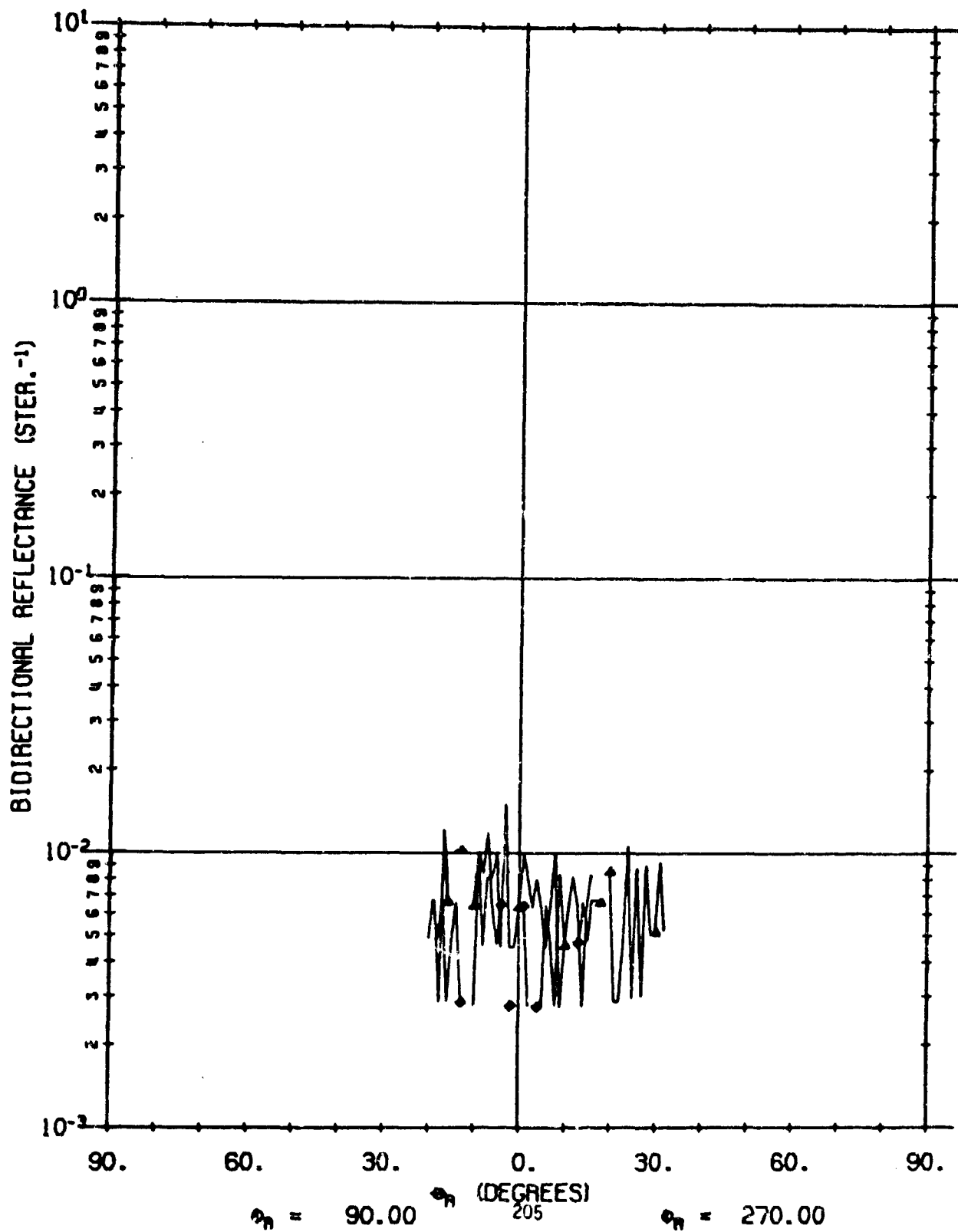
$\lambda = 3.39$   
 $\phi_i = 40.0$   
 $\phi_i = 180.0$



A02022

604

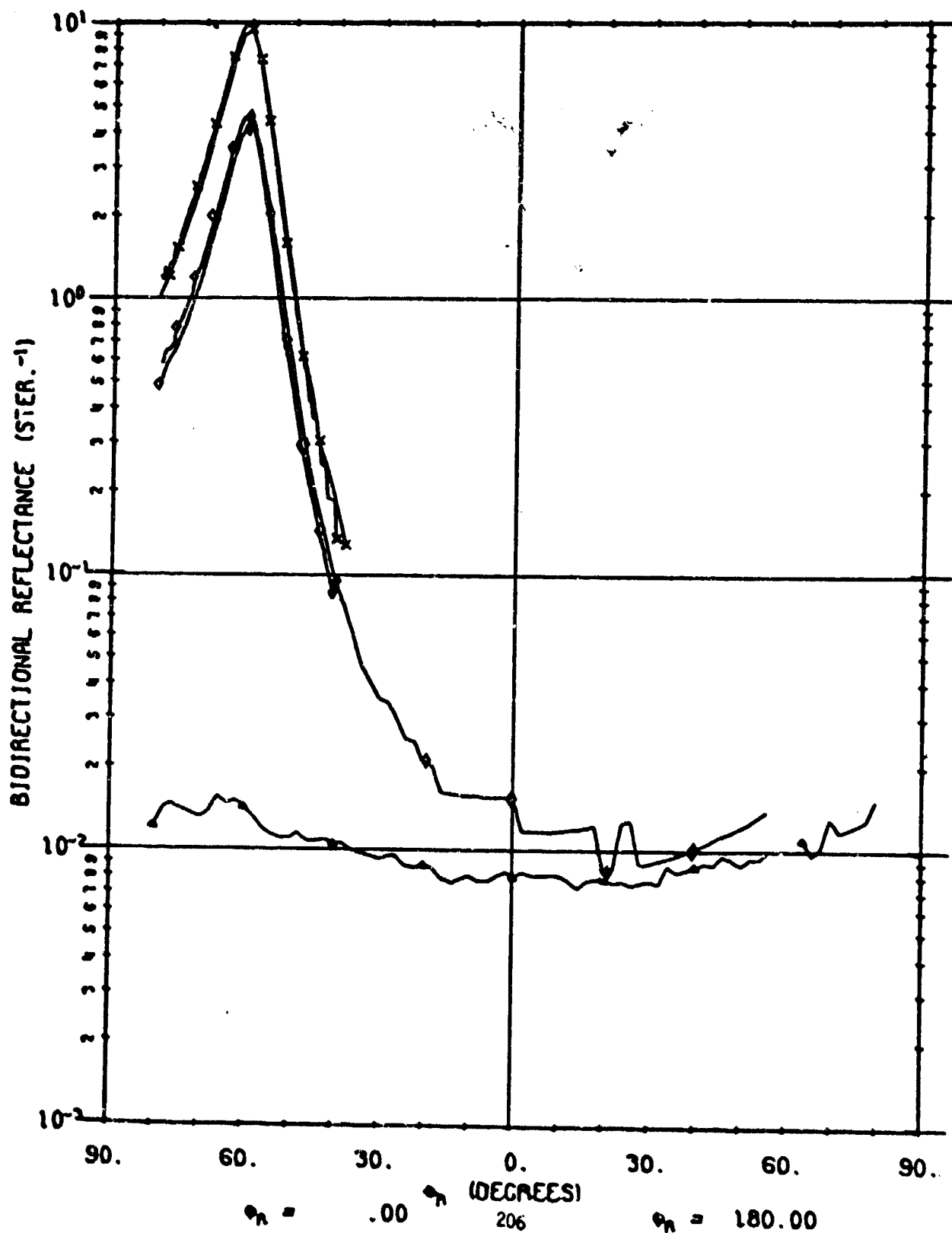
$\lambda = 10.60$   
 $\phi_i = 40.0$   
 $\phi_r = 180.0$





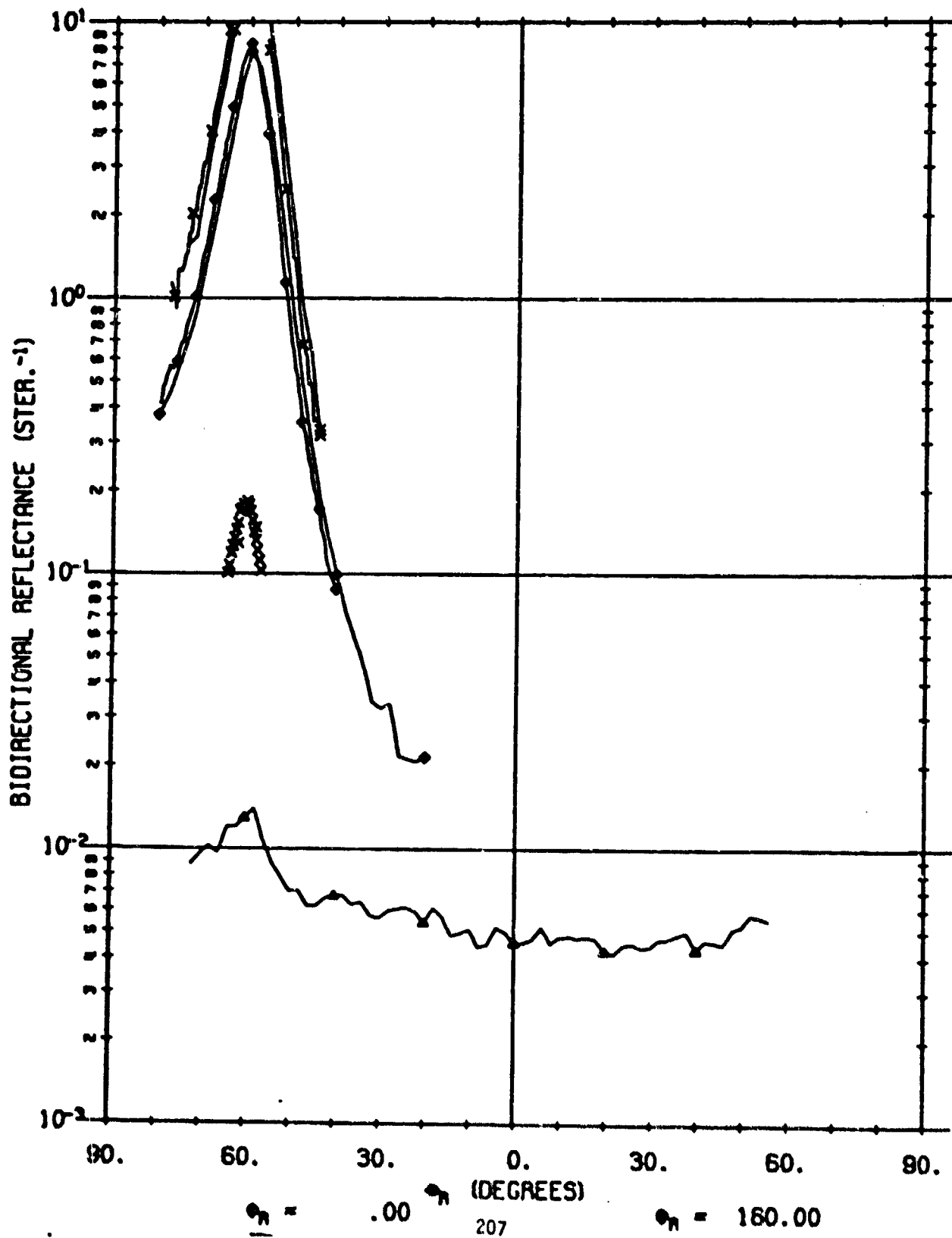
A02022 202

$\lambda = .63$   
 $\phi_i = 60.0$   
 $\phi_f = 180.0$



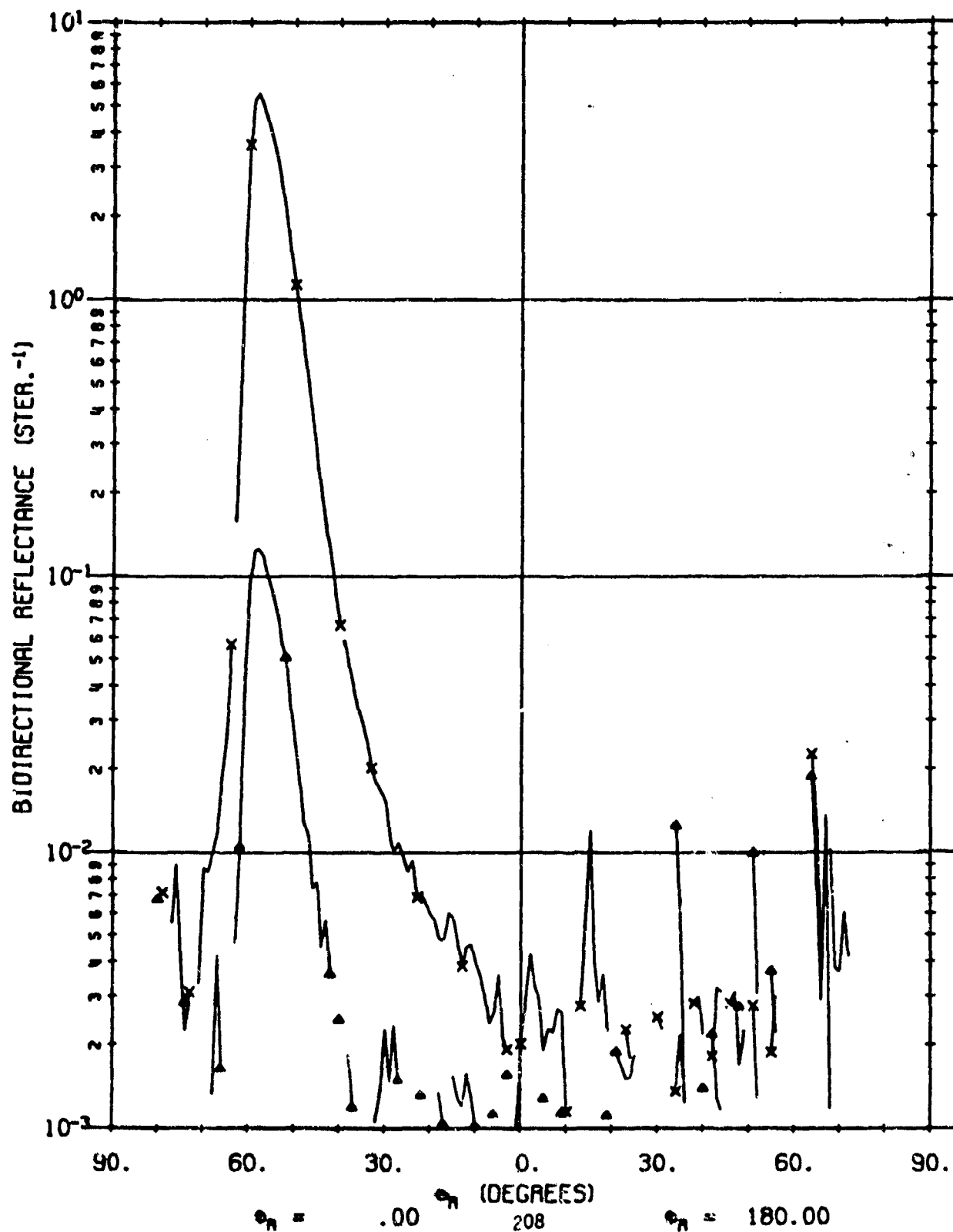
A02022 201

$\lambda = 1.06$   
 $\phi_1 = 60.0$   
 $\phi_2 = 180.0$



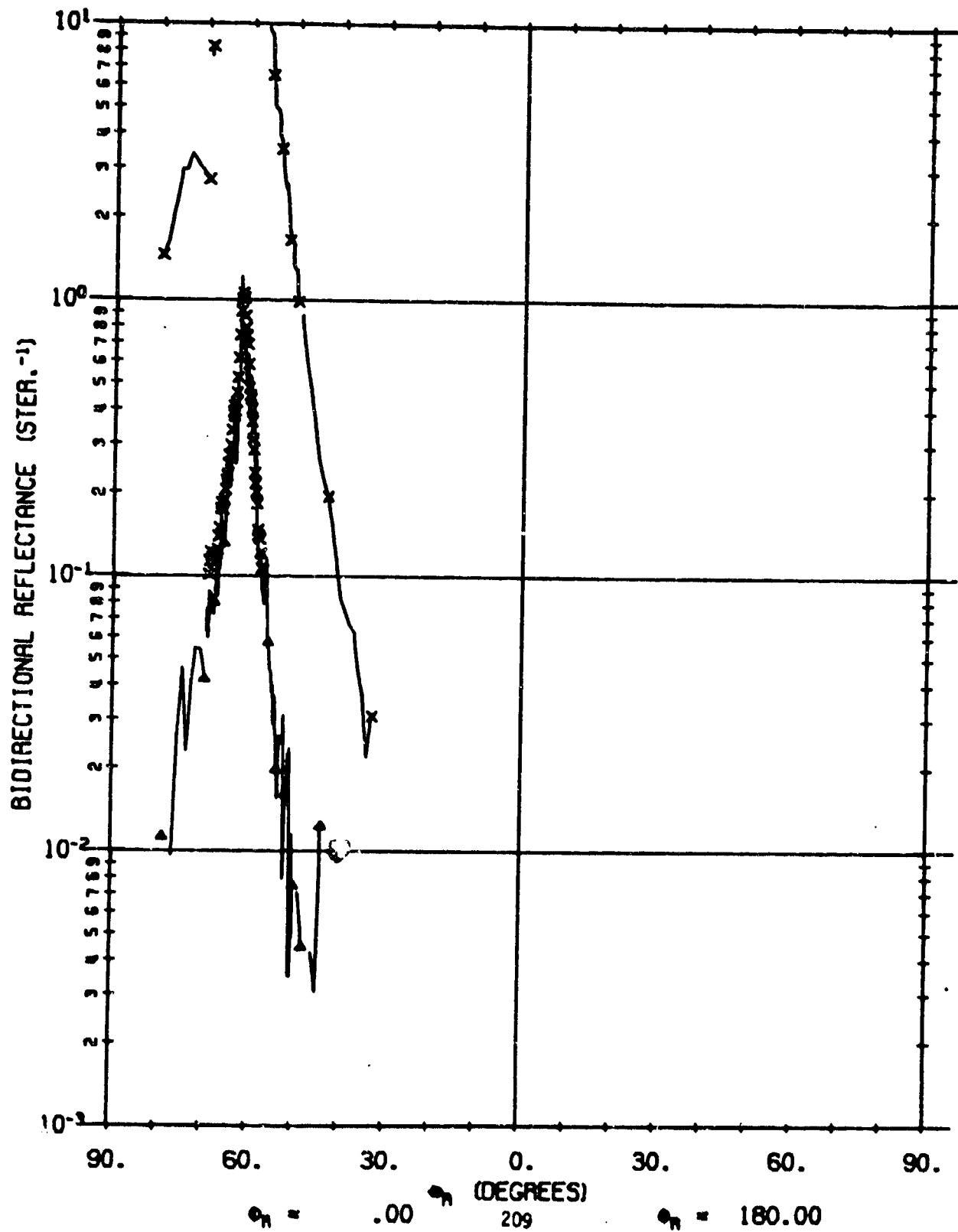
A02022 702

$\lambda = 3.39$   
 $\phi_1 = 60.0$   
 $\phi_2 = 180.0$



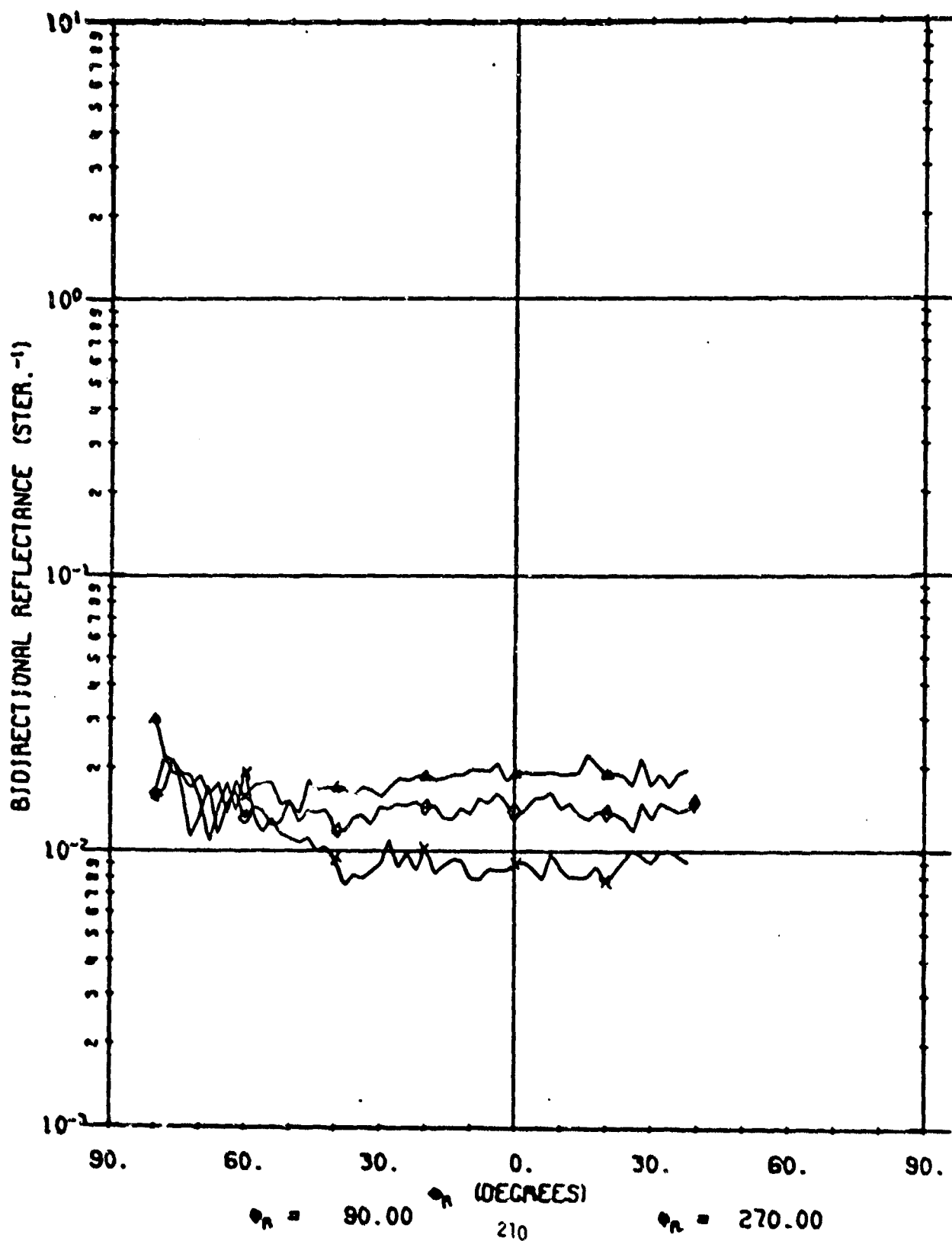
A02022 602

$\lambda = 10.60$   
 $\phi_i = 60.0$   
 $\phi_t = 180.0$



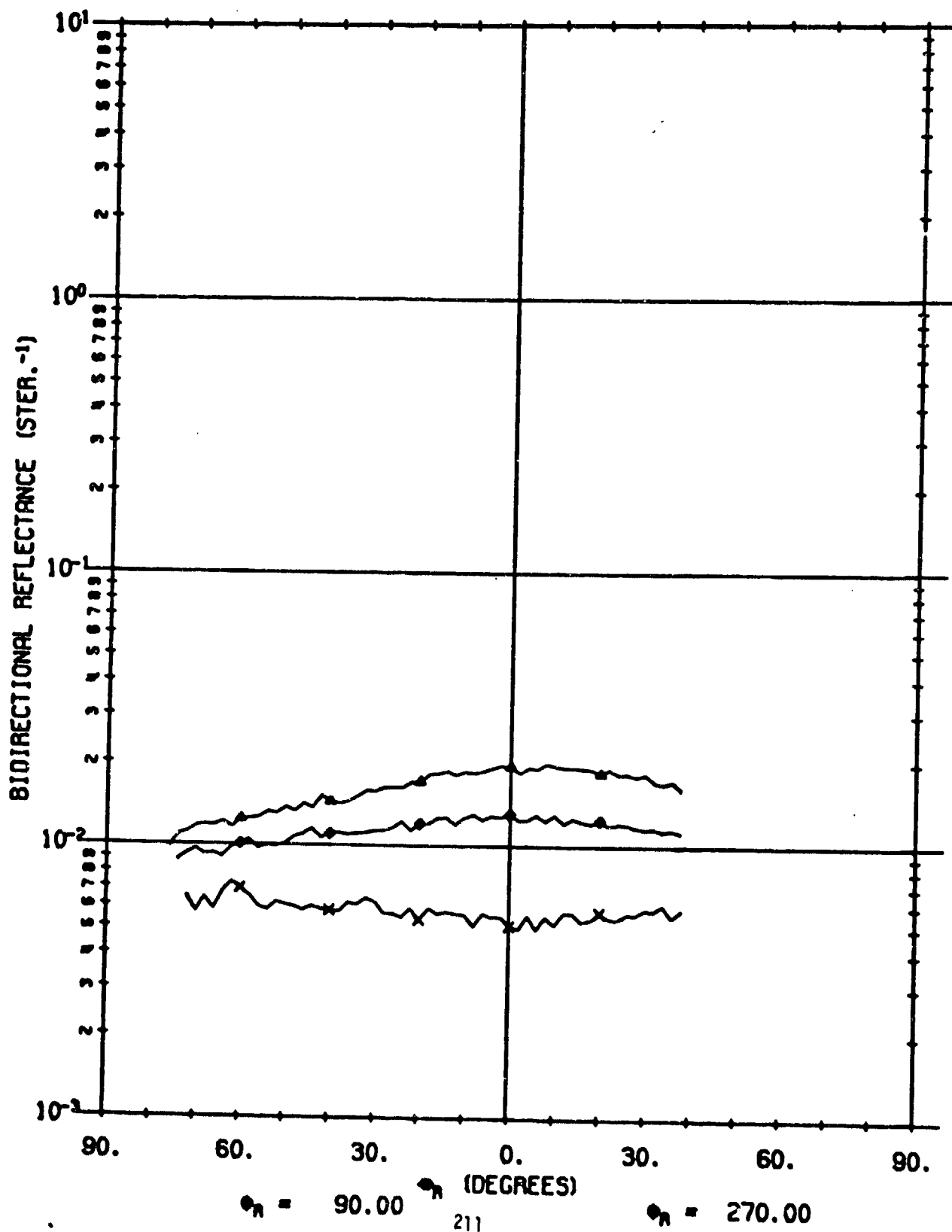
A02022 202

$\lambda = .63$   
 $\phi_i = 60.0$   
 $\phi_f = 180.0$



A02022 201

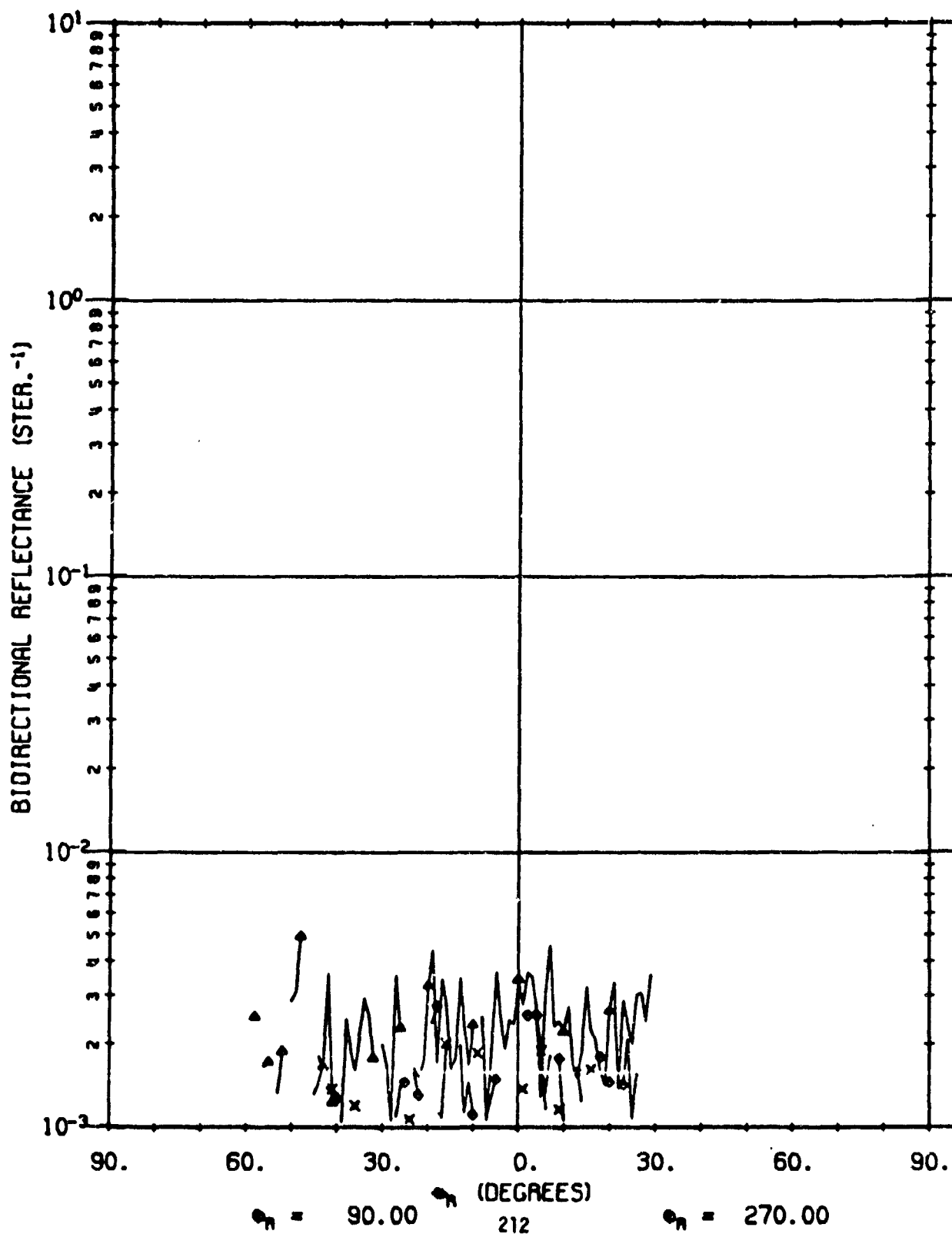
$\lambda = 1.06$   
 $\phi_i = 60.0$   
 $\phi_j = 180.0$



A02022 701

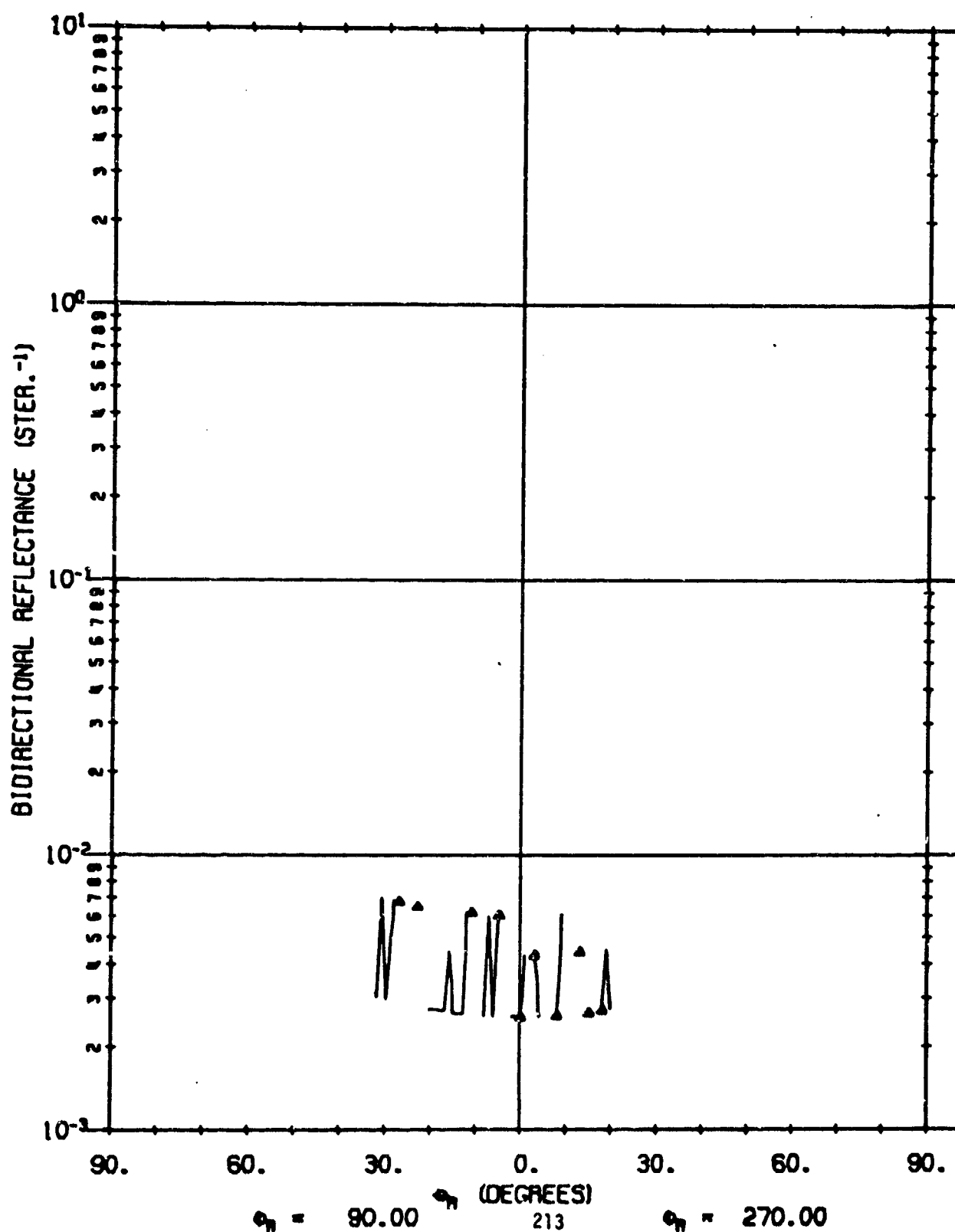
$\lambda = 3.39$   
 $\phi_i = 60.0$   
 $\phi_i = 180.0$

82



A02022 604

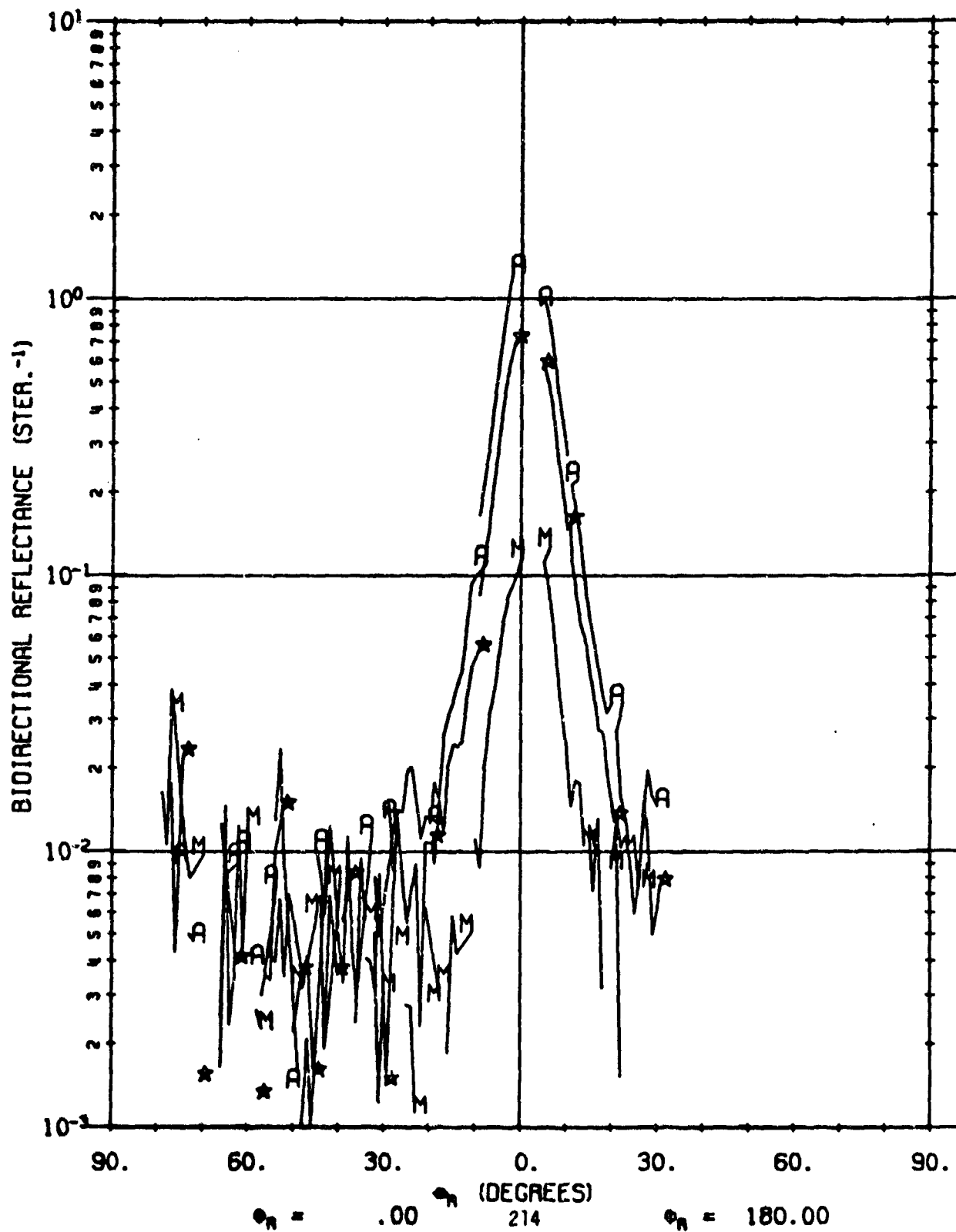
$\lambda = 10.60$   
 $\phi_i = 60.0$   
 $\phi_t = 180.0$





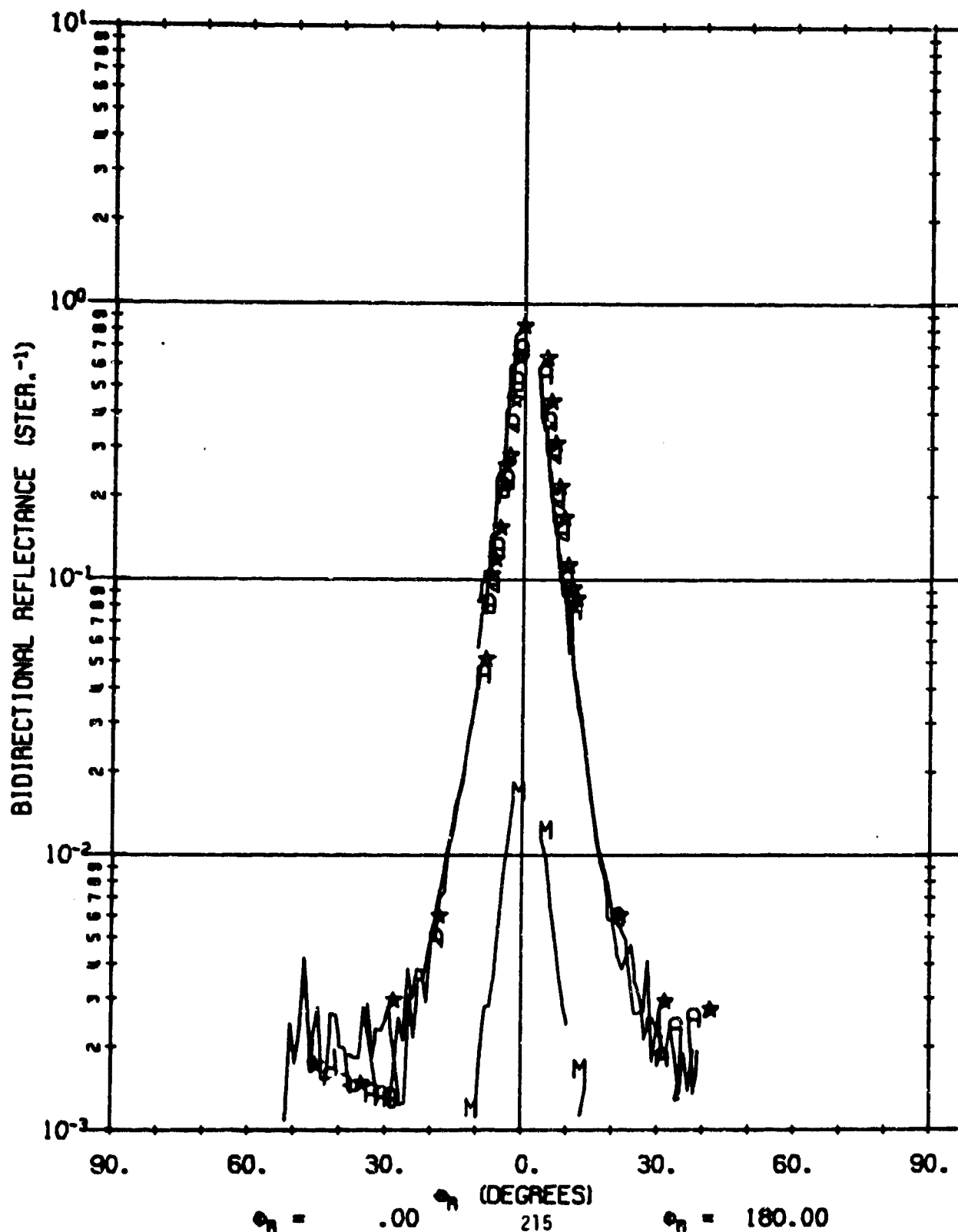
A02022 703

$\lambda = 3.39$   
 $\phi_1 = .0$   
 $\phi_2 = 180.0$



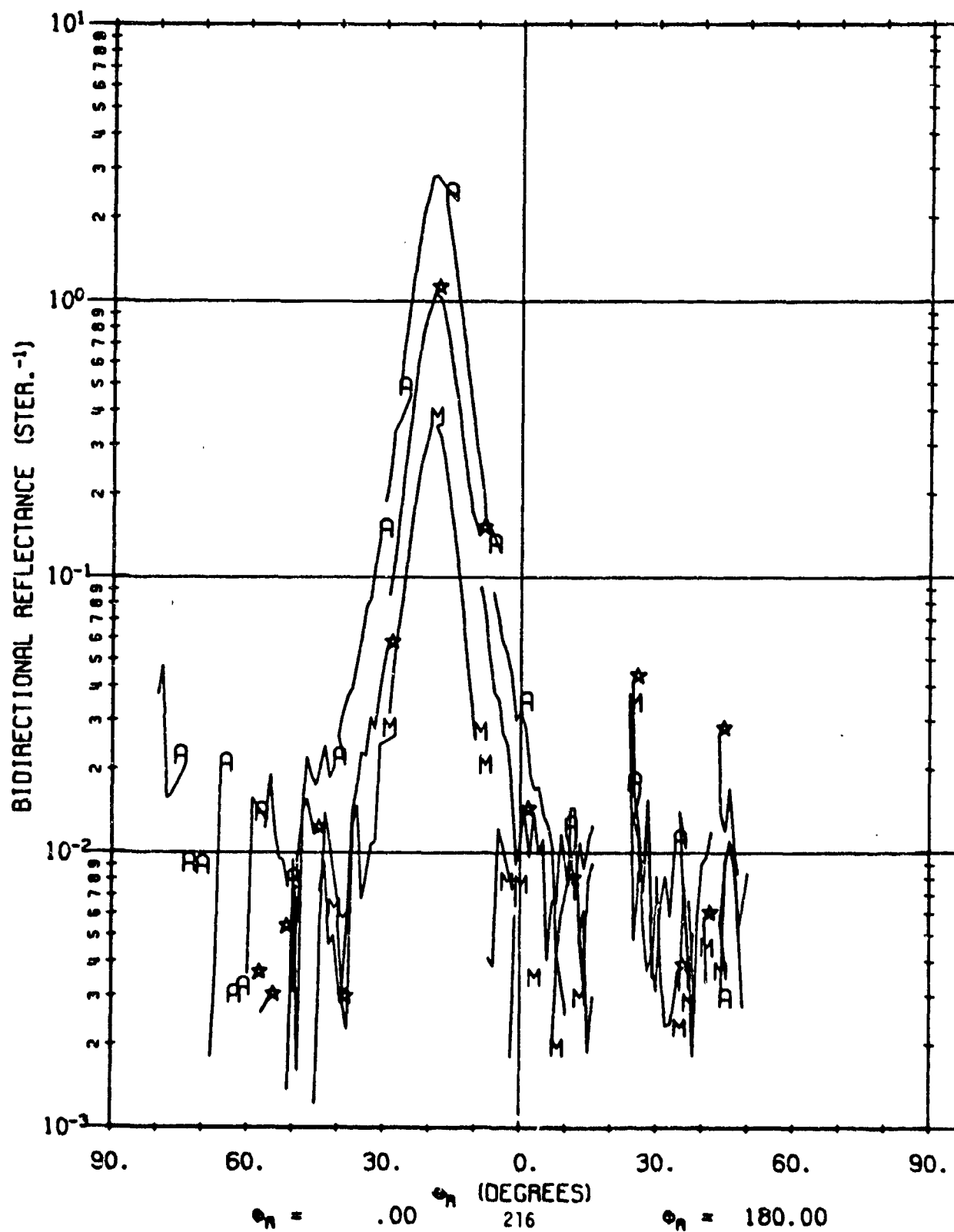
A02022 603

$\lambda = 10.60$   
 $\phi_i = 0$   
 $\phi_f = 180.0$



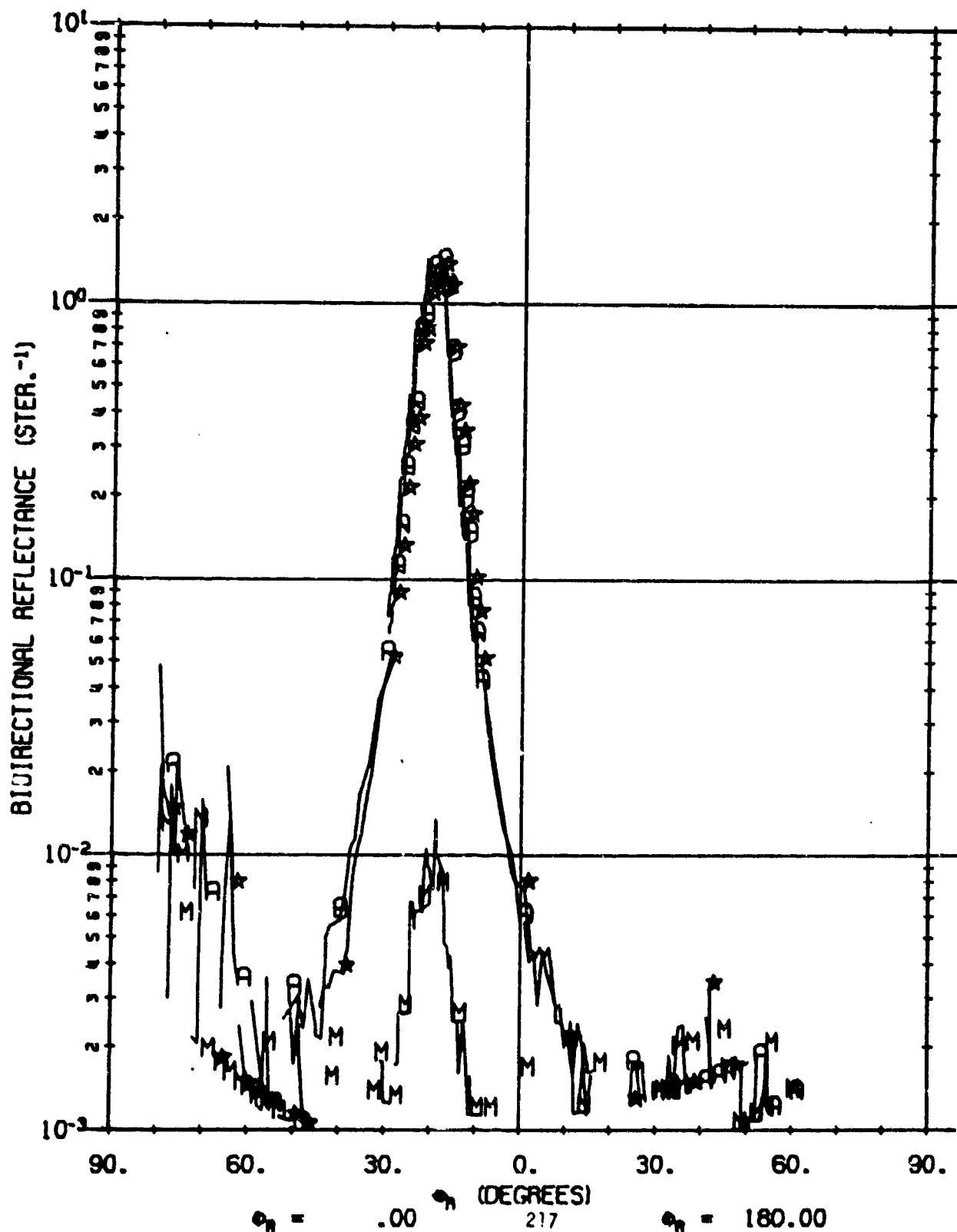
A02022 703

$\lambda = 3.39$   
 $\phi_i = 20.0$   
 $\phi_f = 180.0$



A02022 603

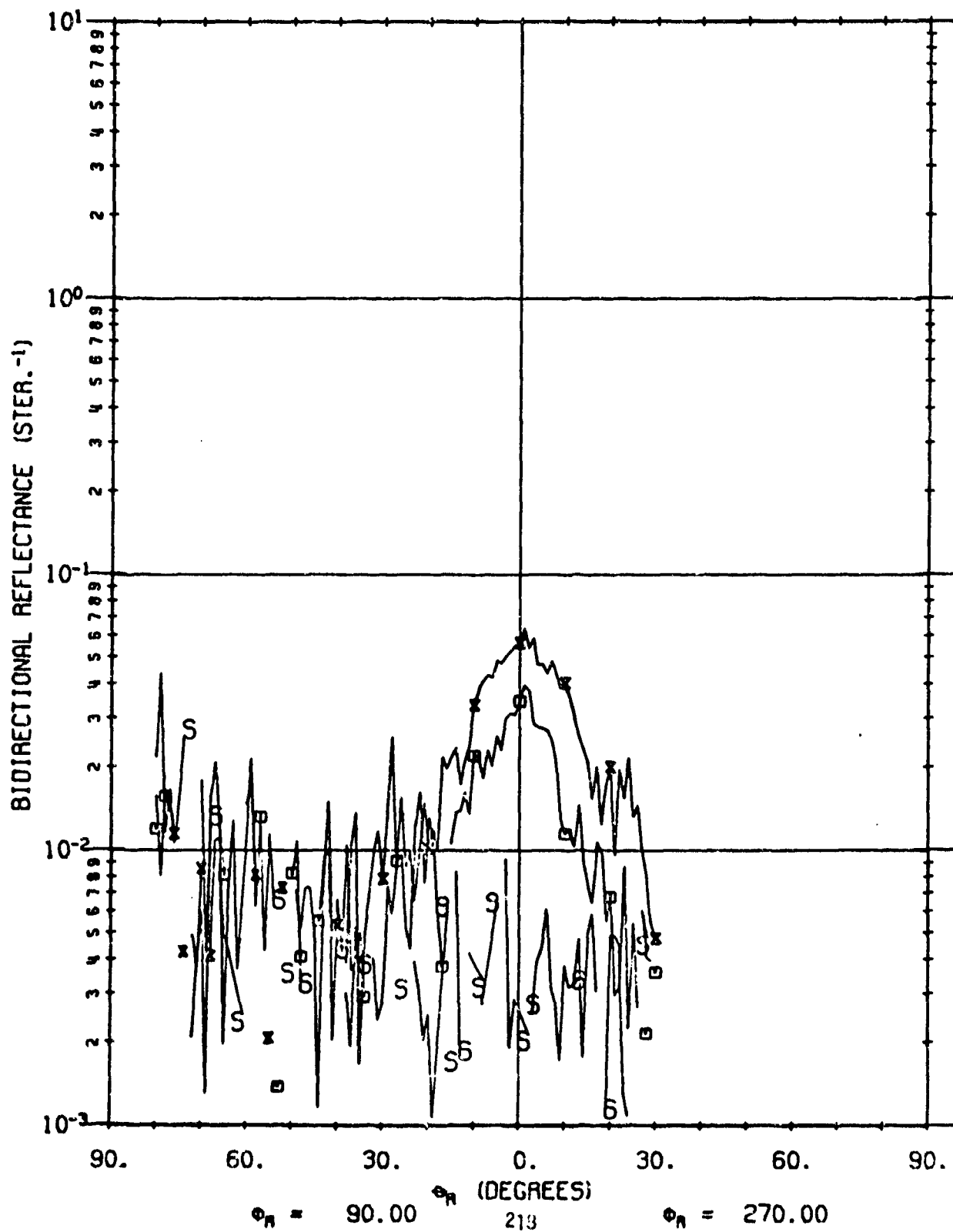
$\lambda = 10.60$   
 $\phi_i = 20.0$   
 $\phi_f = 180.0$



$\phi_n = .00$   $\phi_n = 180.00$

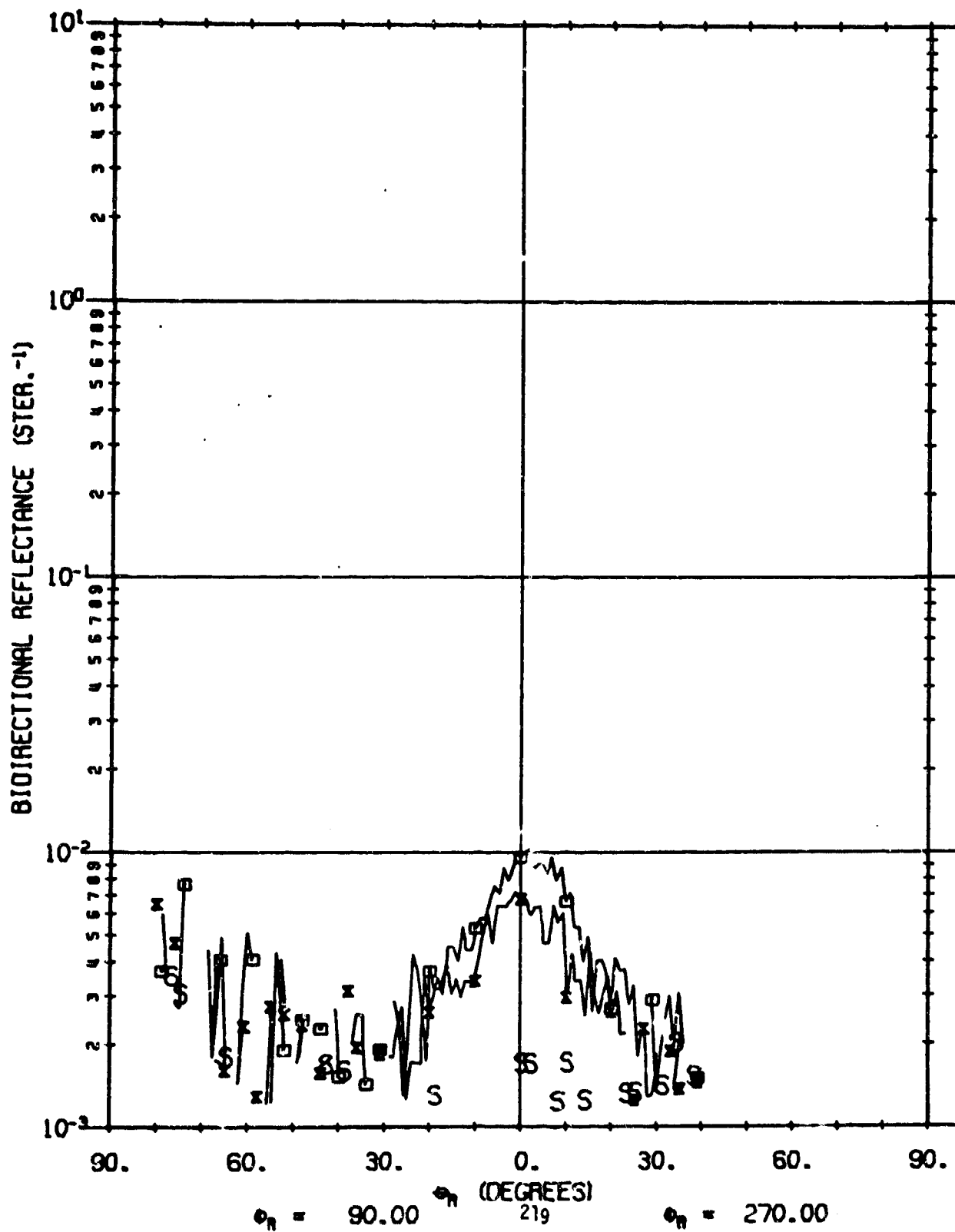
A02022 703

$\lambda = 3.39$   
 $\phi_i = 20.0$   
 $\phi_i = 180.0$



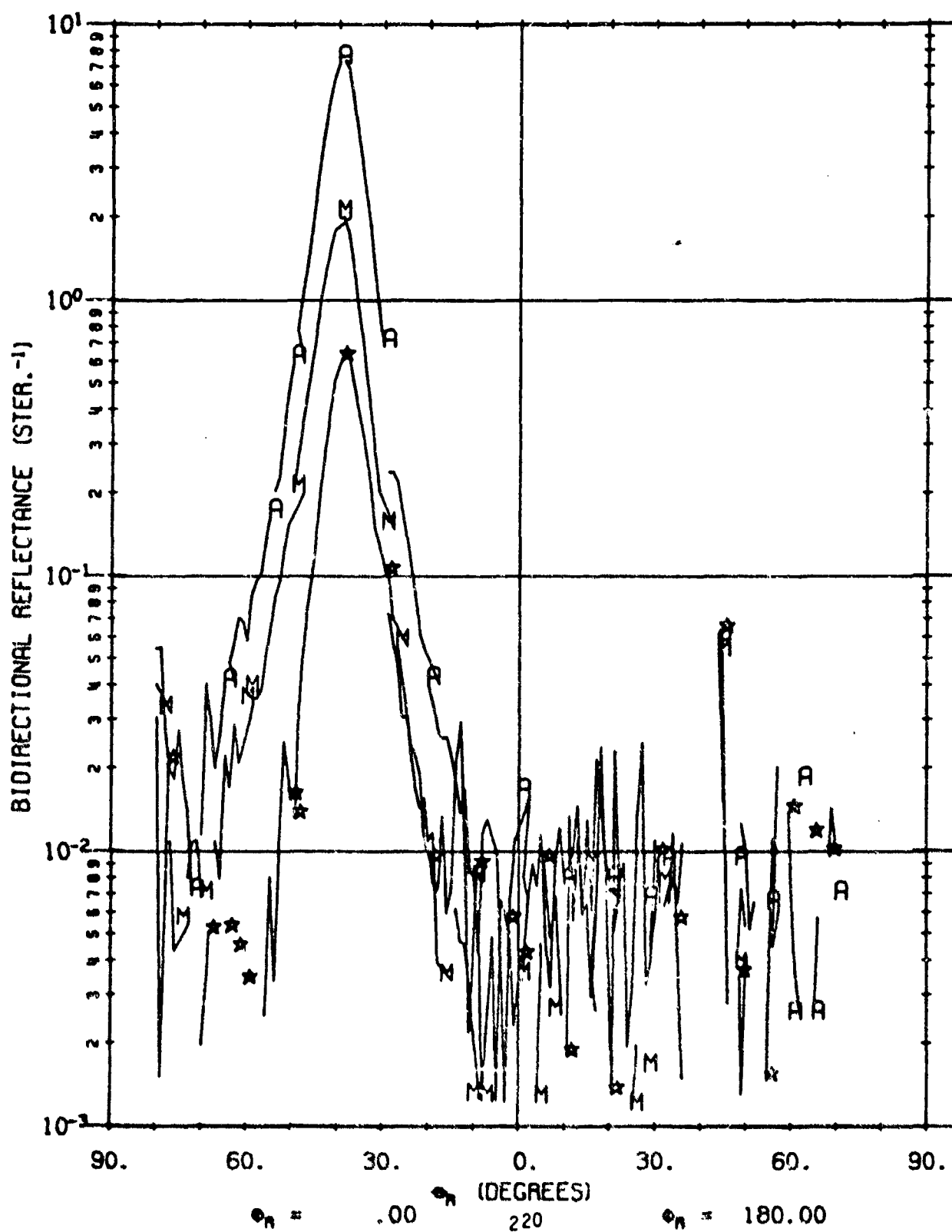
A02022 603

$\lambda = 10.60$   
 $\phi_i = 20.0$   
 $\phi_t = 180.0$



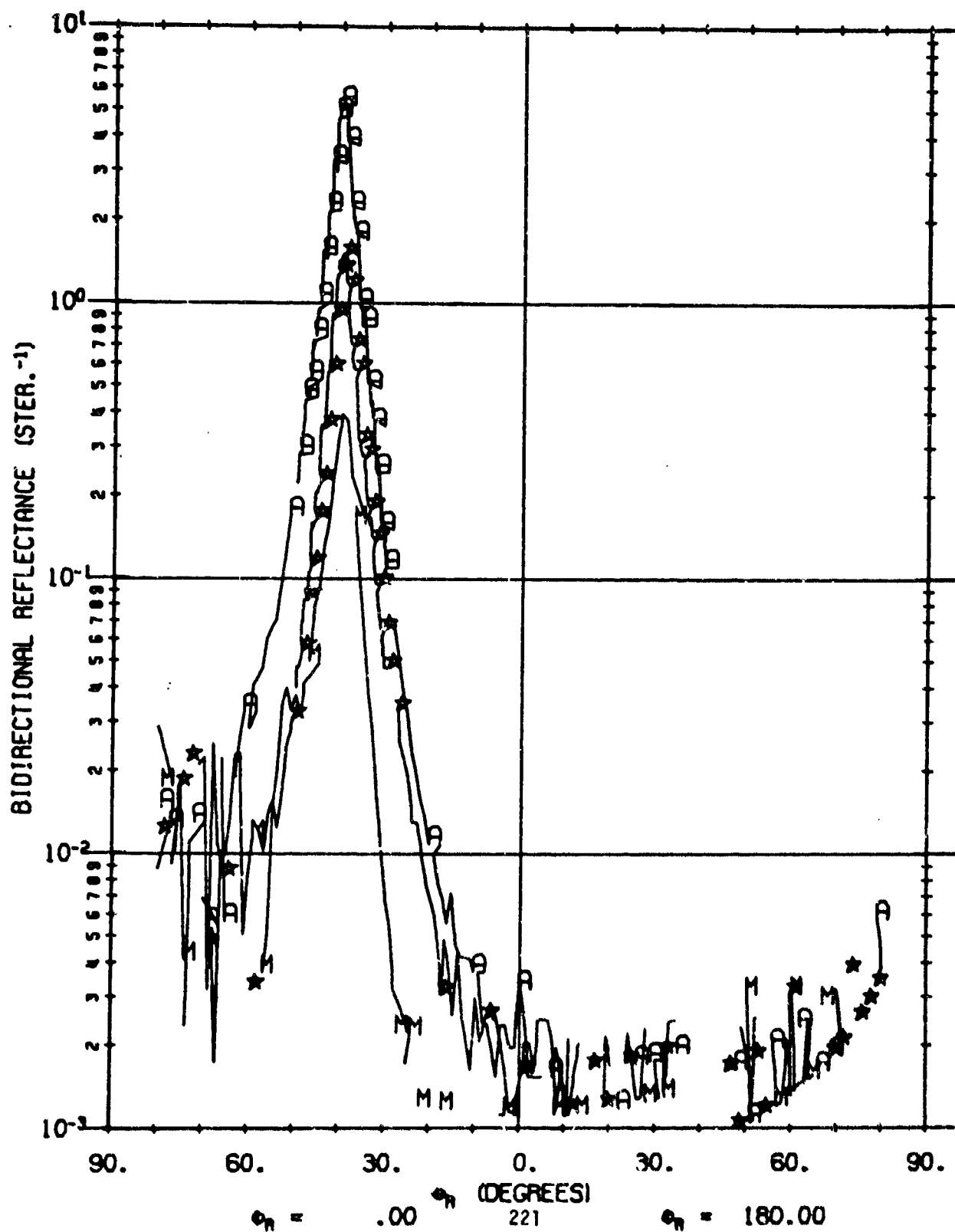
A02022 703

$\lambda = 3.39$   
 $\phi_i = 40.0$   
 $\phi_f = 180.0$



A02022 603

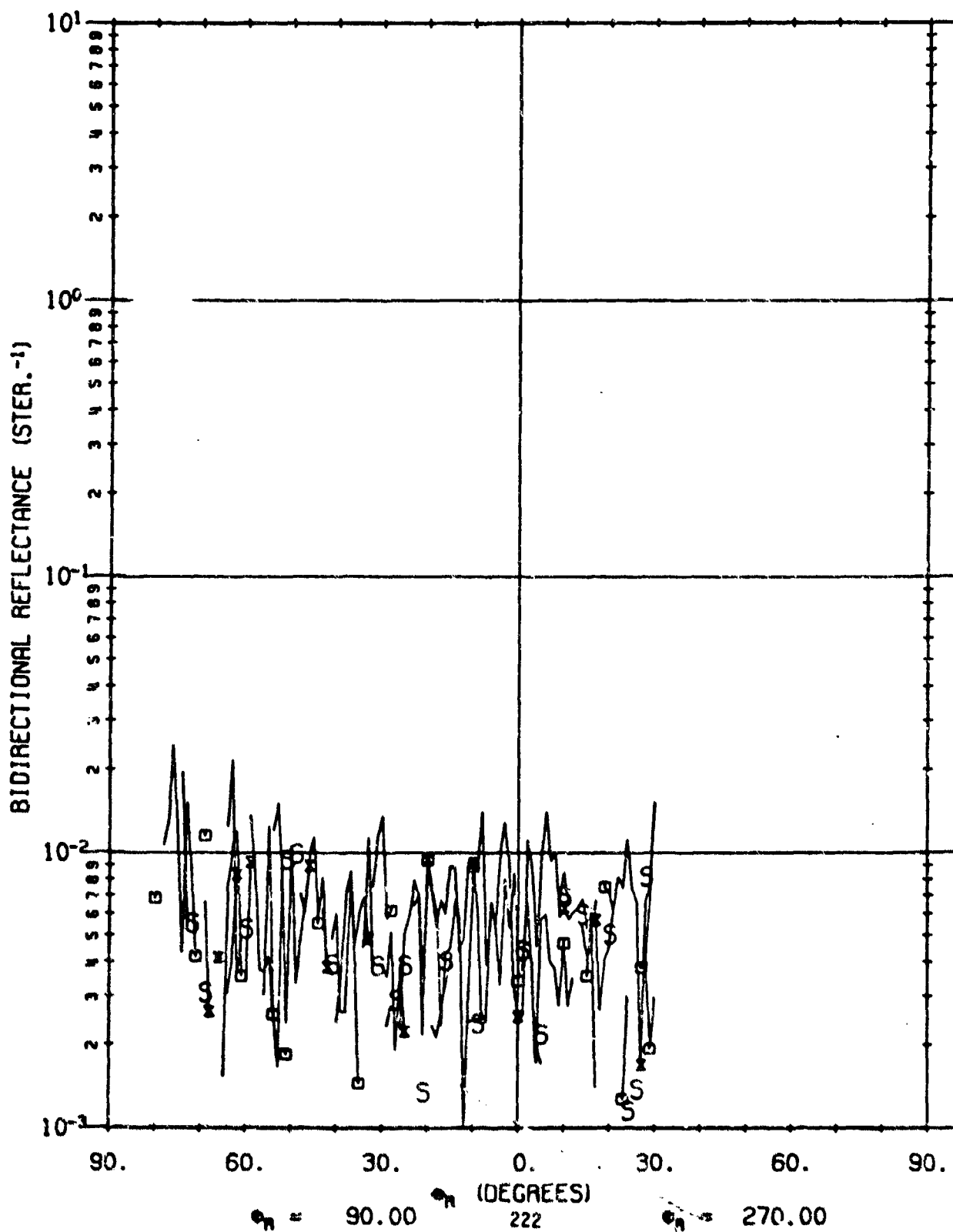
$\lambda = 10.60$   
 $\phi_i = 40.0$   
 $\phi_f = 180.0$





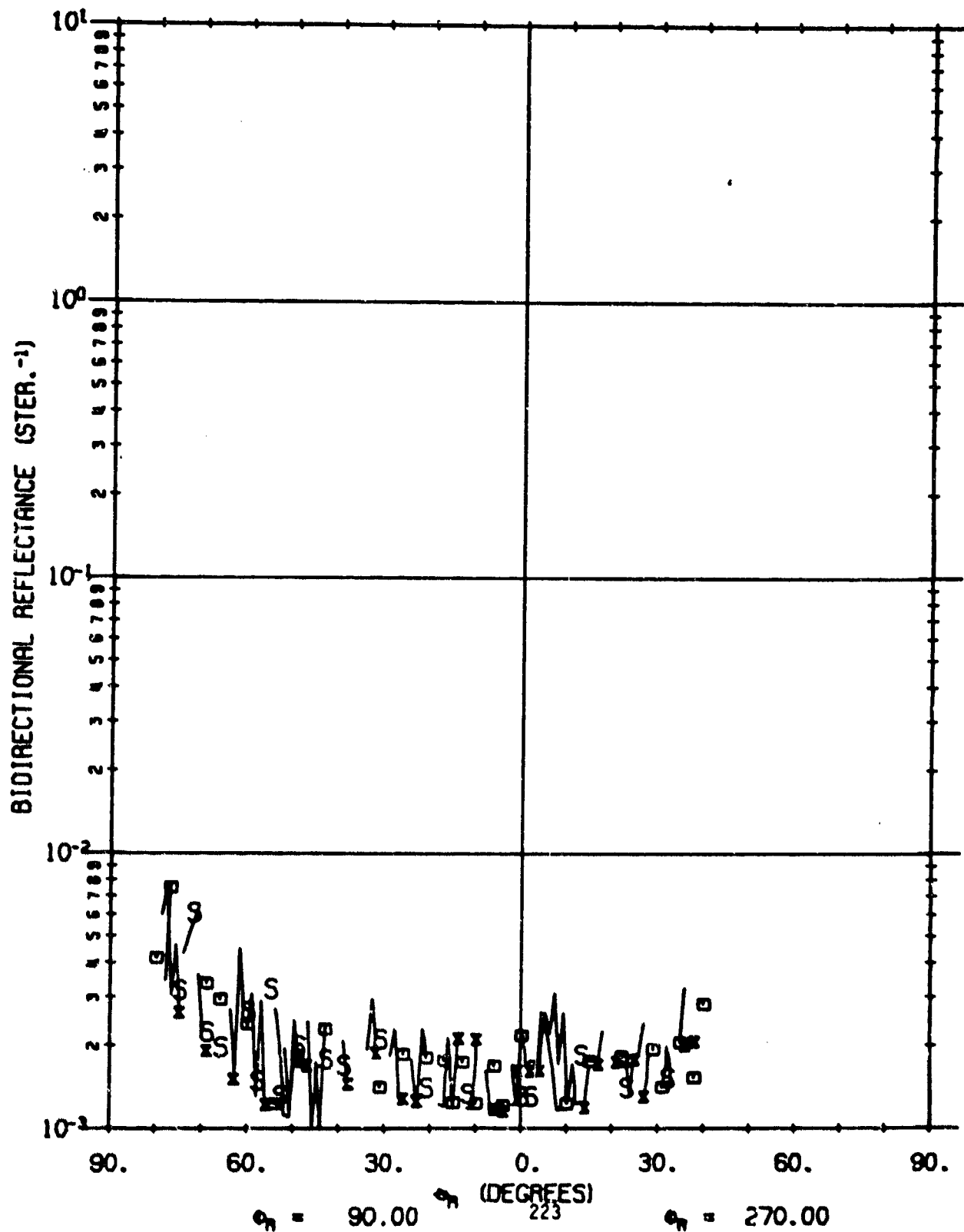
A02022 703

$\lambda$  = 3.39  
 $\phi_1$  = 40.0  
 $\phi_2$  = 180.0



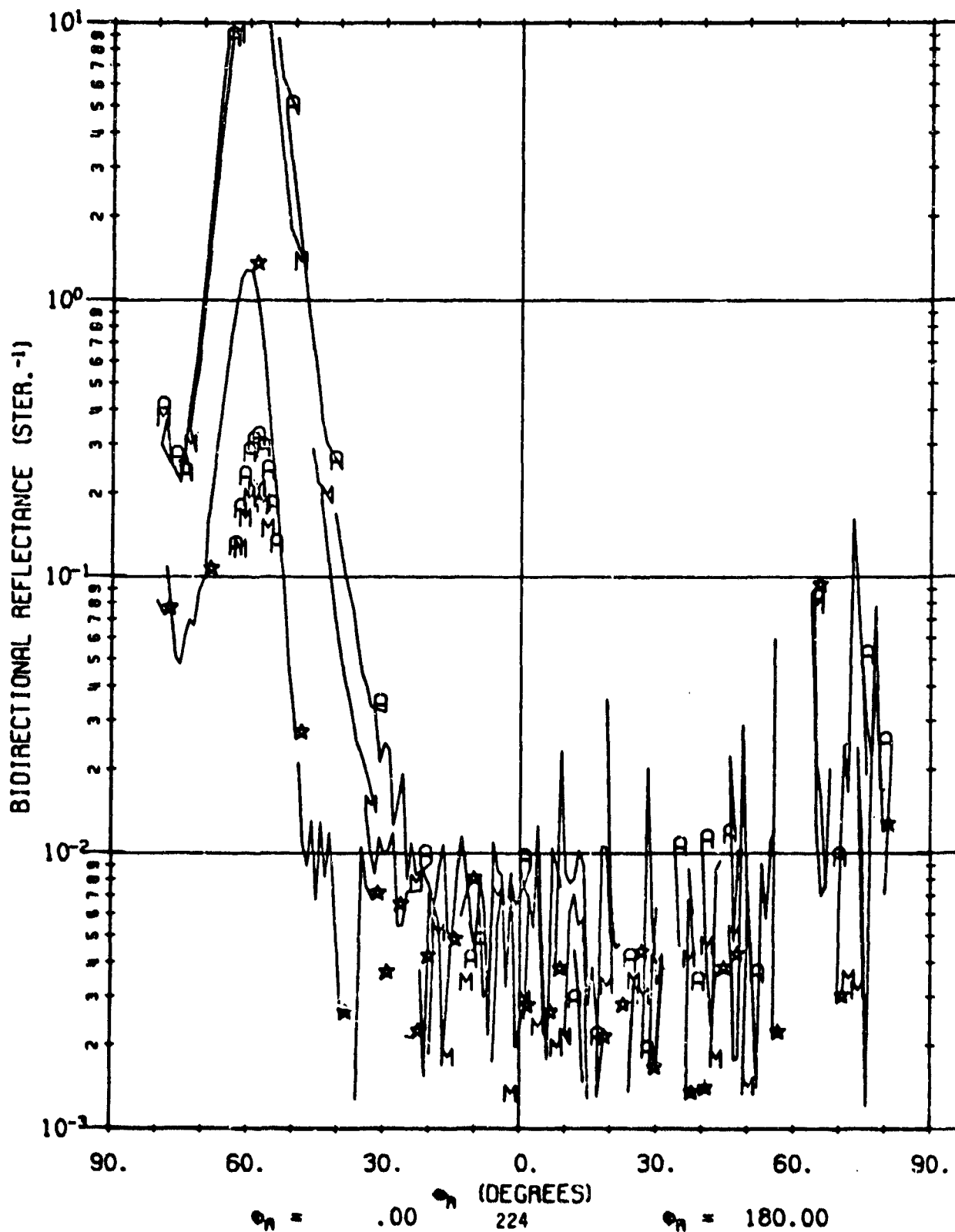
A02022 603

$\lambda = 10.60$   
 $\phi_i = 40.0$   
 $\phi_f = 180.0$



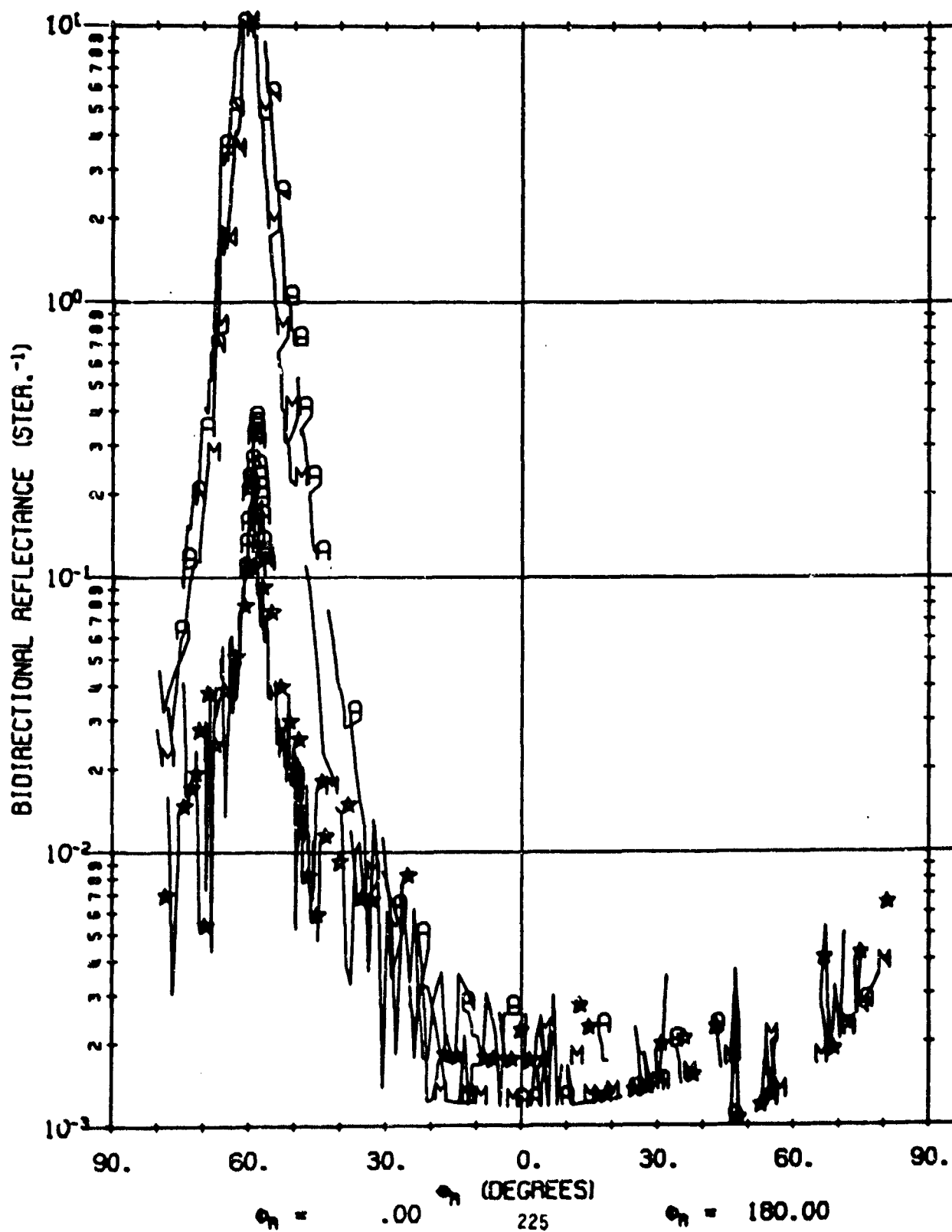
A02022 703

$\lambda = 3.39$   
 $\phi_i = 60.0$   
 $\phi_r = 180.0$



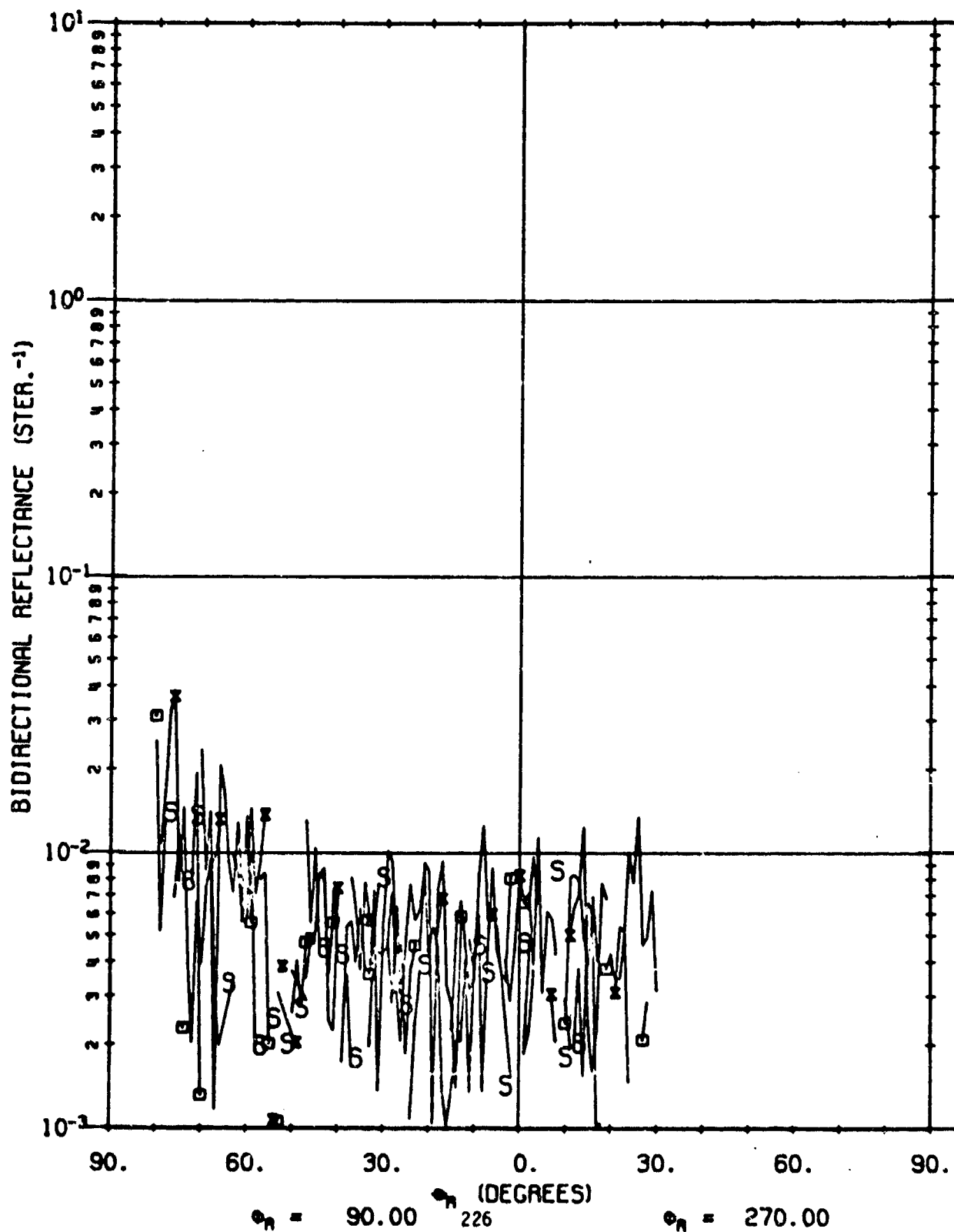
A02022 603

$\lambda = 10.60$   
 $\phi_i = 60.0$   
 $\phi_f = 180.0$



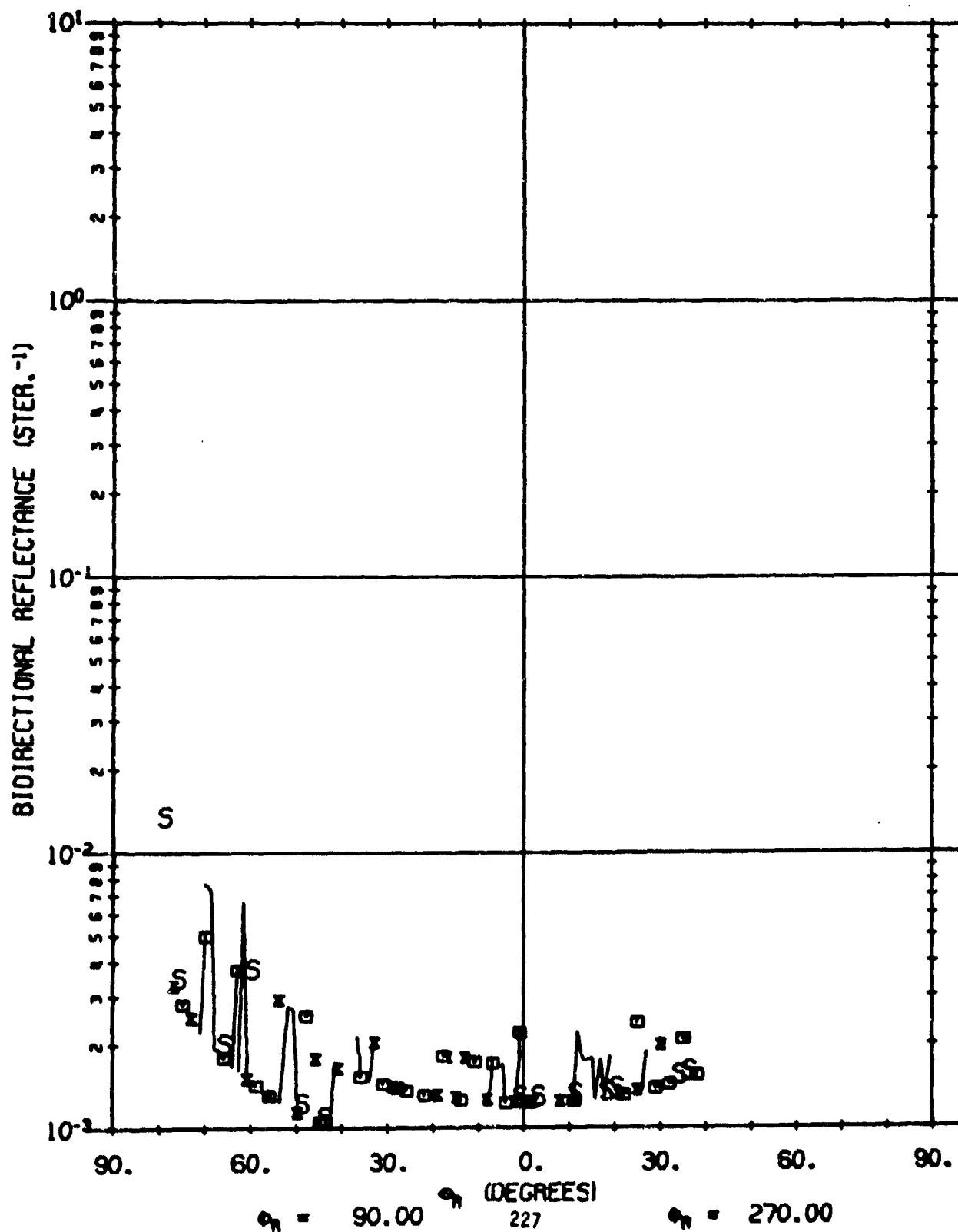
A02022 703

$\lambda = 3.39$   
 $\phi_1 = 60.0$   
 $\phi_2 = 180.0$



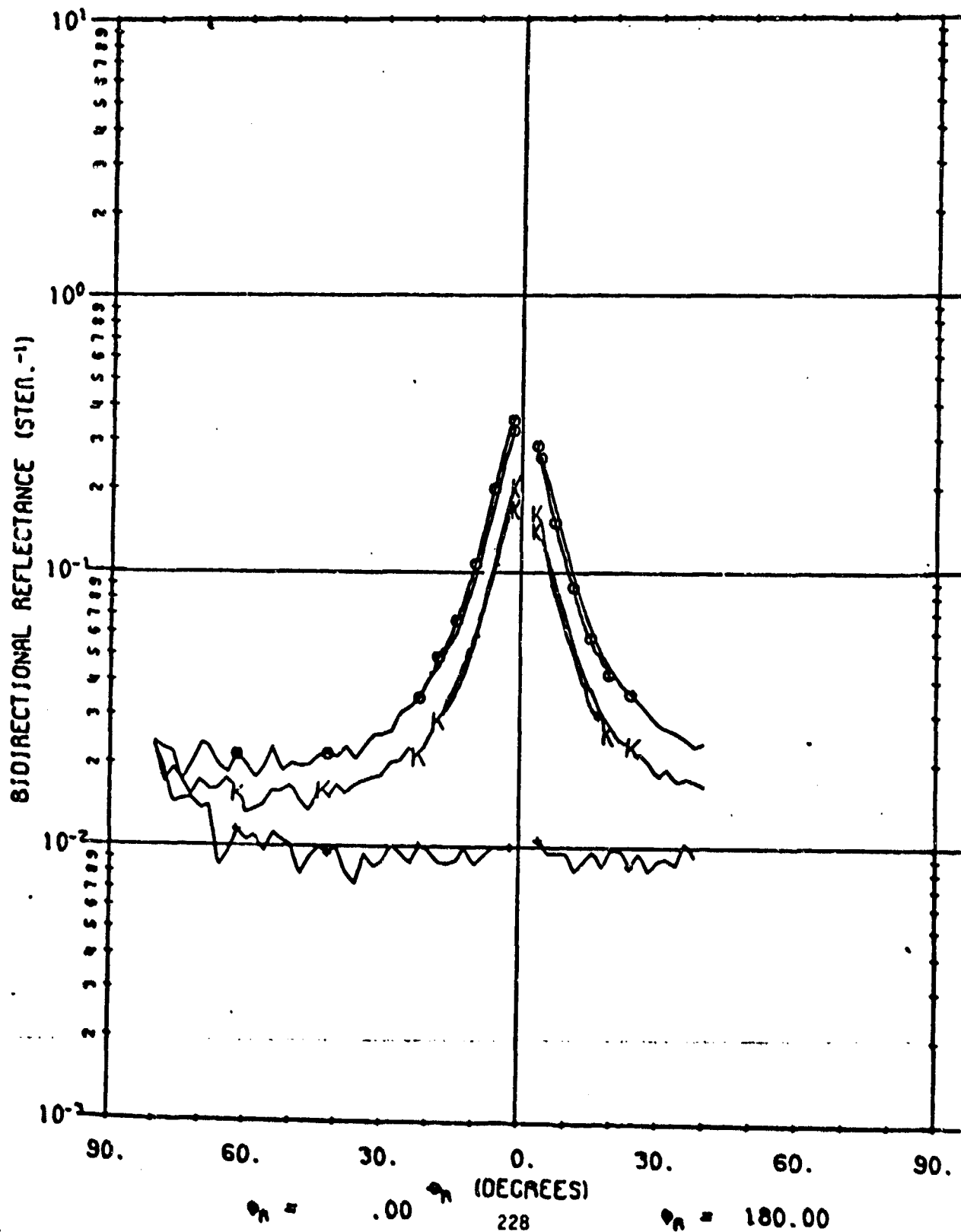
A02022 603

$\lambda = 10.60$   
 $\phi_i = 60.0$   
 $\phi_r = 180.0$



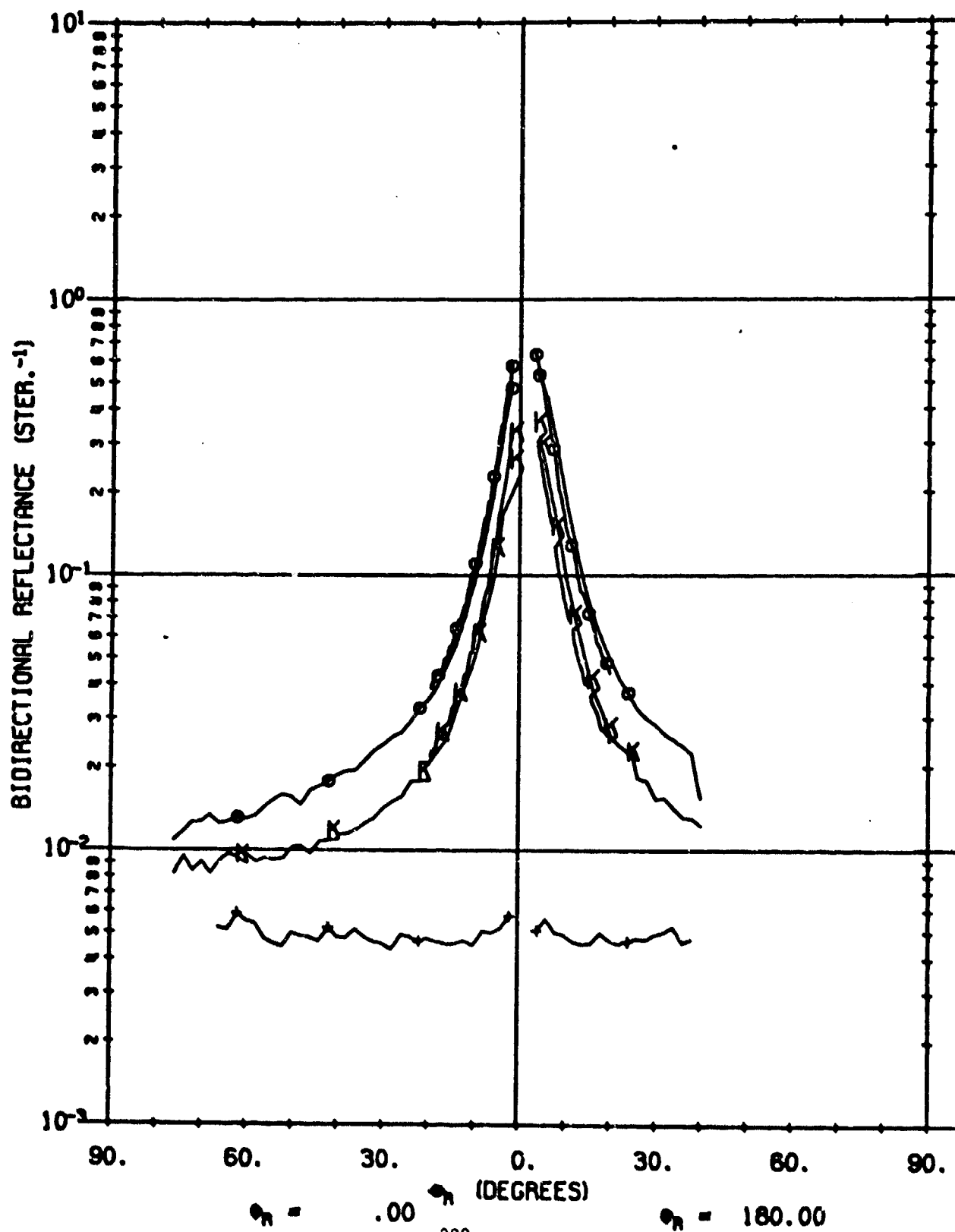
A02022 202

$\lambda = .63$   
 $\phi_i = .0$   
 $\phi_i = 180.0$



HUZEK 201

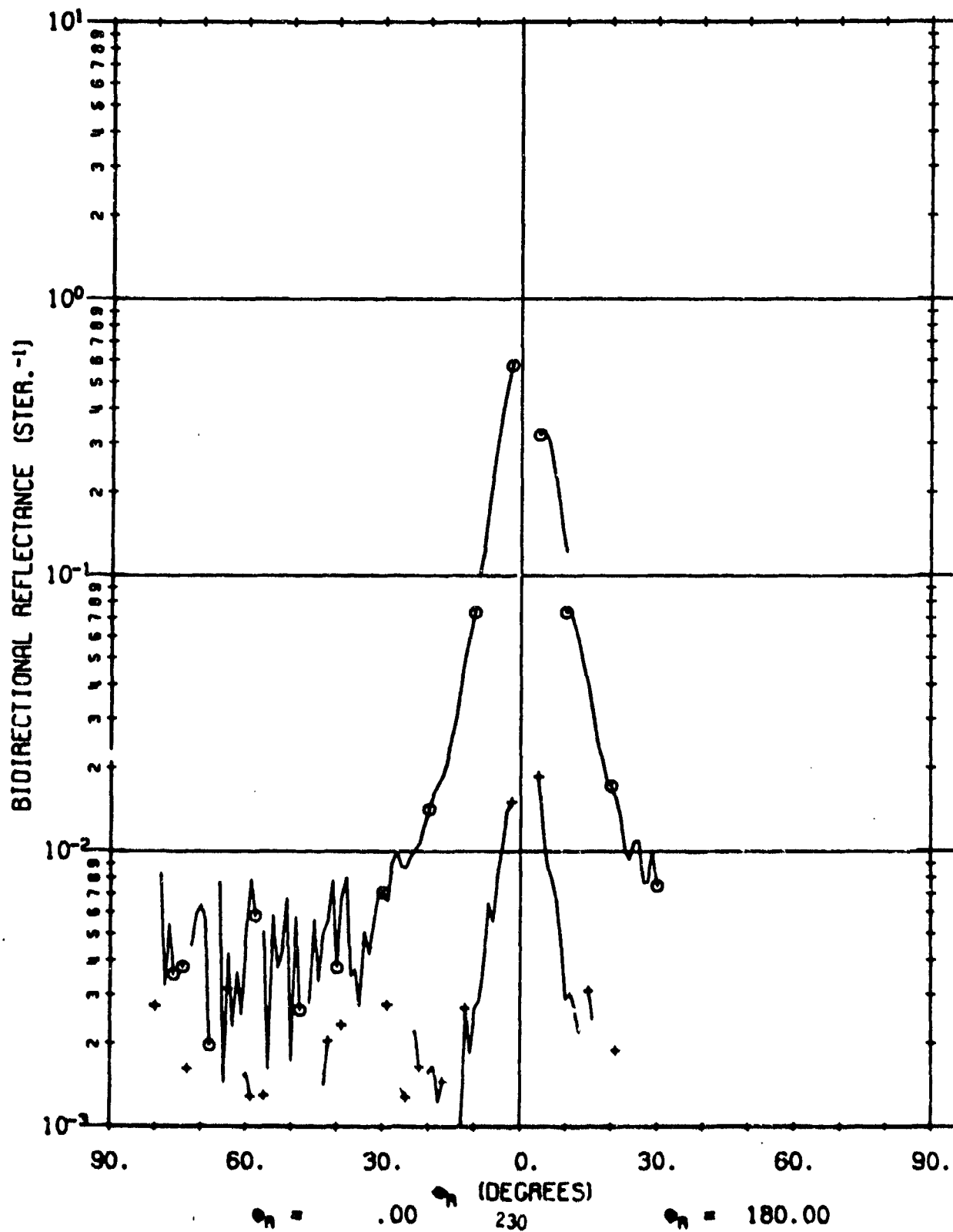
$\lambda = 1.06$   
 $\phi_1 = .0$   
 $\phi_2 = 180.0$





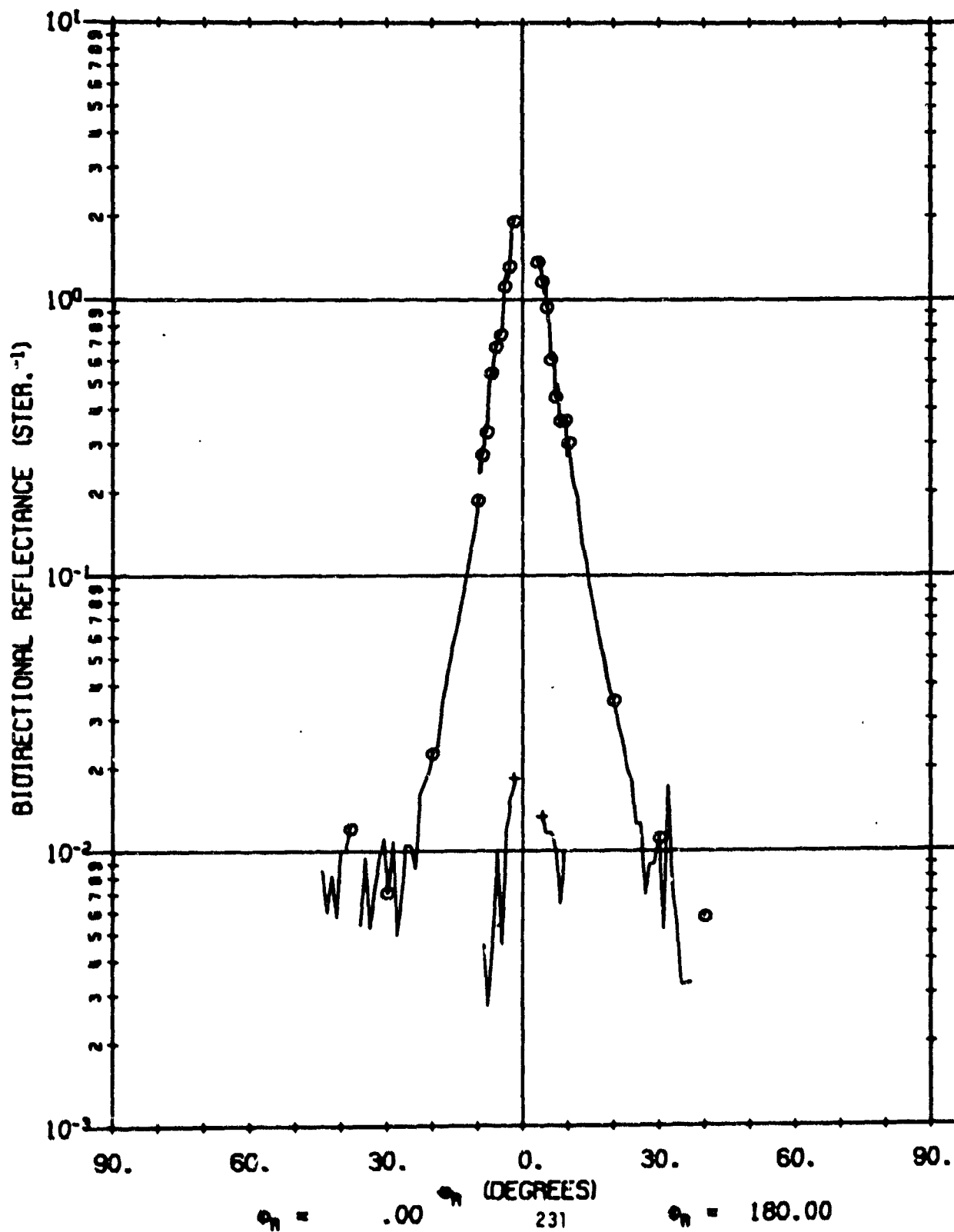
A02022 701

$\lambda = 3.39$   
 $\phi_1 = .0$   
 $\phi_2 = 180.0$



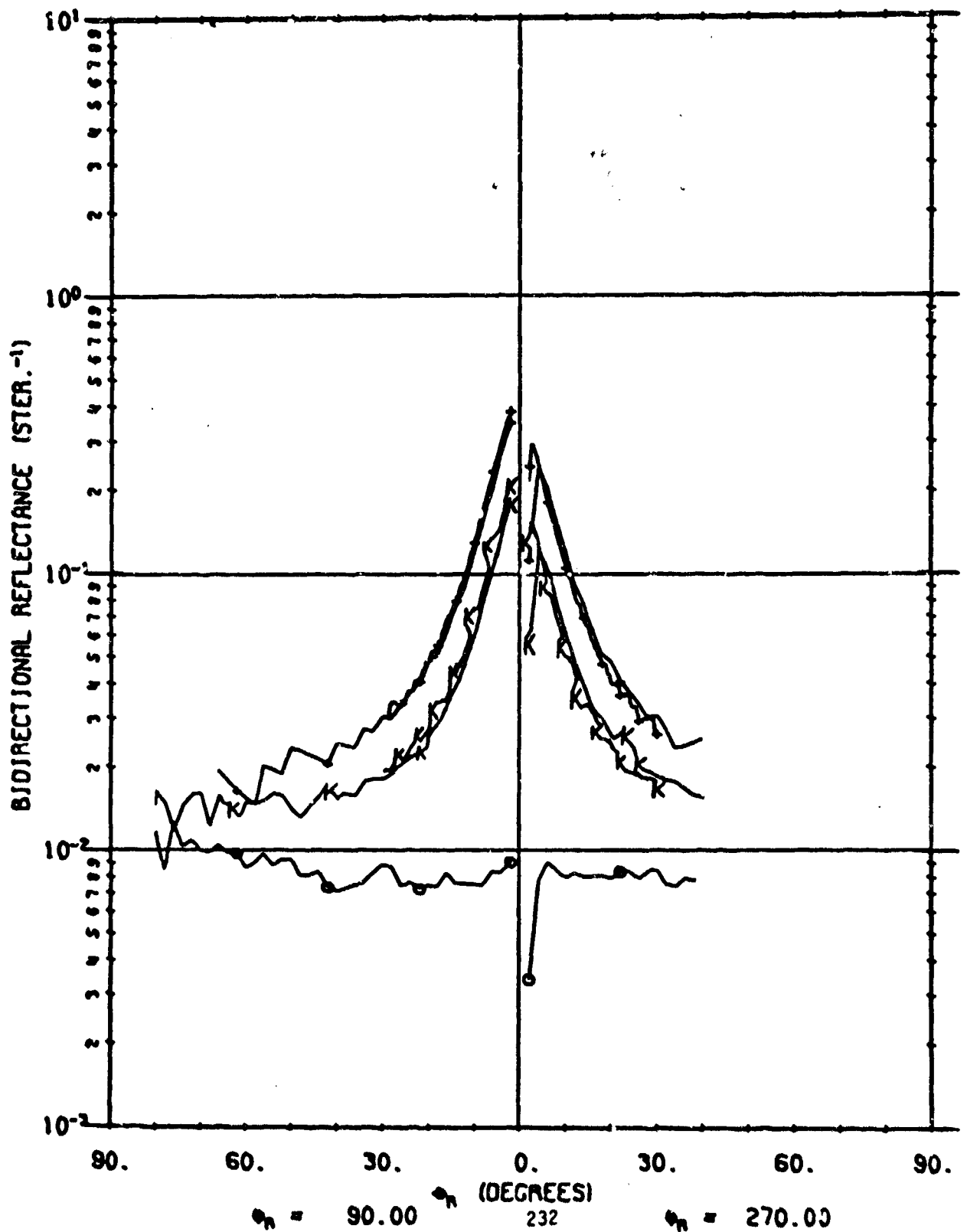
A02022 604

$\lambda = 10.60$   
 $\phi_i = 180.0$   
 $\phi_t = 180.0$



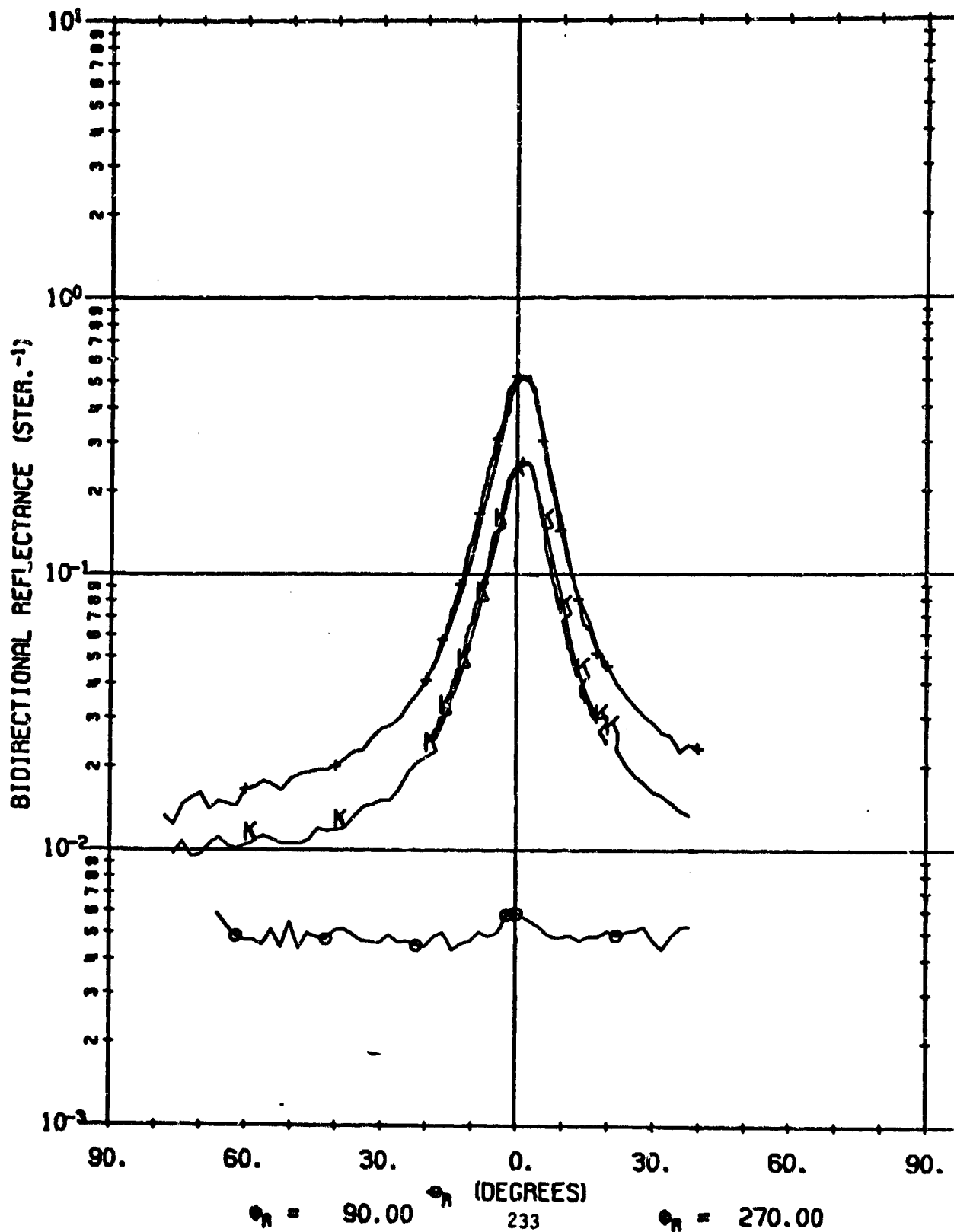
A02022 202

$\lambda = .63$   
 $\phi_i = .0$   
 $\phi_i = 180.0$



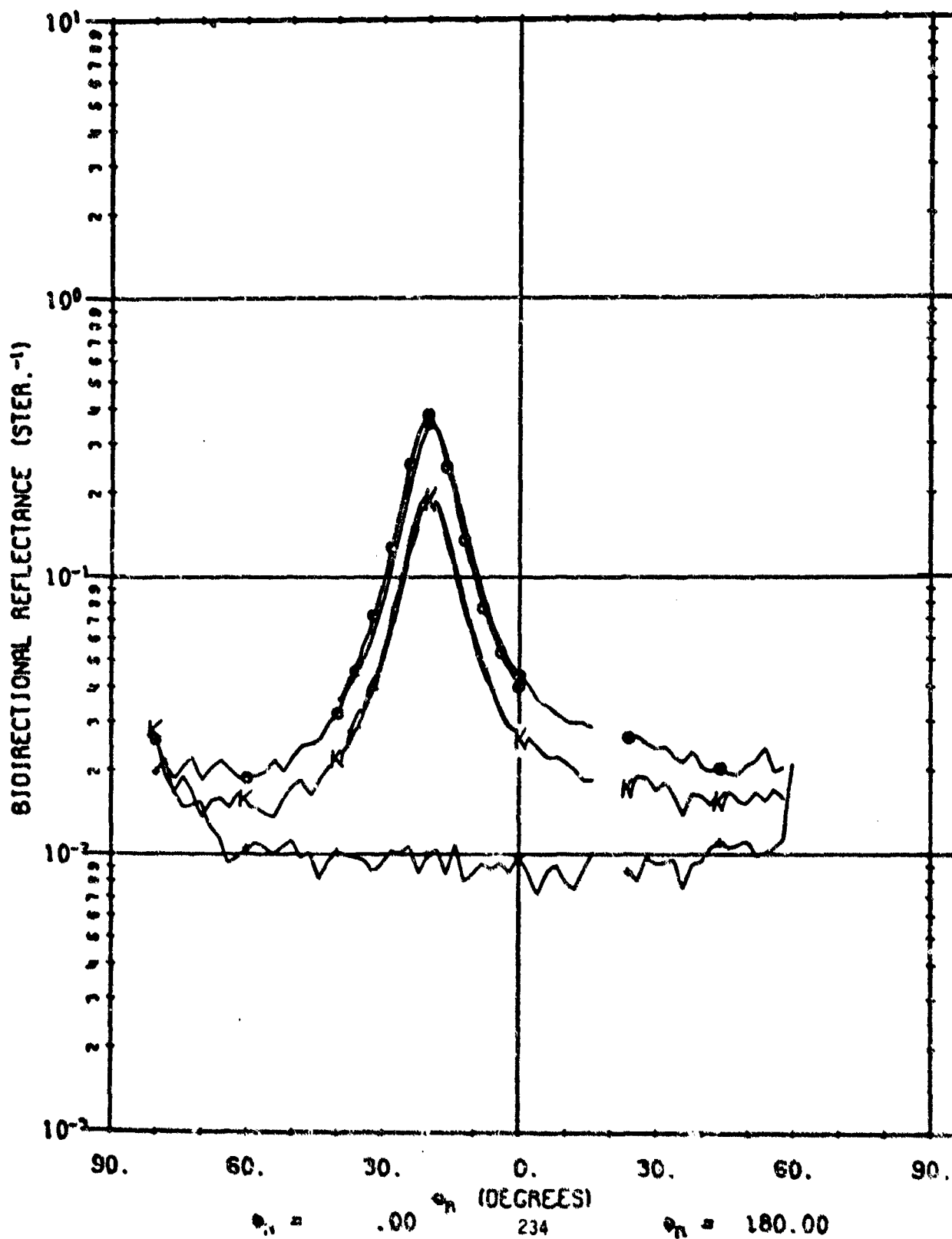
A02022 201

$\lambda = 1.06$   
 $\phi_1 = 180.0$



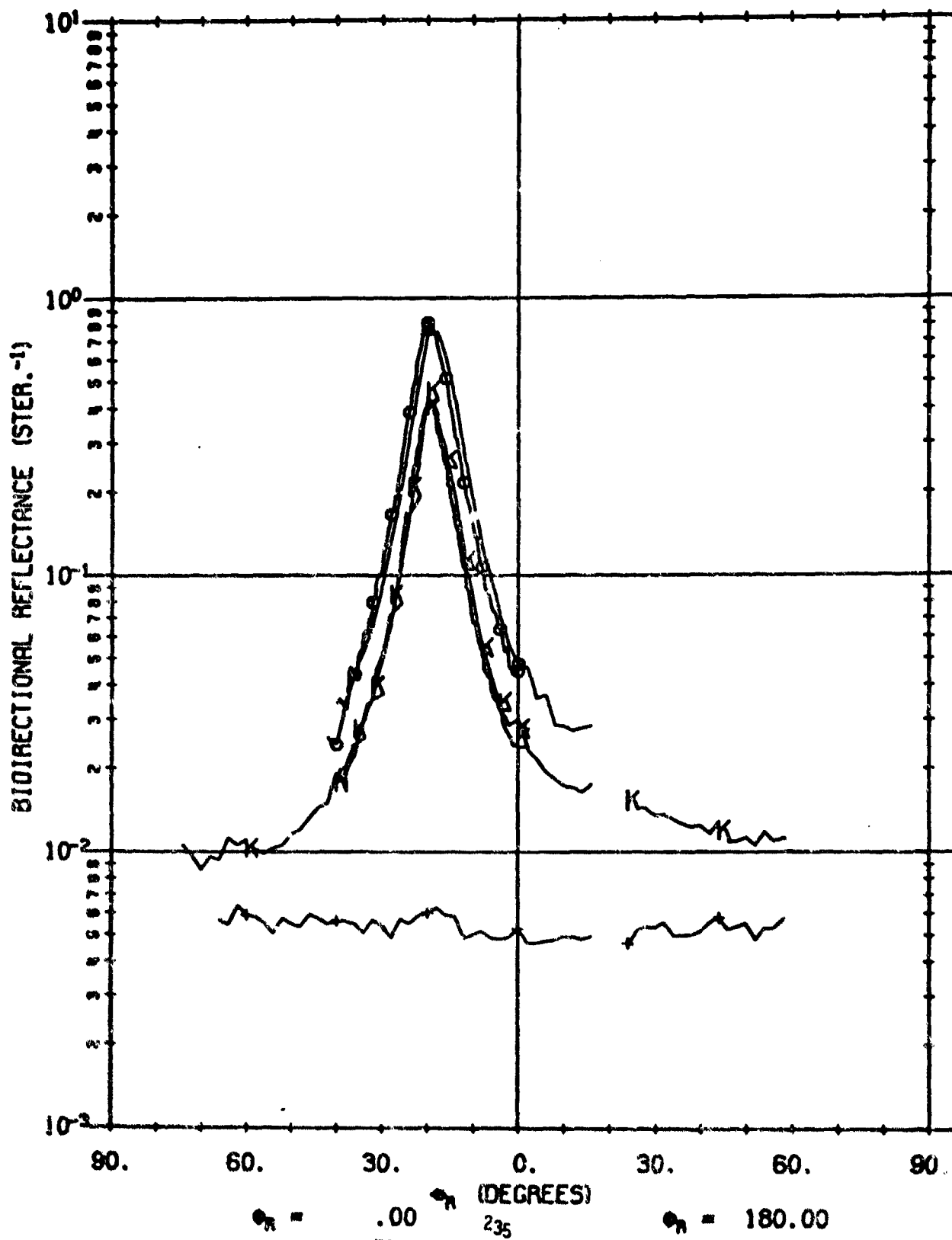
A02022 202

$\lambda = .63$   
 $\phi_i = 20.0$   
 $\phi_f = 180.0$



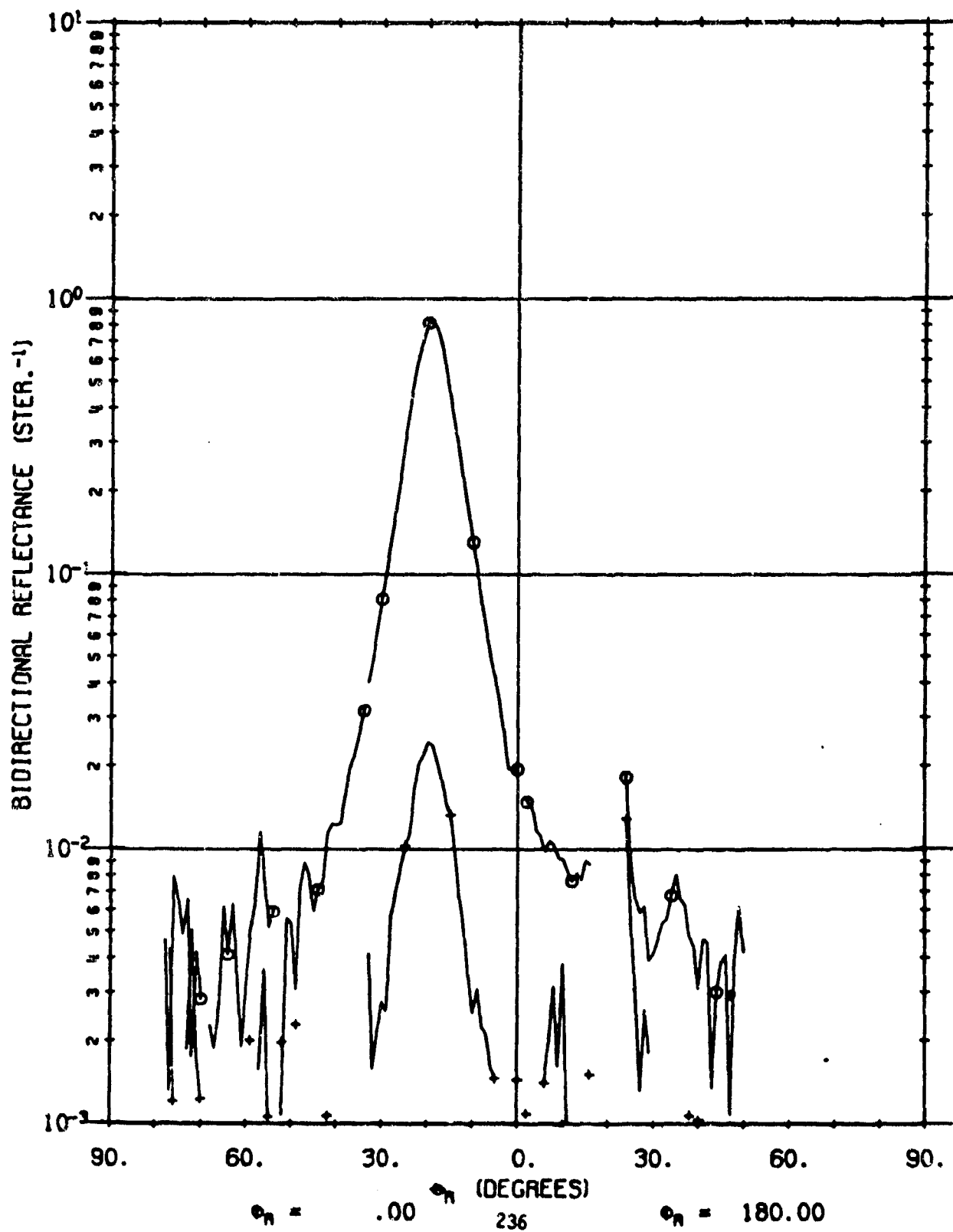
A02022 201

$\lambda = 1.06$   
 $\theta_i = 20.0$   
 $\phi_i = 180.0$



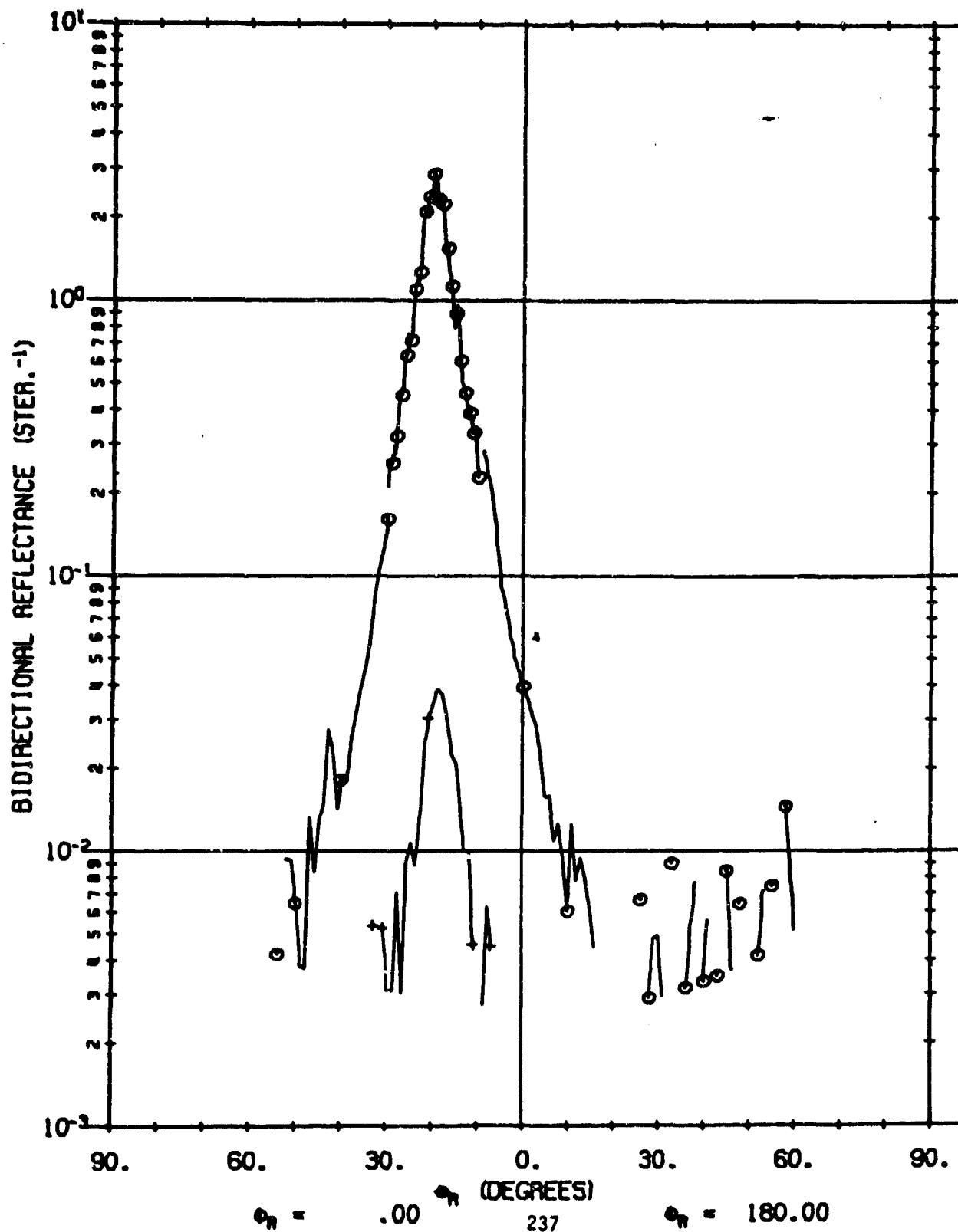
A02022 701

$\lambda = 3.39$   
 $\phi_i = 20.0$   
 $\phi_i = 180.0$



A02022 604

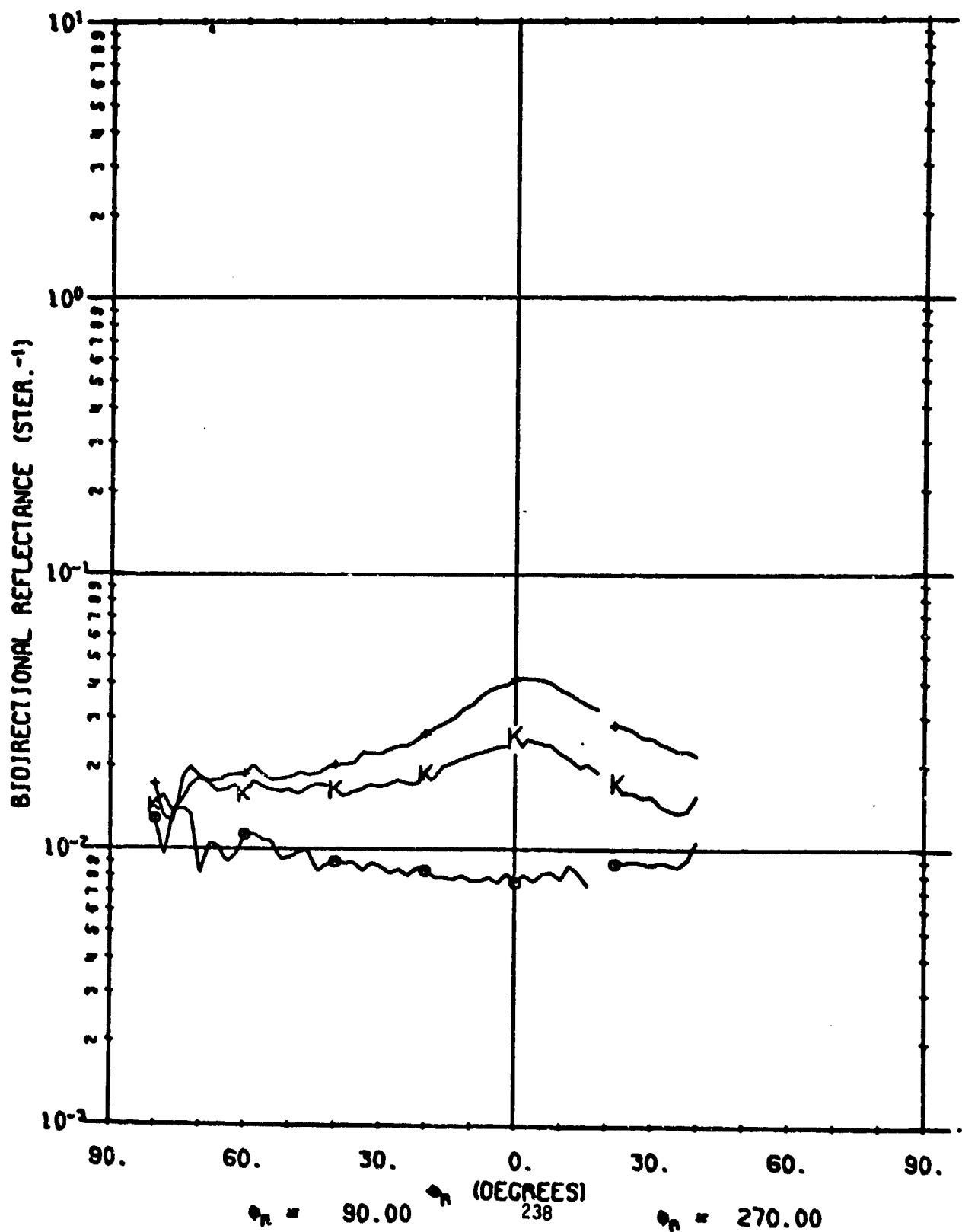
$\lambda = 10.60$   
 $\phi_i = 20.0$   
 $\phi_f = 180.0$





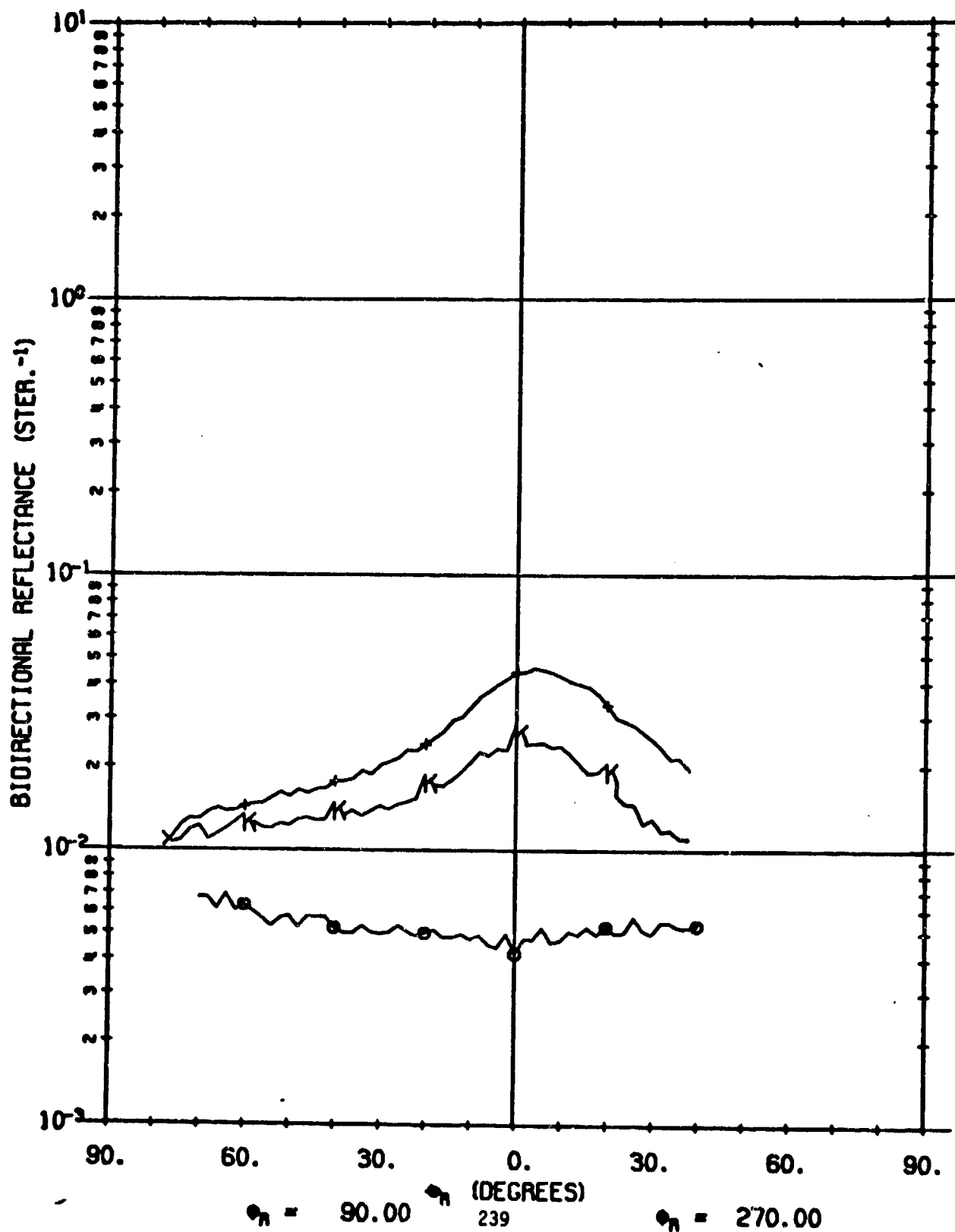
A02022 202

$\lambda = .63$   
 $\phi_1 = 20.0$   
 $\phi_2 = 180.0$



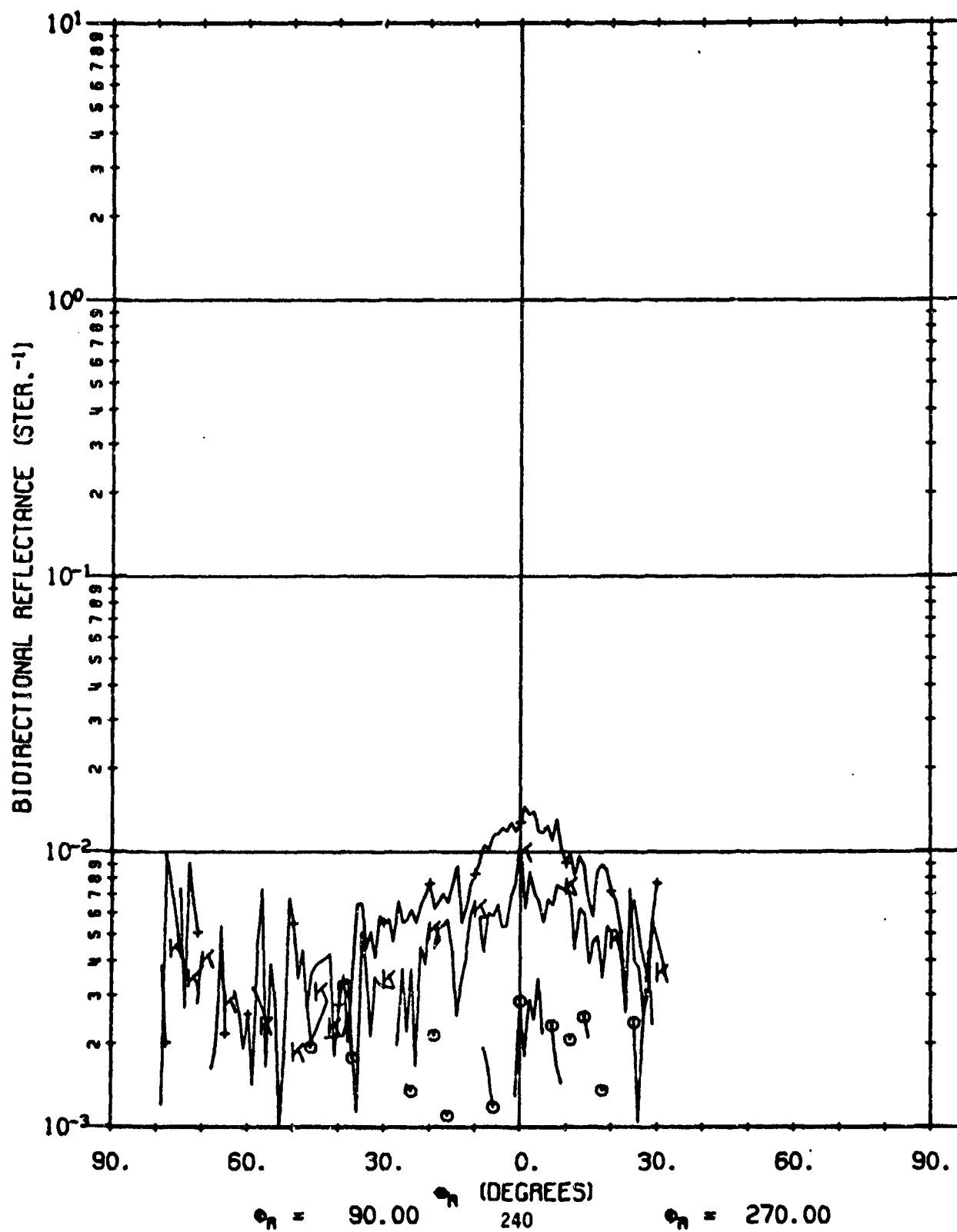
A02022 201

$\lambda = 1.06$   
 $\phi_i = 20.0$   
 $\phi_j = 180.0$



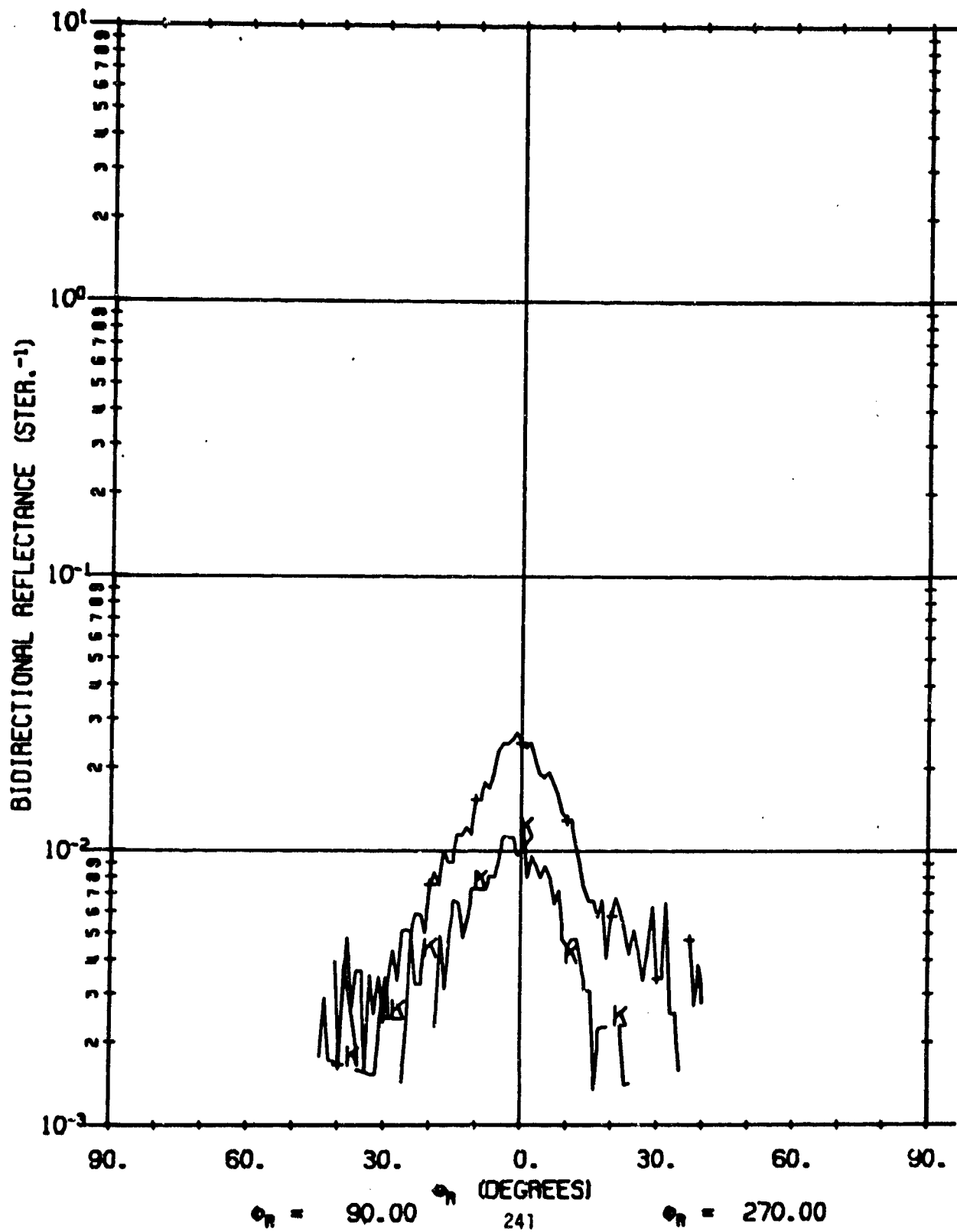
A02022 702

$\lambda = 3.39$   
 $\phi_i = 20.0$   
 $\phi_i = 180.0$



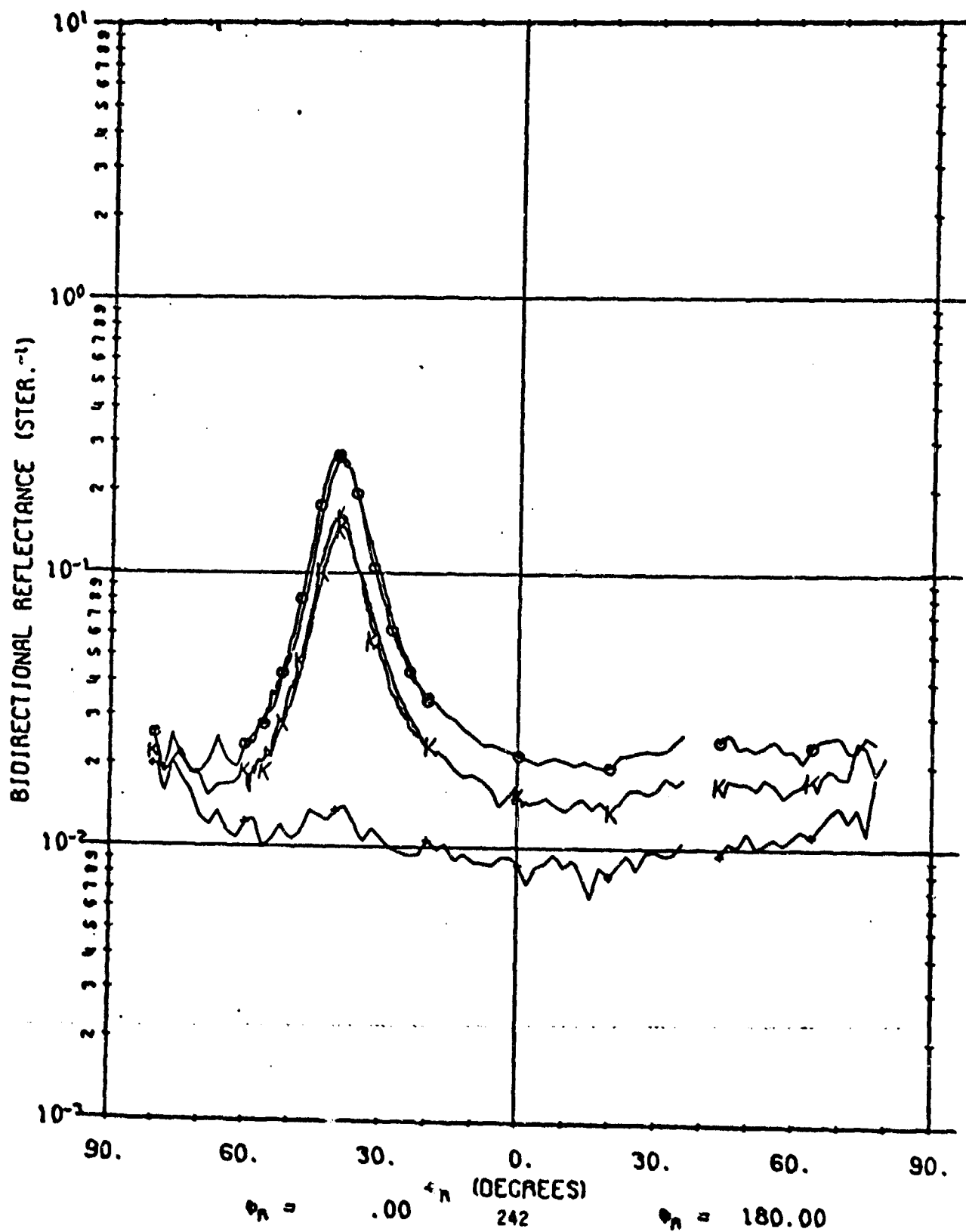
A02022 602

$\lambda = 10.60$   
 $\phi_i = 20.0$   
 $\phi_t = 180.0$



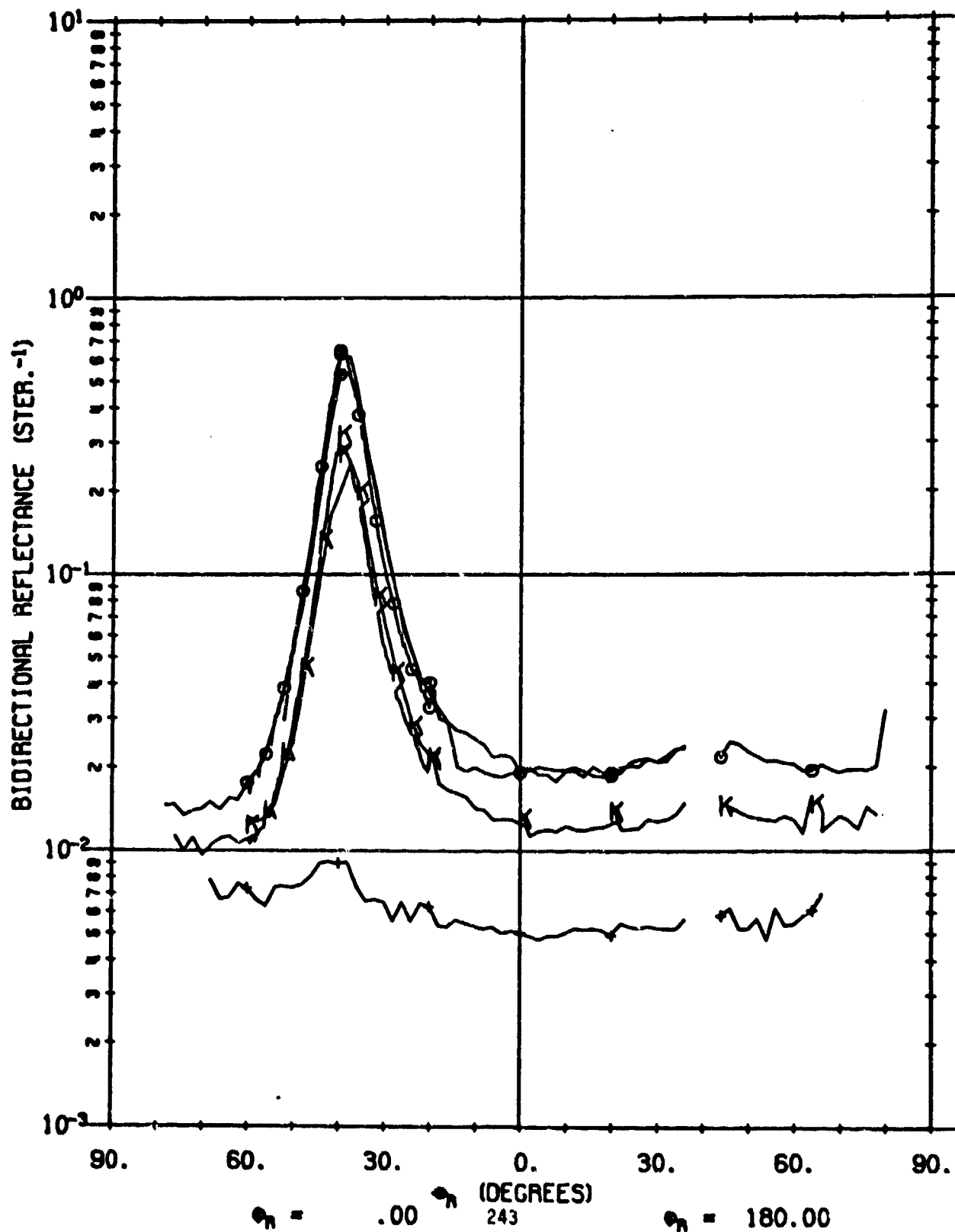
A02022 202

$\lambda = .63$   
 $\phi_i = 40.0$   
 $\phi_j = 180.0$



A02022 201

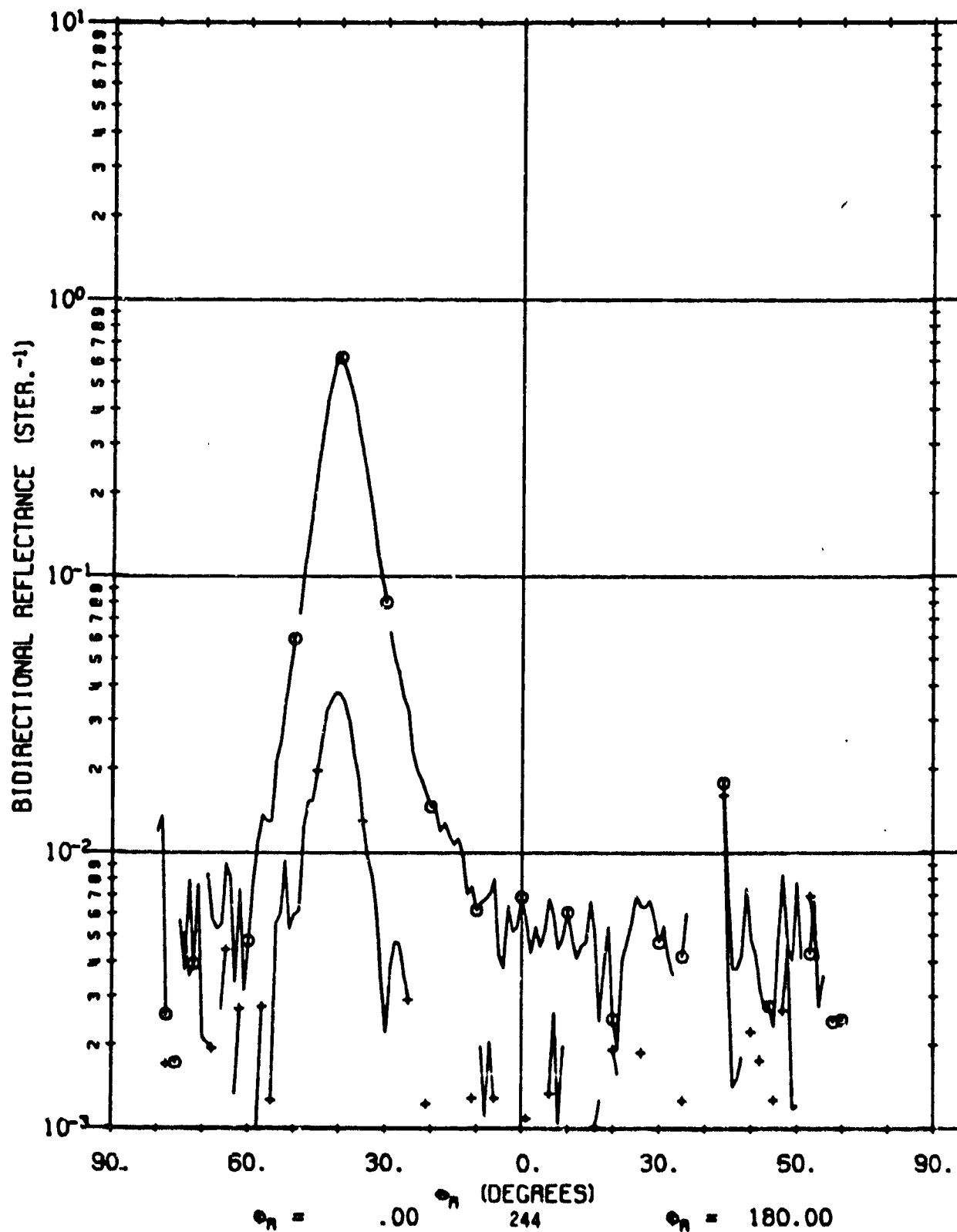
$\lambda = 1.06$   
 $\phi_1 = 40.0$   
 $\phi_2 = 180.0$



A02022 701

$\lambda = 3.39$   
 $\phi_i = 40.0$   
 $\phi_f = 180.0$

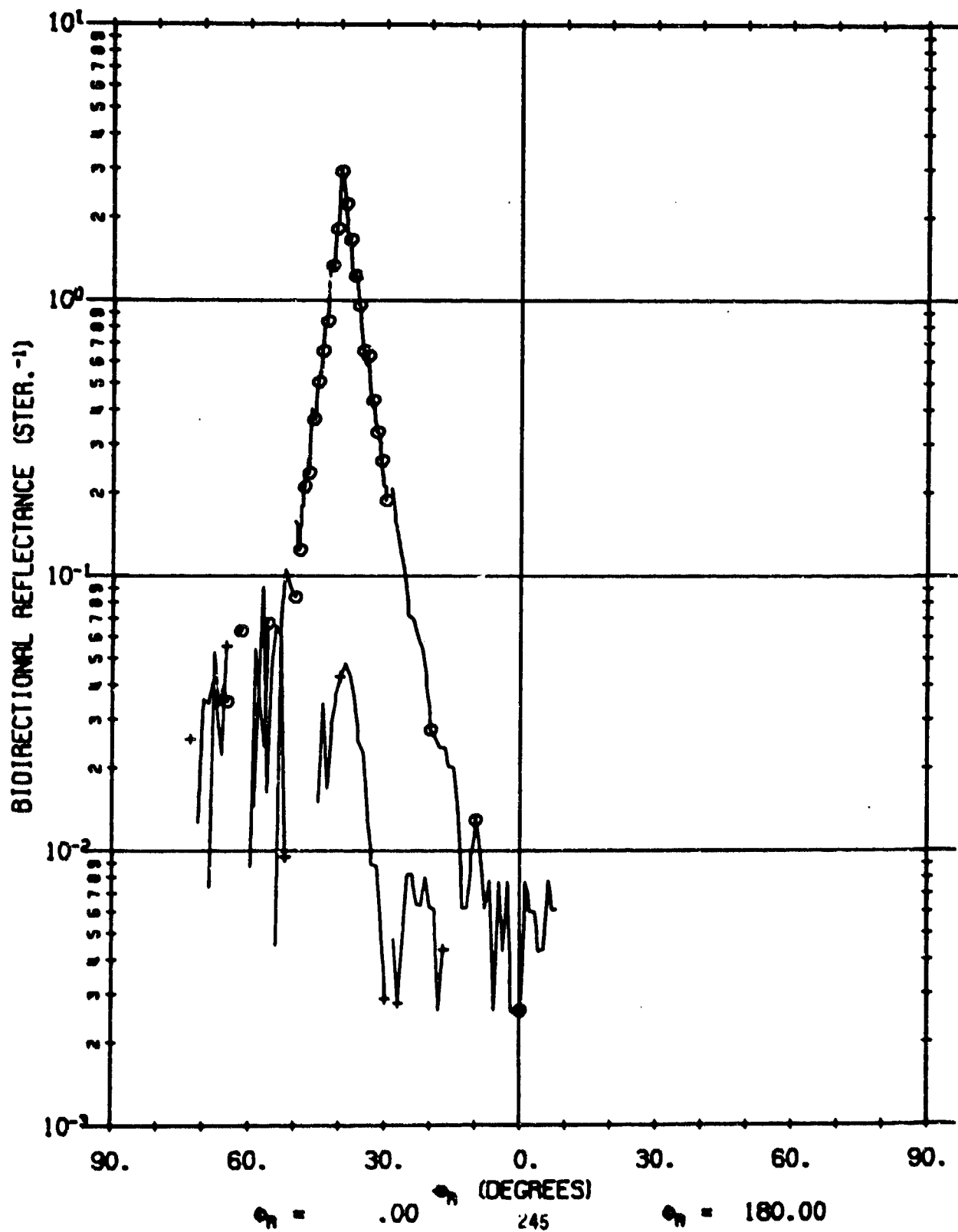
77



U

A02022 604

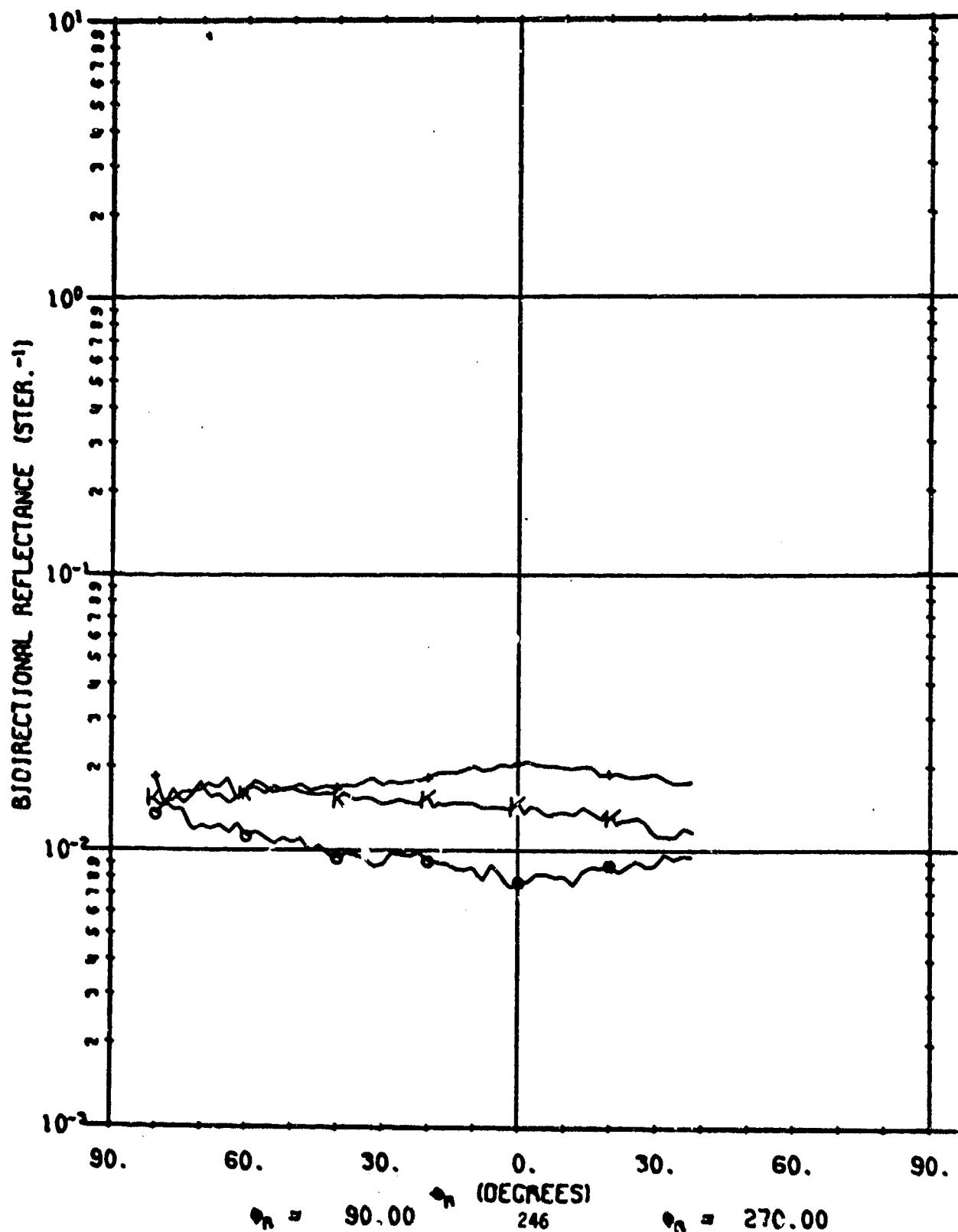
$\lambda = 10.60$   
 $\phi_i = 40.0$   
 $\phi_f = 180.0$





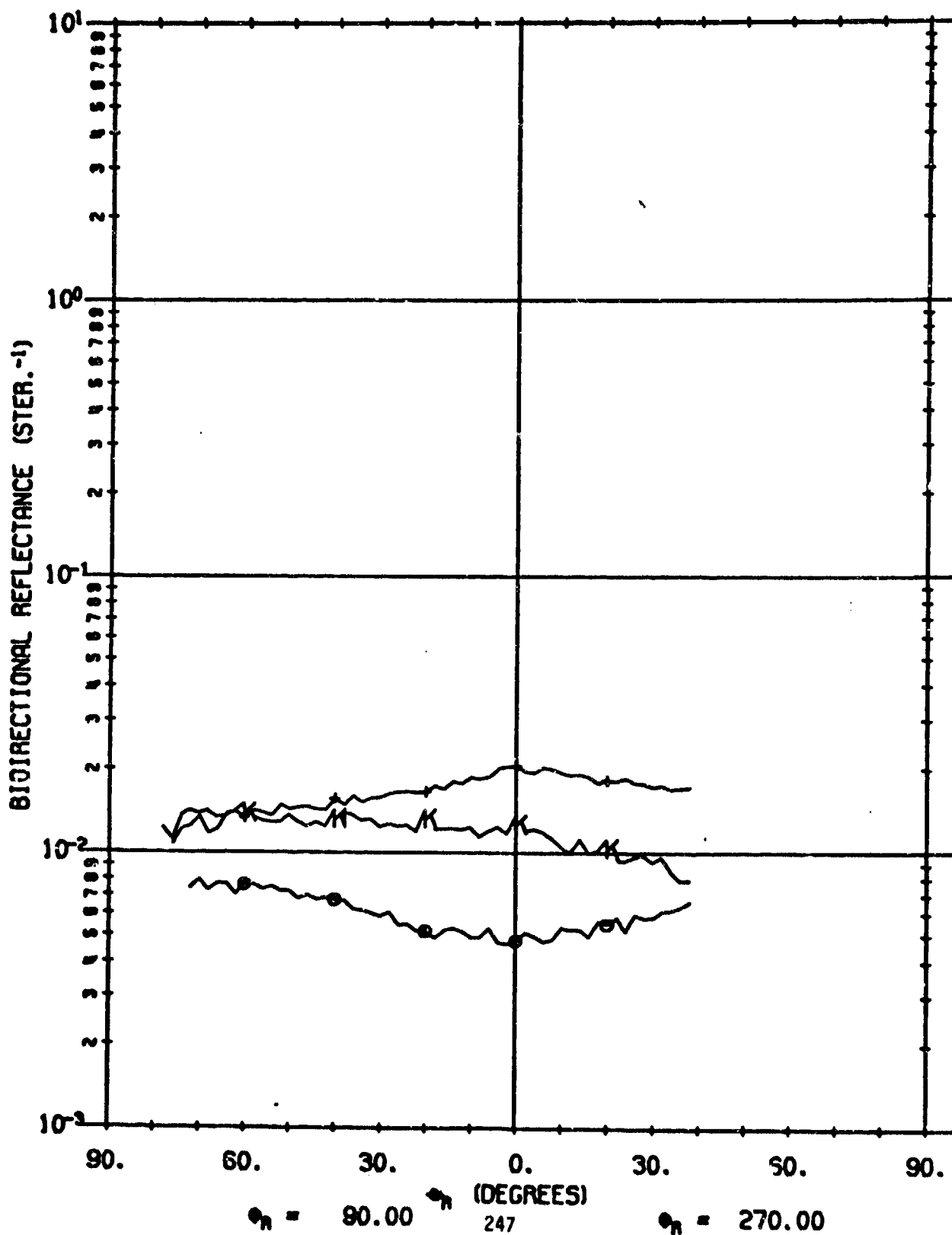
A02022 202

$\lambda = .63$   
 $\phi_1 = 40.0$   
 $\phi_2 = 180.0$



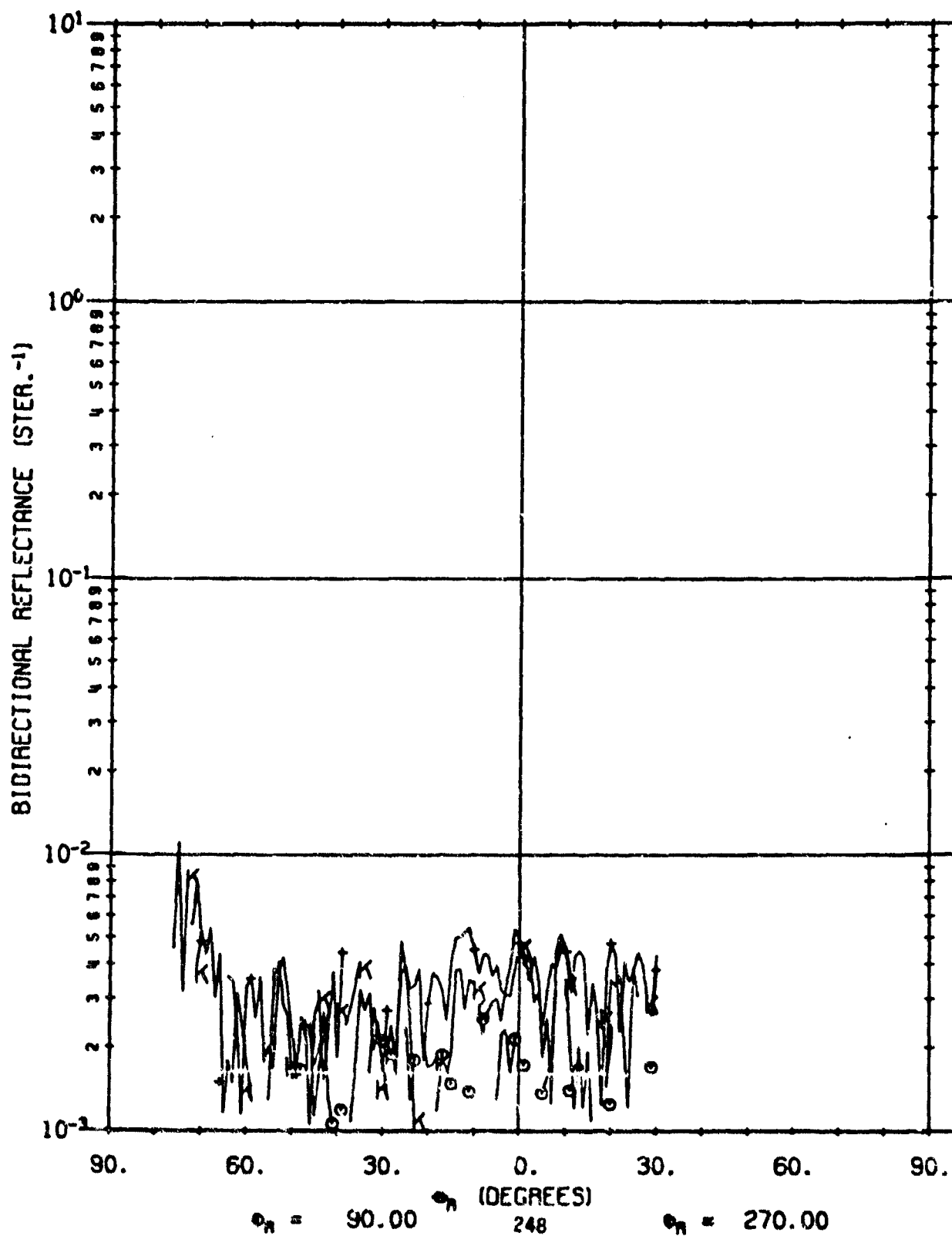
HU2022 201

$\lambda = 1.06$   
 $\phi_i = 40.0$   
 $\phi_j = 180.0$



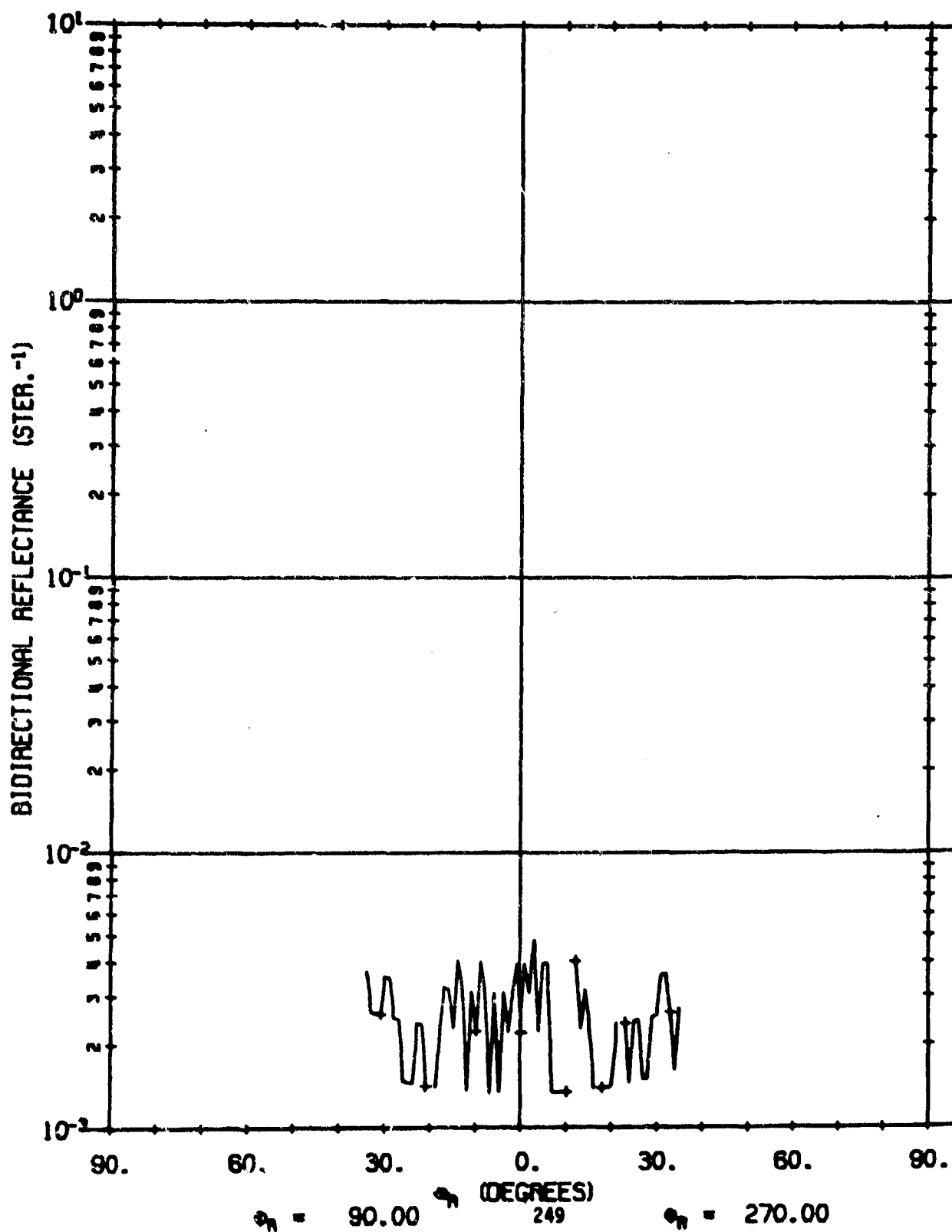
A02022 702

$\lambda = 3.39$   
 $\phi_1 = 40.0$   
 $\phi_2 = 180.0$



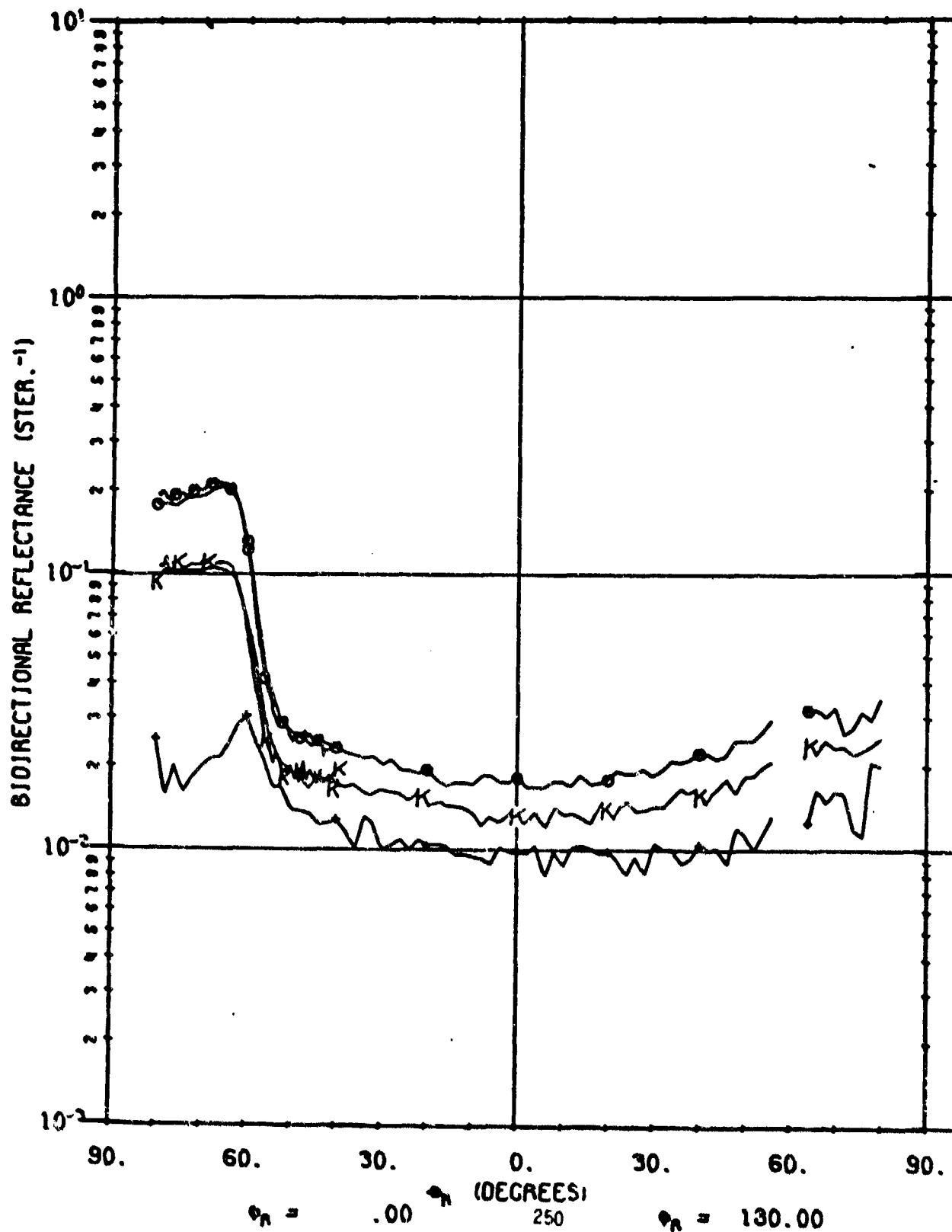
A02022 602

$\lambda = 10.60$   
 $\phi = 40.0$   
 $\theta = 180.0$



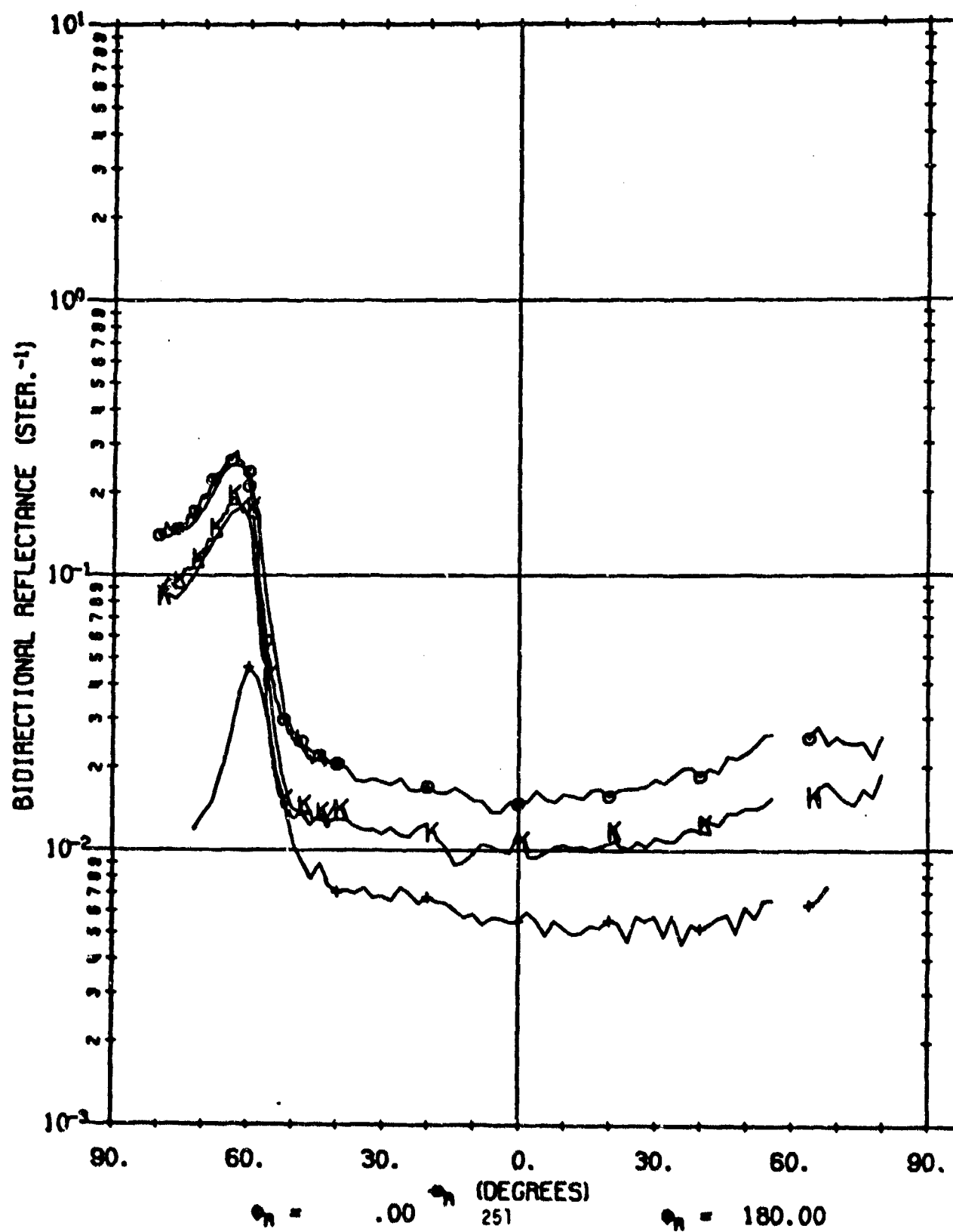
A02022 202

$\lambda = .63$   
 $\phi_i = 60.0$   
 $\phi_i = 180.0$



A02022 201

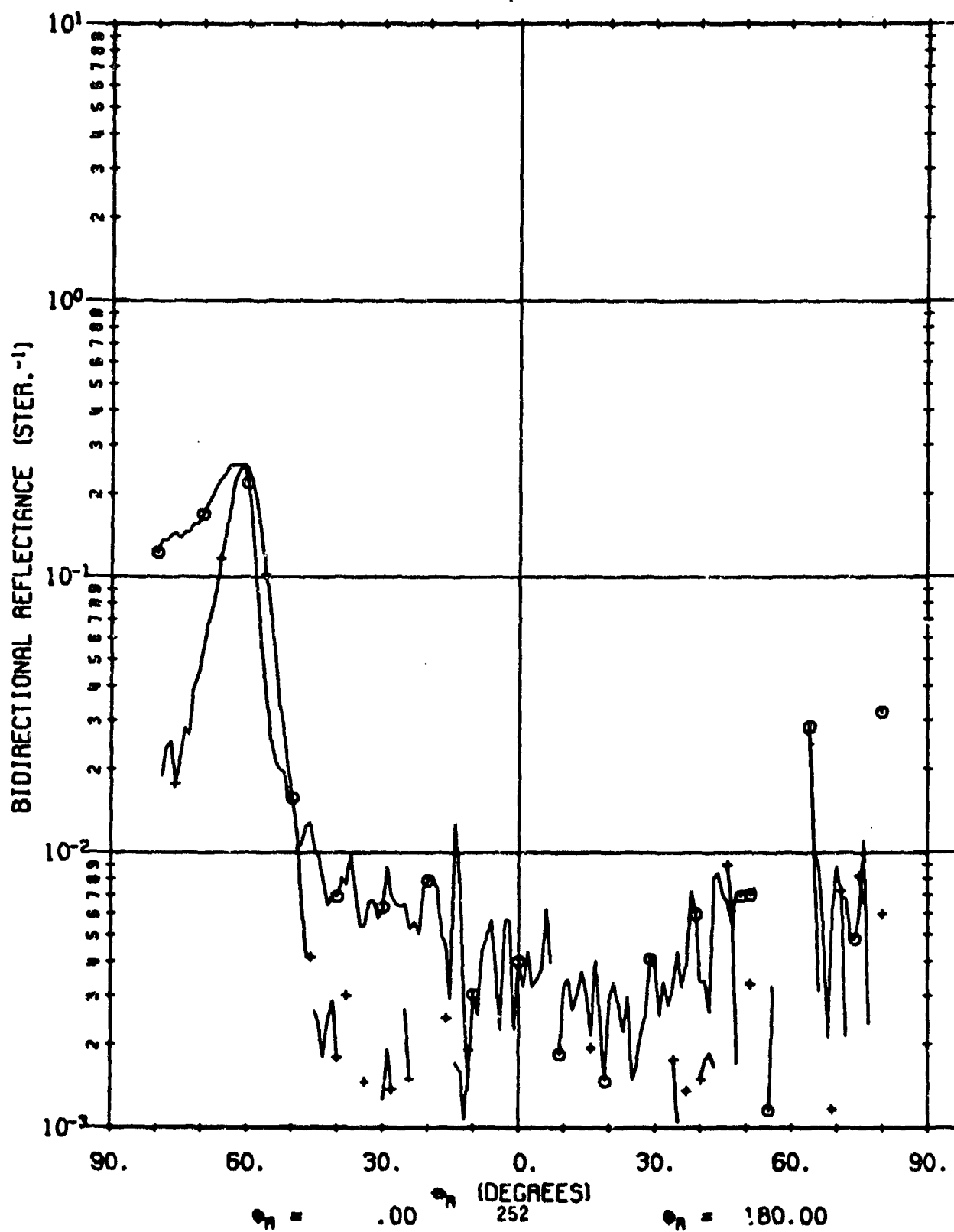
$\lambda = 1.06$   
 $\phi_1 = 60.0$   
 $\phi_2 = 180.0$



A02022 701

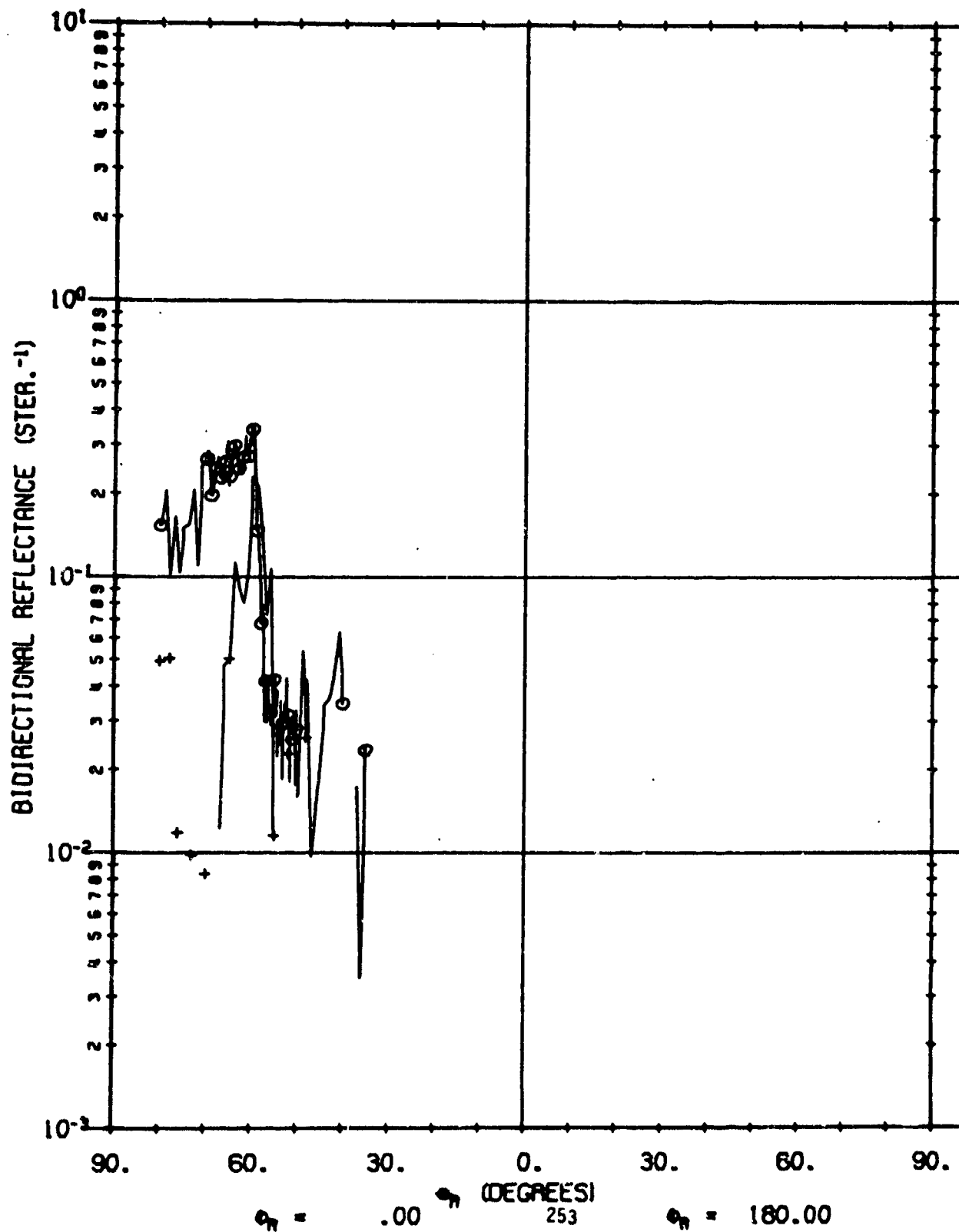
$\lambda = 3.39$   
 $\phi_j = 60.0$   
 $\phi_i = 180.0$

74



A02022 604

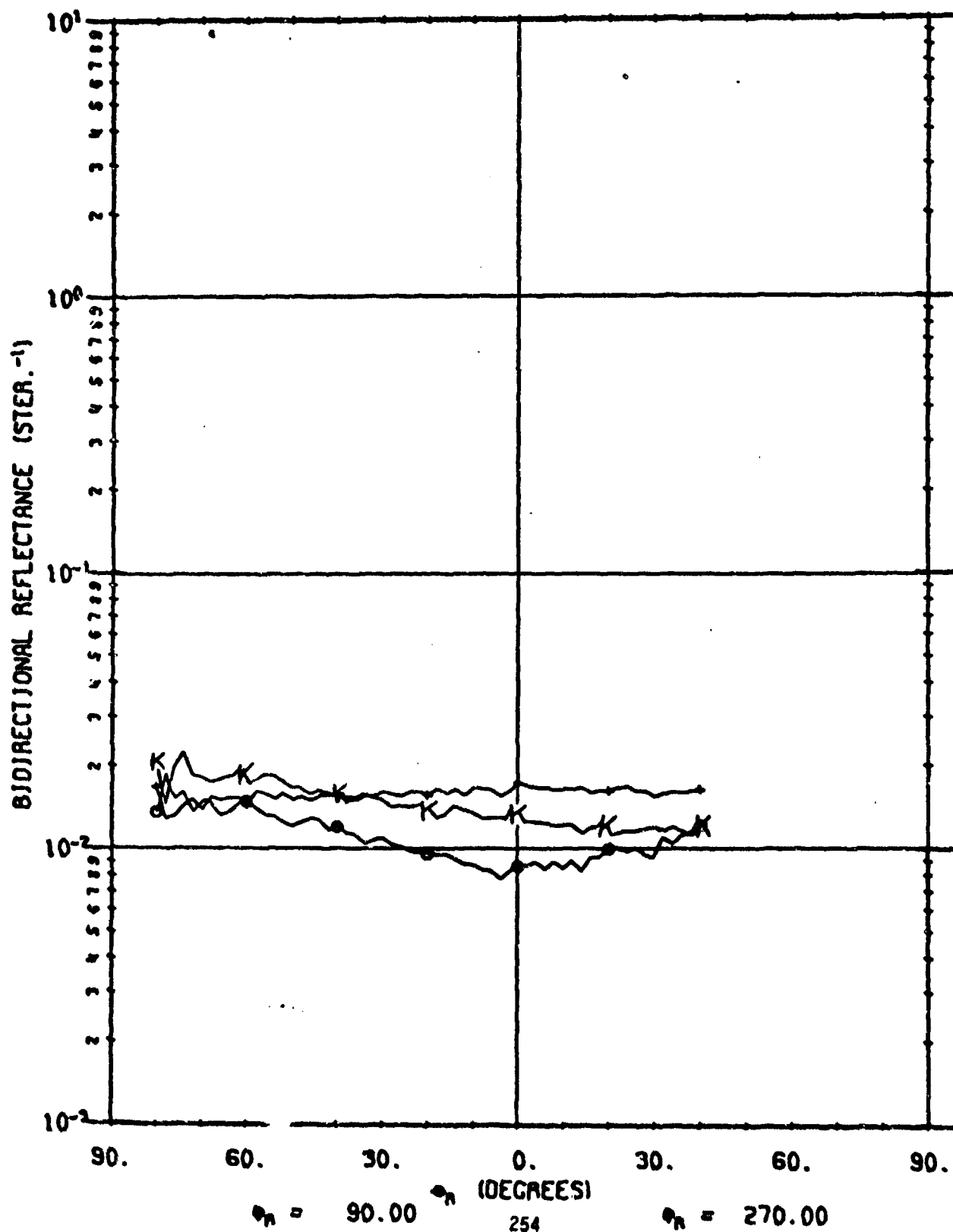
$\lambda = 10.60$   
 $\phi_i = 60.0$   
 $\phi_t = 180.0$





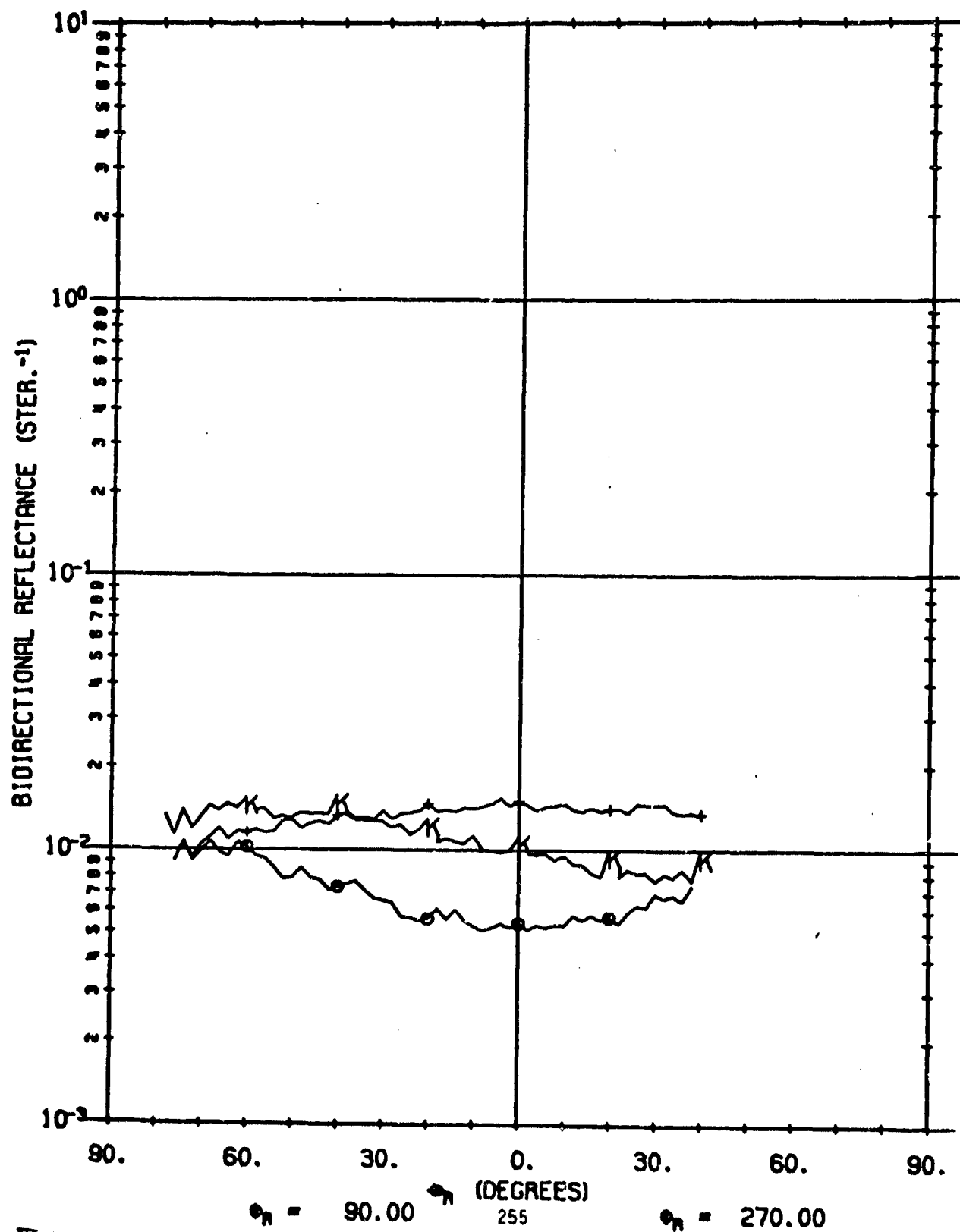
A02022 202

$\lambda = .63$   
 $\phi_i = 60.0$   
 $\phi_i = 180.0$



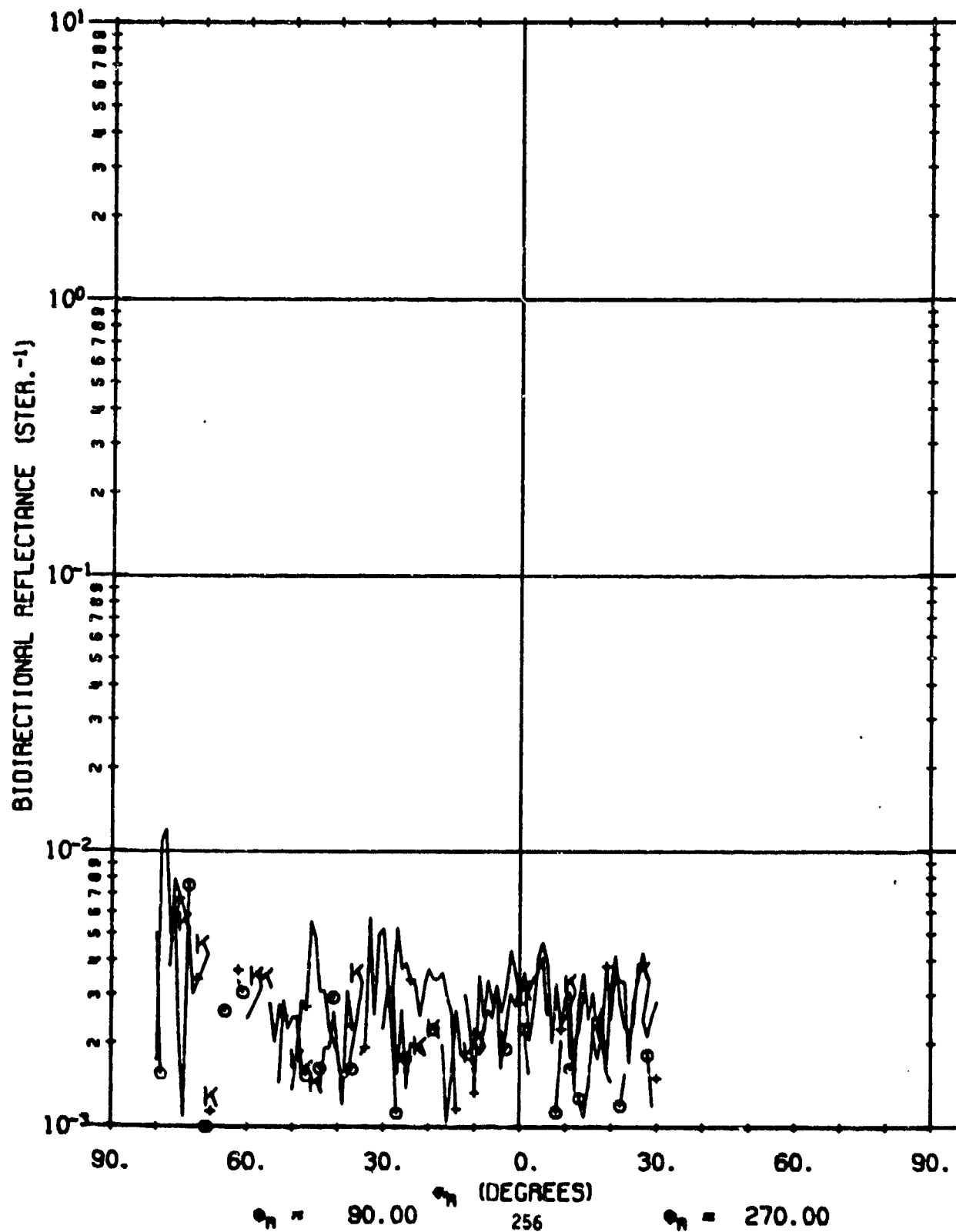
A02022 201

$\lambda = 1.06$   
 $\phi_i = 60.0$   
 $\phi_f = 180.0$



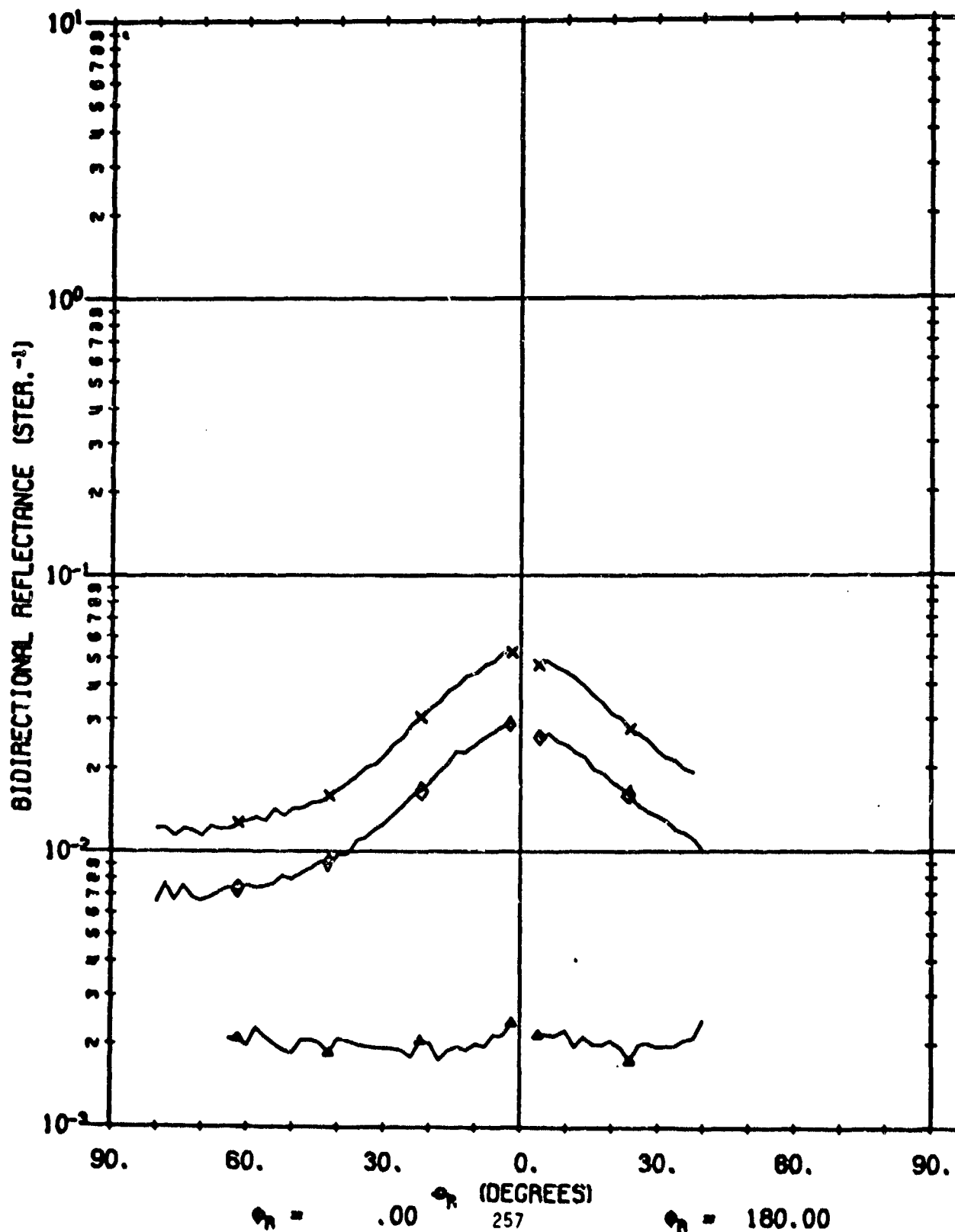
A02022 702

$\lambda = 3.39$   
 $\phi_1 = 60.0$   
 $\phi_2 = 180.0$



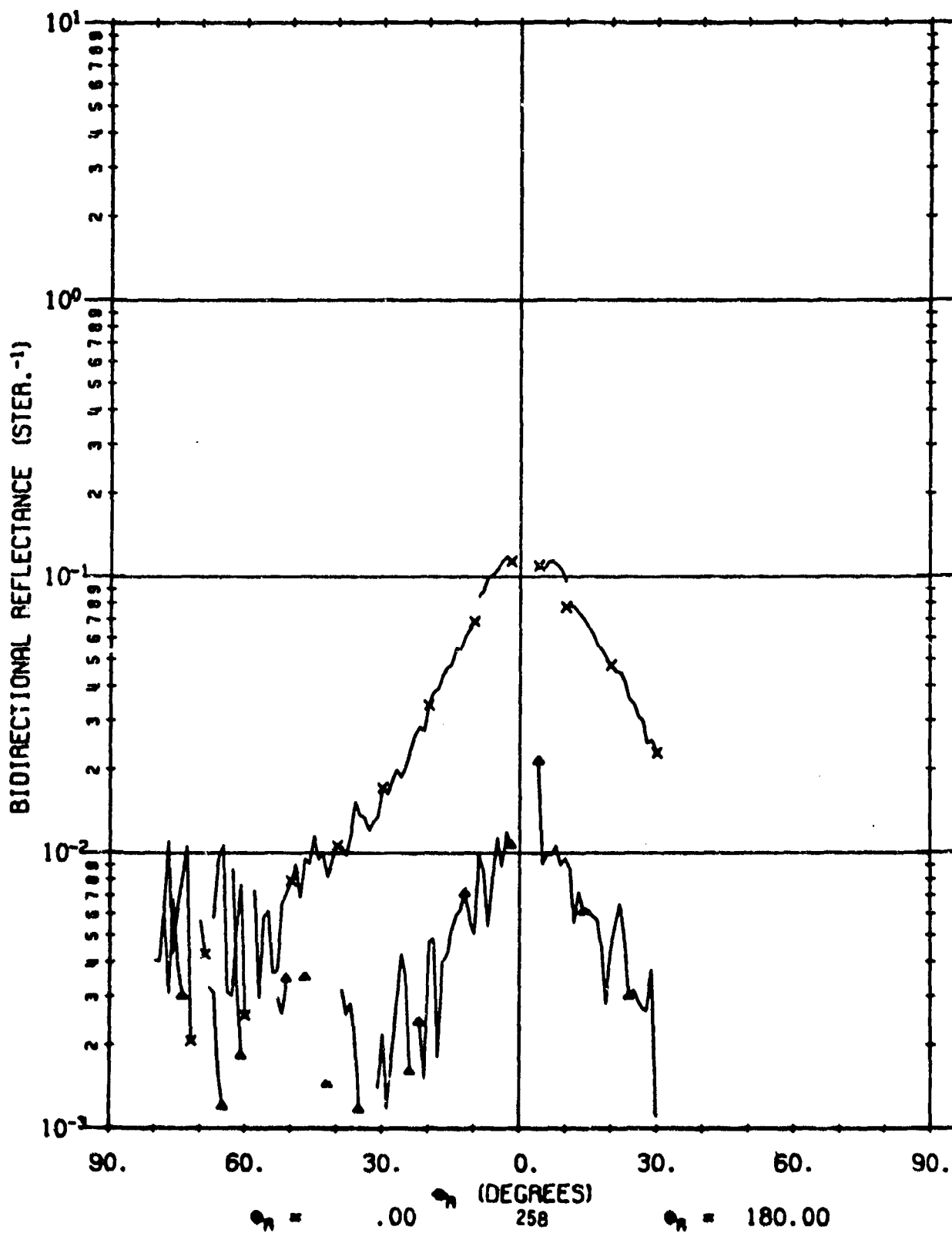
A02023 101

$\lambda = 1.06$   
 $\phi_i = 0.0$   
 $\phi_f = 180.0$



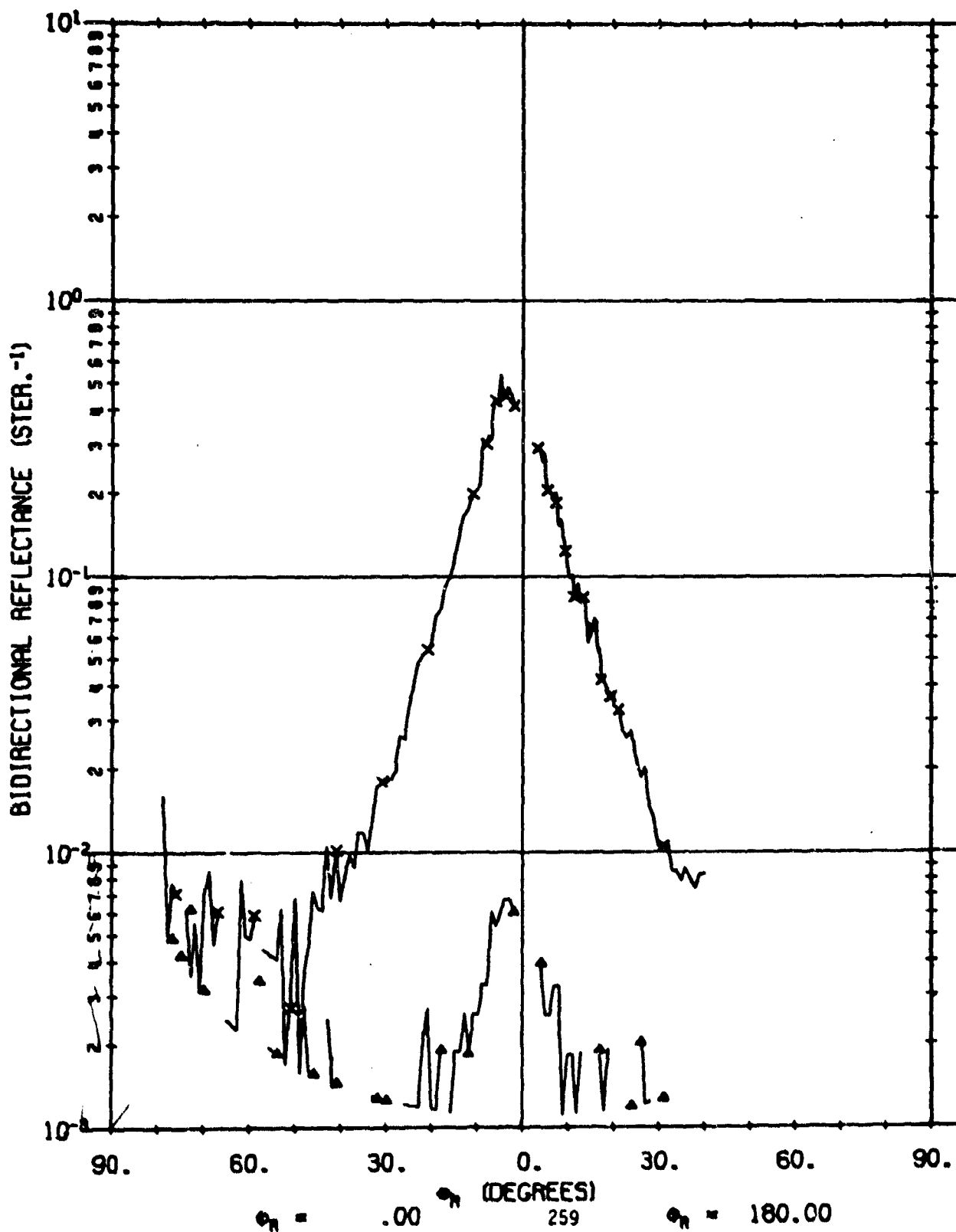
A02023 702

$\lambda = 3.39$   
 $\phi_1 = 0.0$   
 $\phi_2 = 180.0$



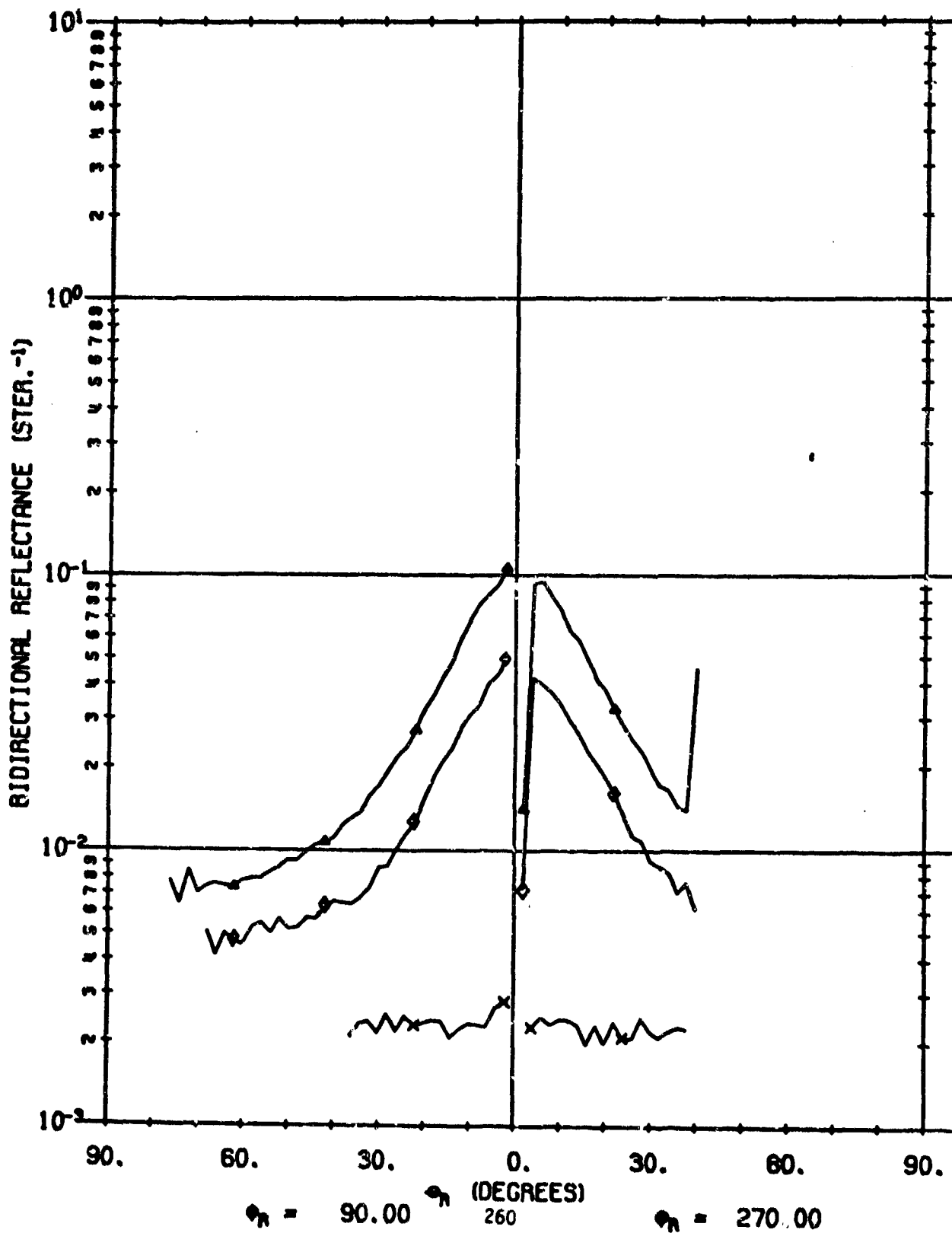
A02023 602

$\lambda = 10.60$   
 $\phi_i = 0$   
 $\phi_f = 180.0$



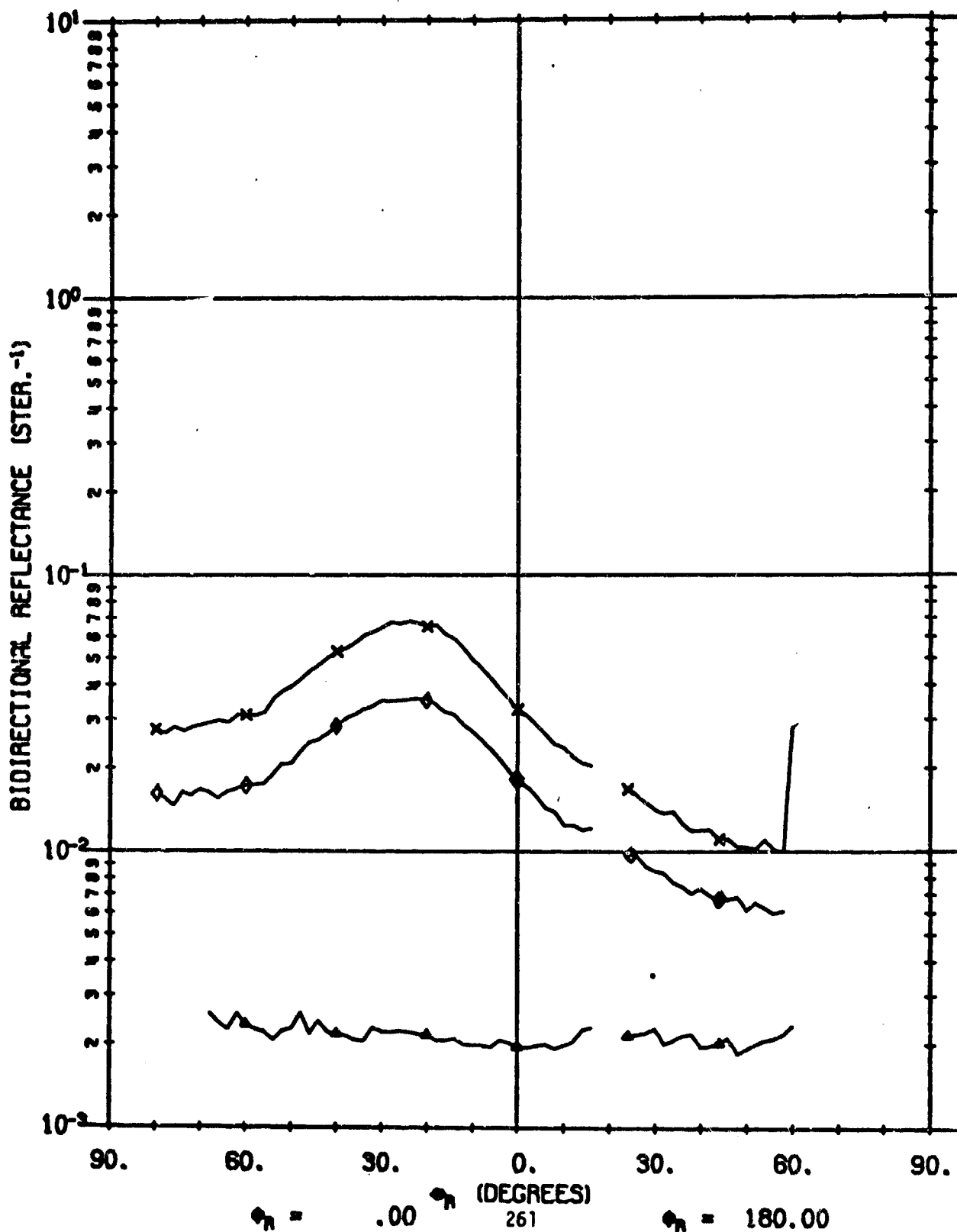
R02023 101

$\lambda = 1.06$   
 $\phi_1 = 180.0$   
 $\phi_2 = 180.0$



A02023 101

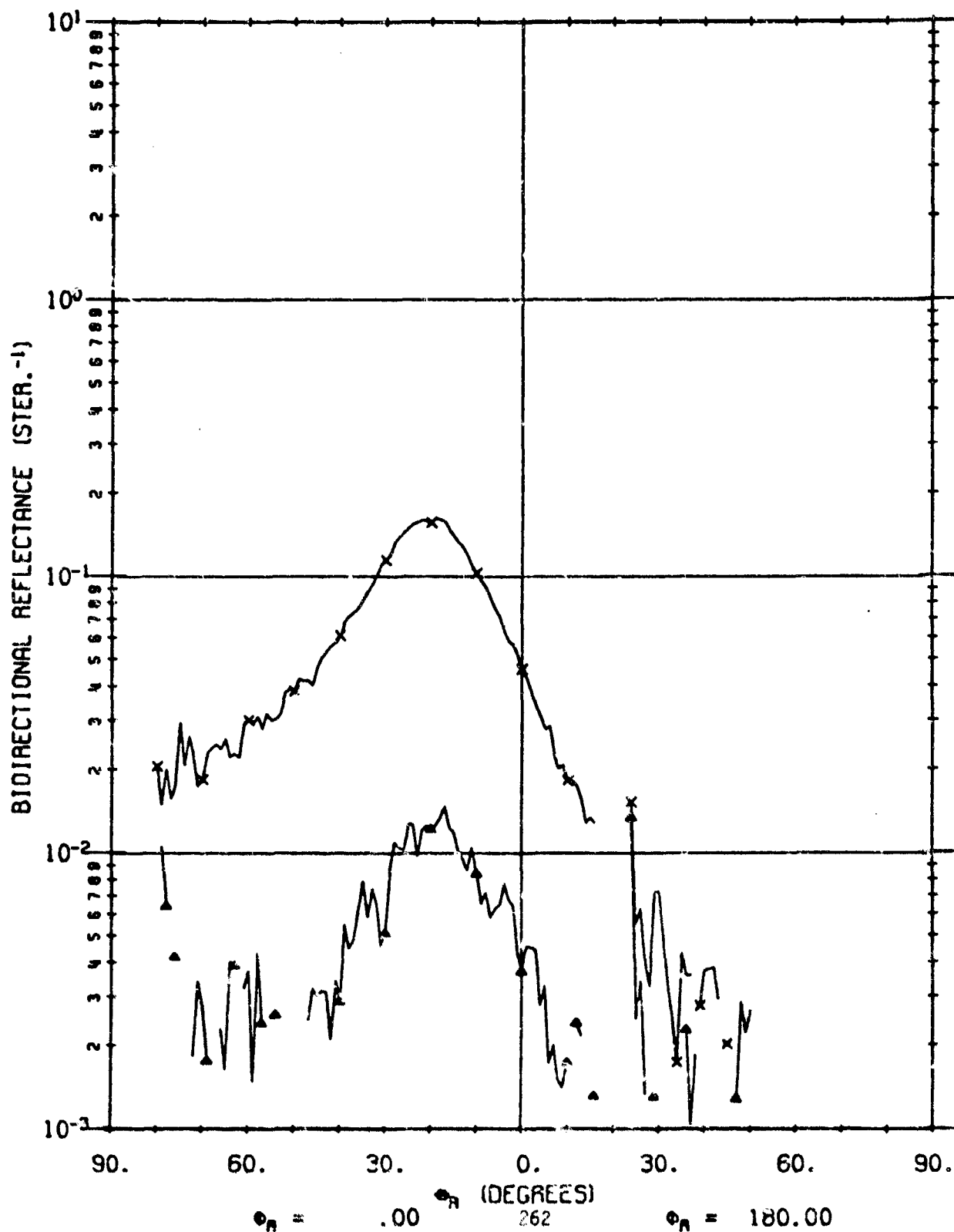
$\lambda = 1.06$   
 $\phi_i = 20.0$   
 $\phi_j = 180.0$





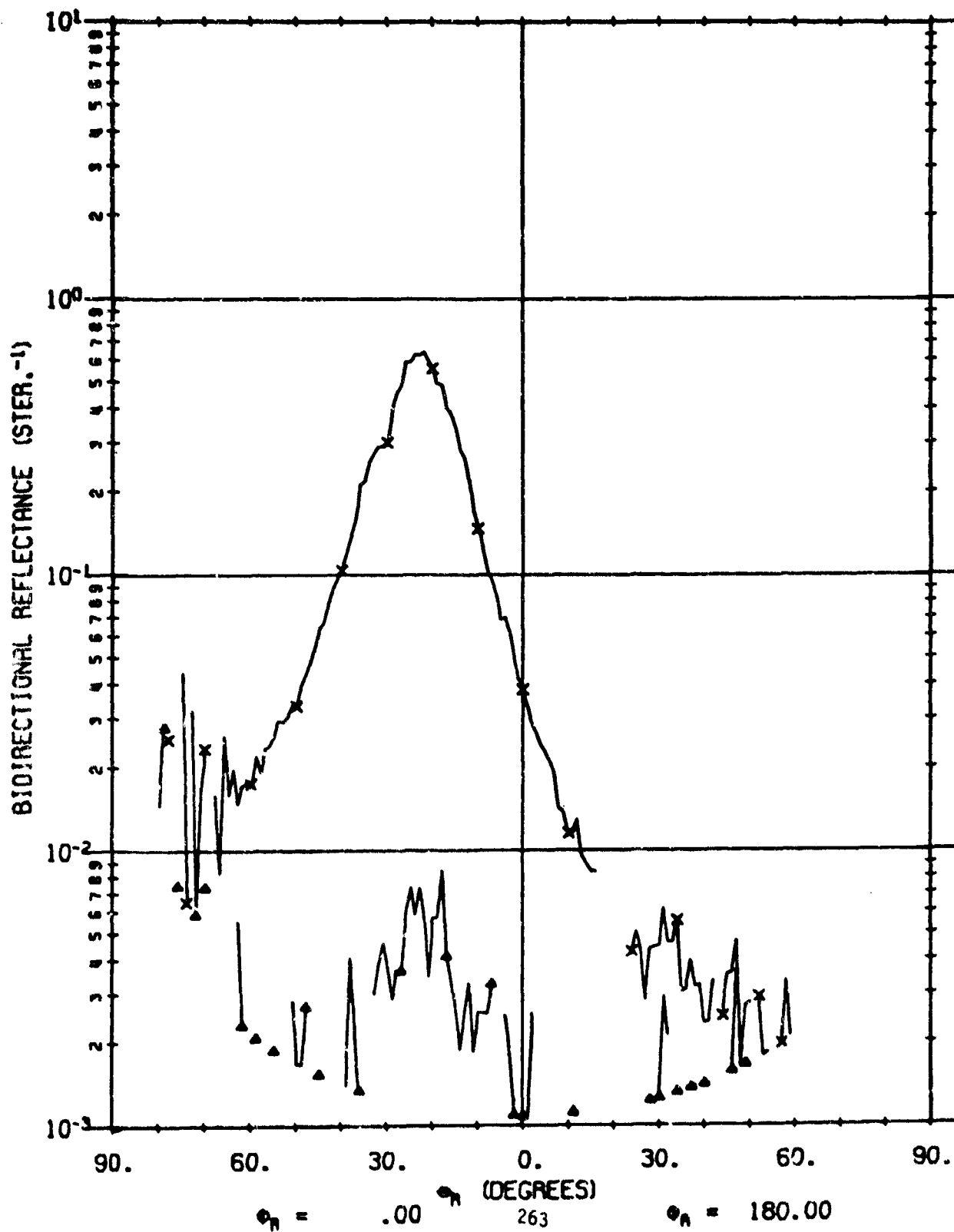
A02023 702

$\lambda = 3.39$   
 $\phi_i = 20.0$   
 $\phi_i = 180.0$



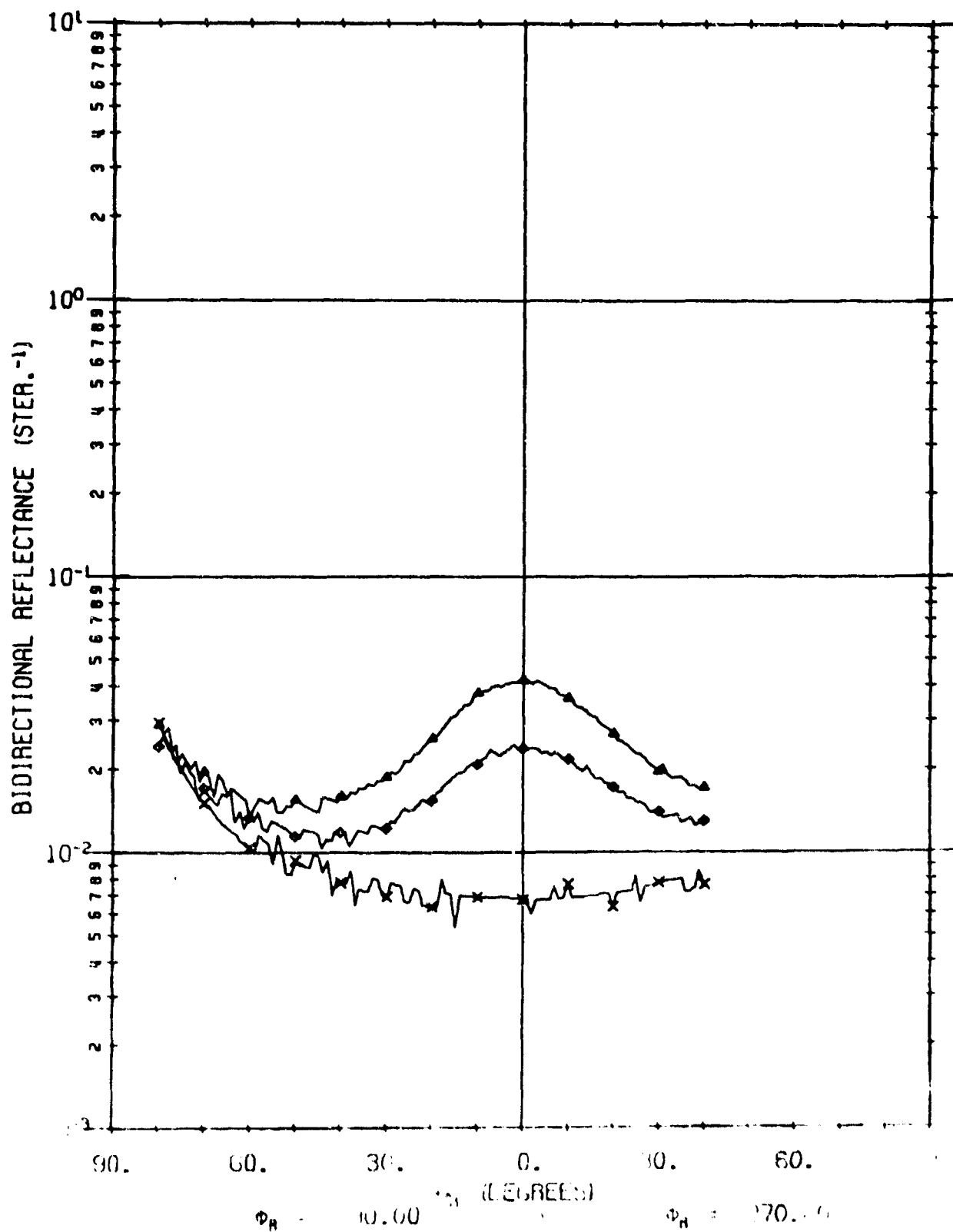
A02023 602

$\lambda = 10.60$   
 $\phi_i = 20.0$   
 $\phi_f = 180.0$



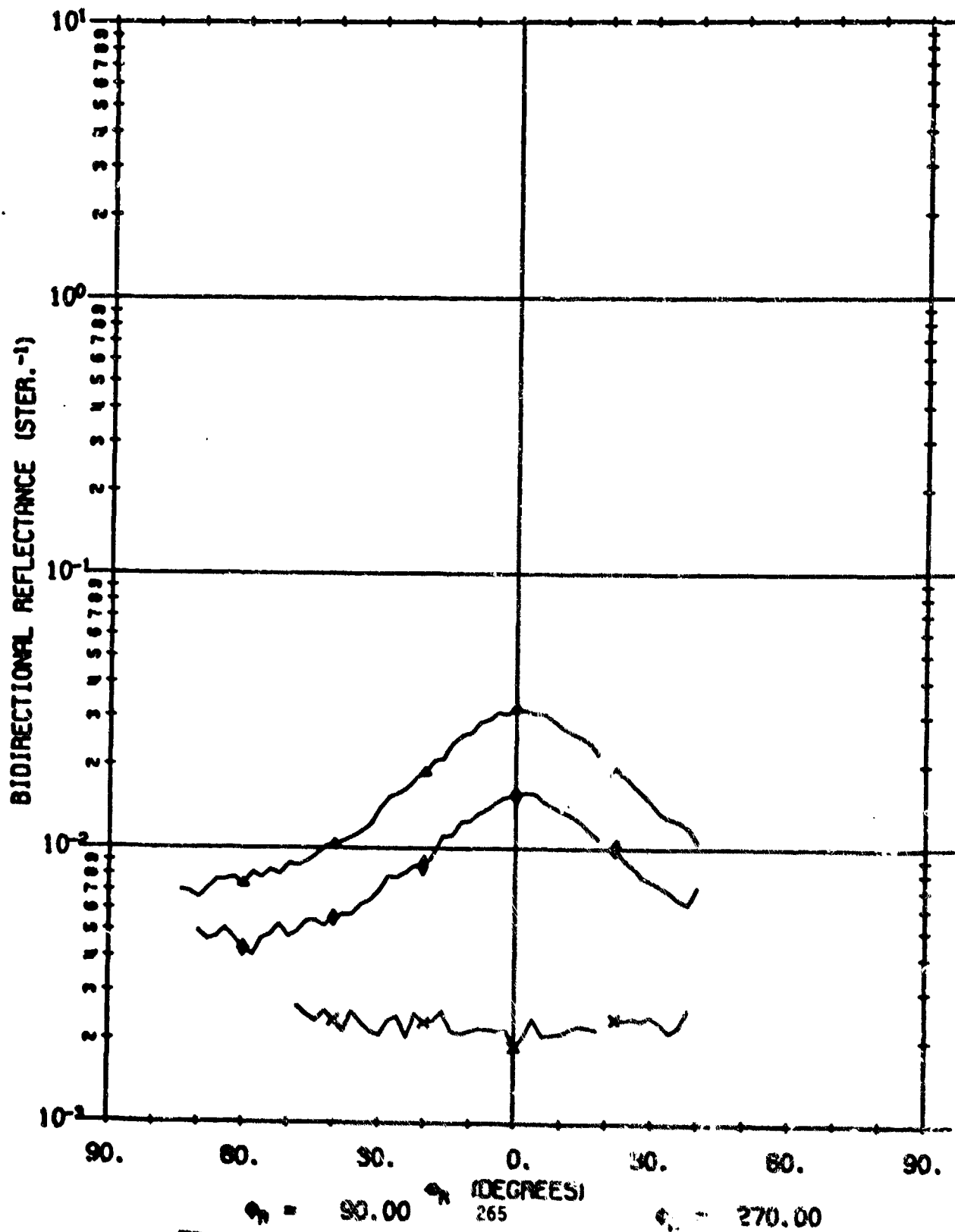
A02023 501

$\lambda = .63$   
 $\phi_i = 20.0$   
 $\phi_i = 180.0$



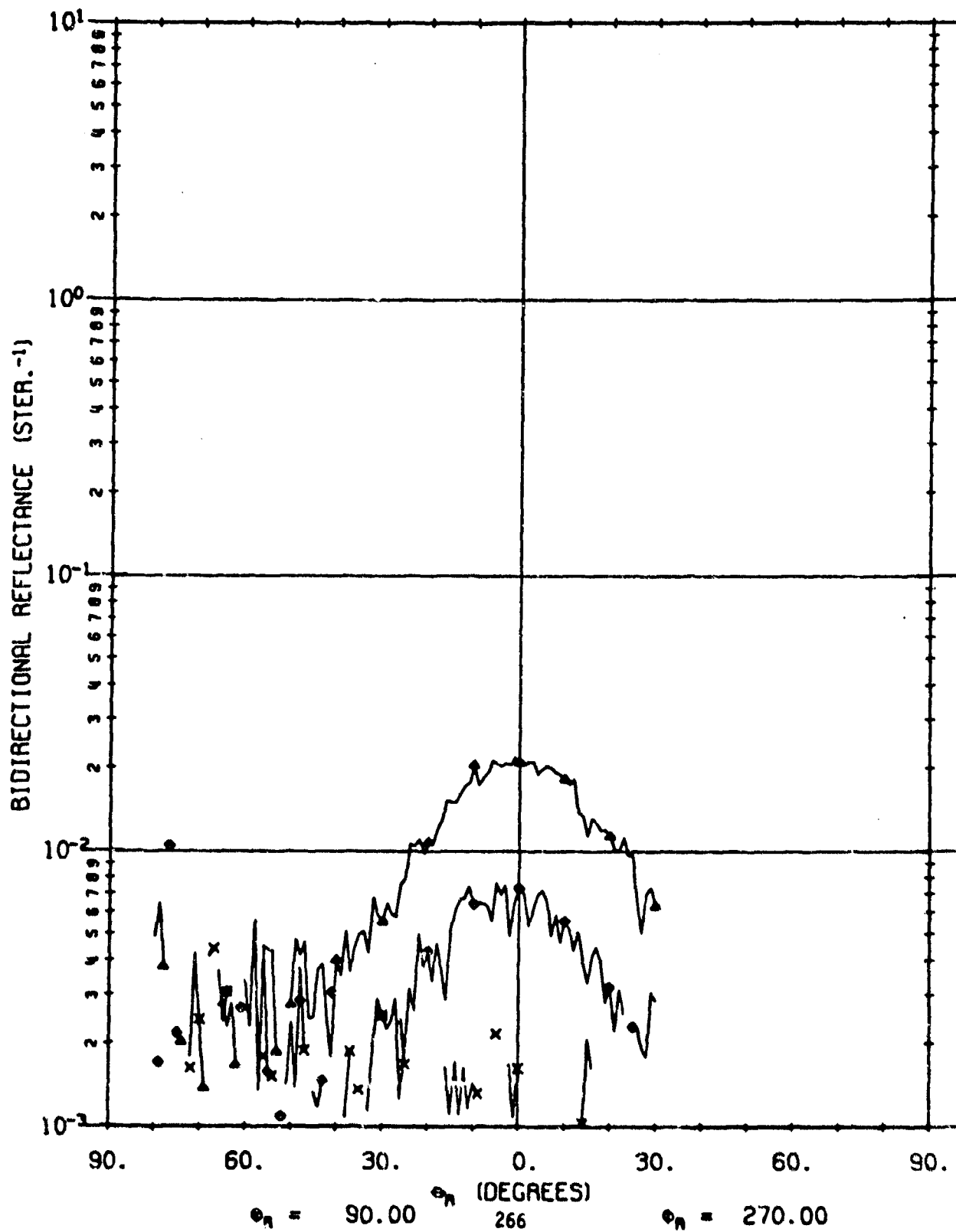
A02023 101

$\lambda = 1.06$   
 $\phi_i = 20.0$   
 $\phi_i = 180.0$



A02023 701

$\lambda = 3.39$   
 $\phi_1 = 20.0$   
 $\phi_2 = 180.0$



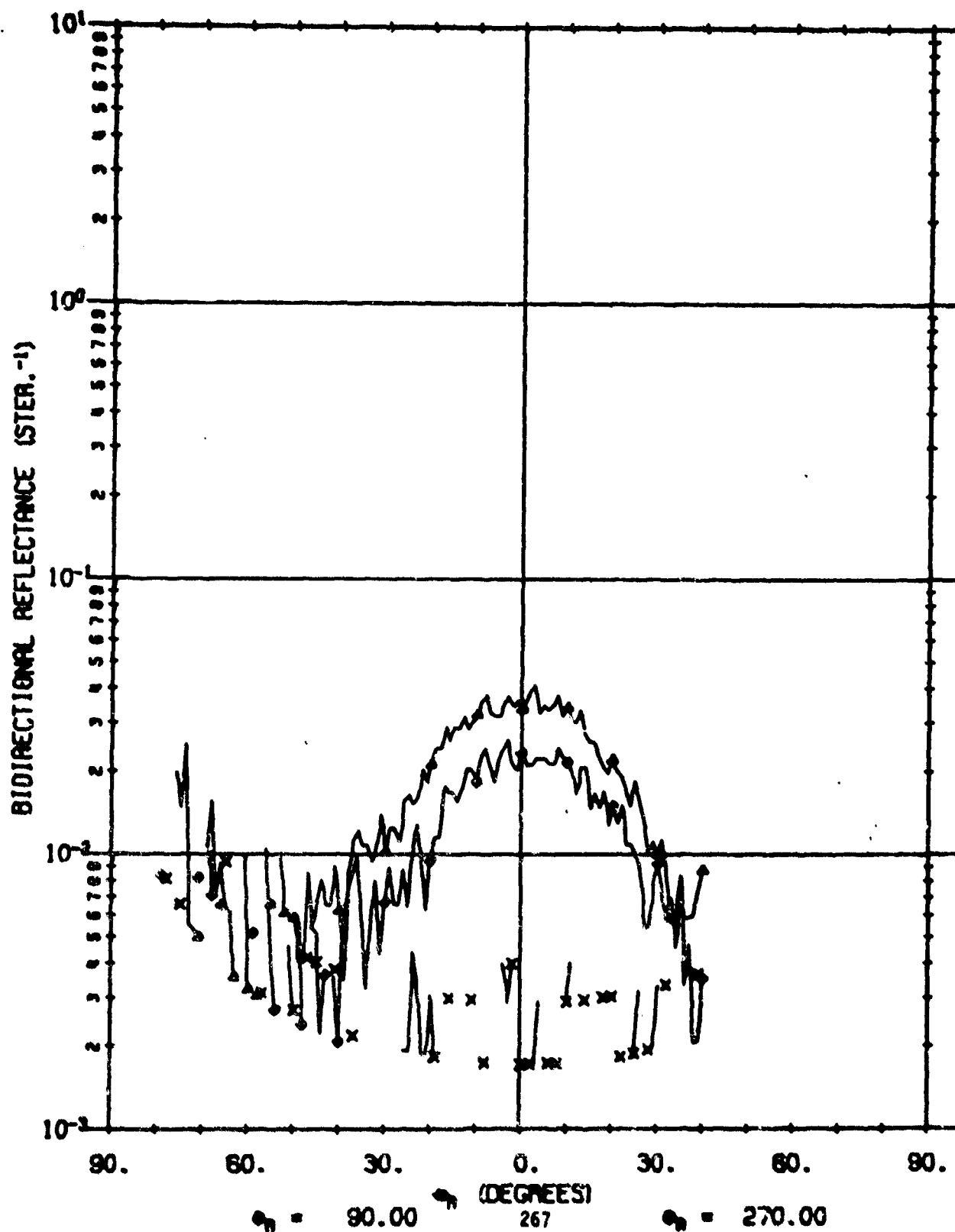
A02023

604

$\lambda = 10.60$

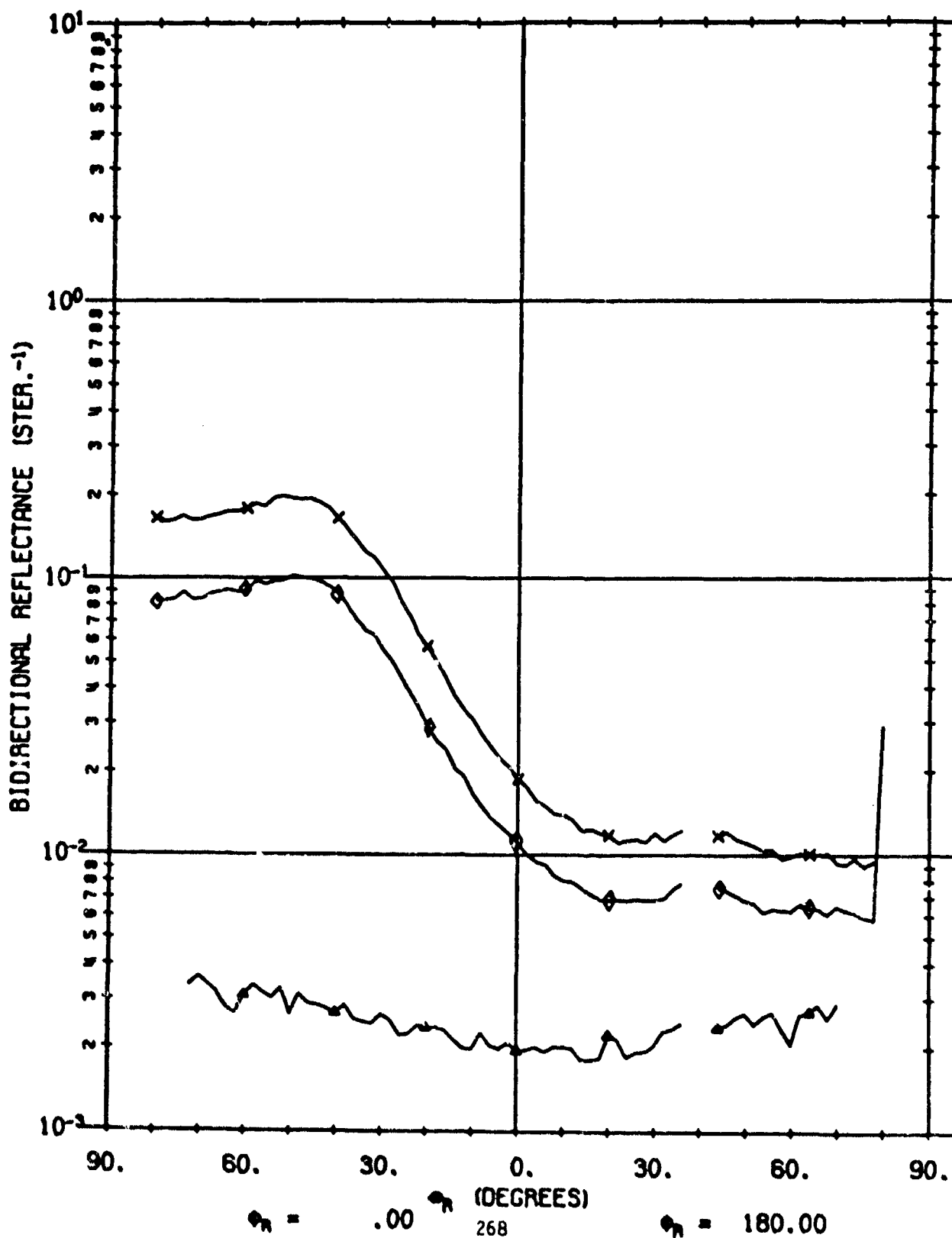
$\phi_i = 20.0$

$\phi_f = 180.0$



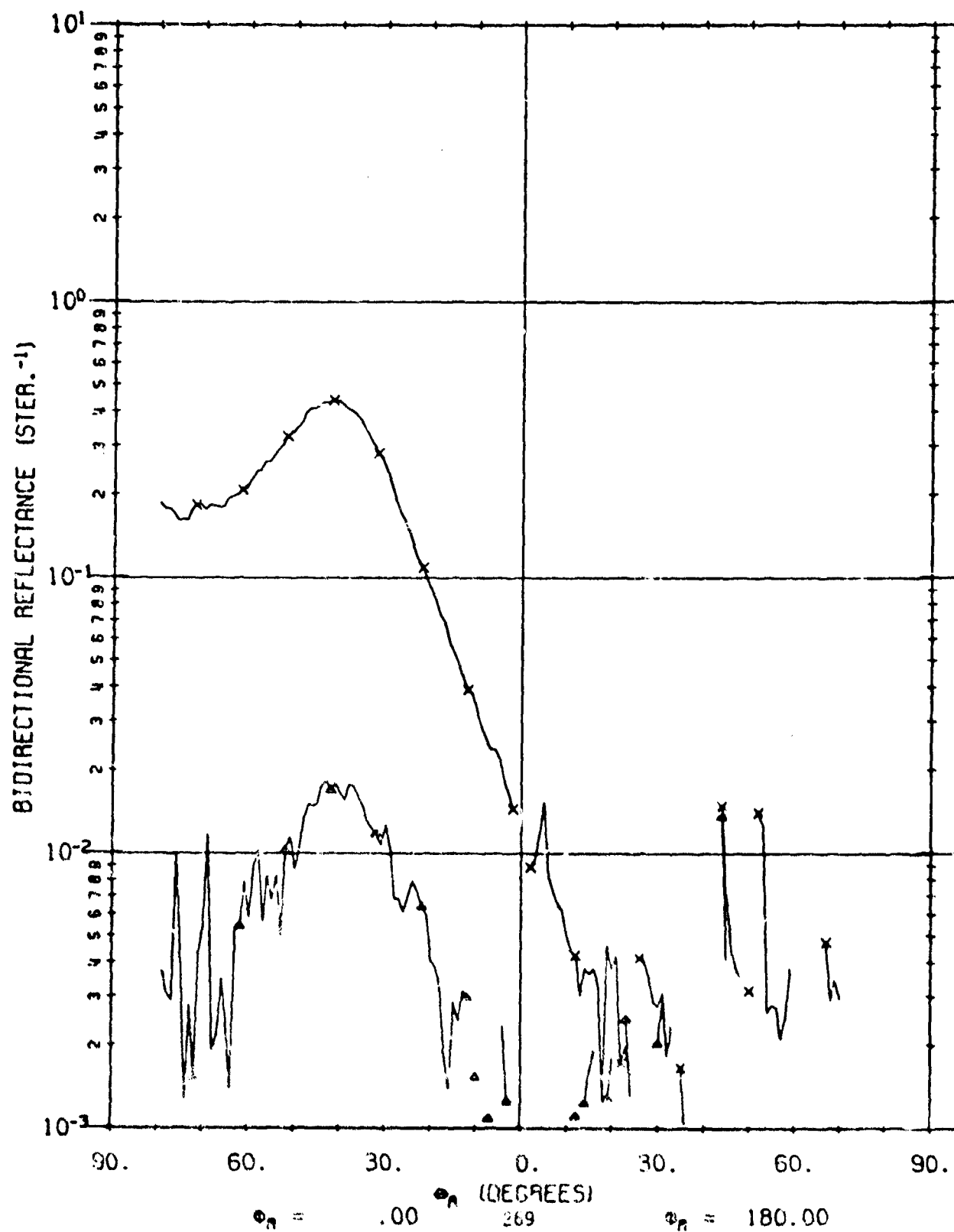
A02023 101

$\lambda = 1.06$   
 $\phi_1 = 40.0$   
 $\phi_2 = 180.0$



A02023 702

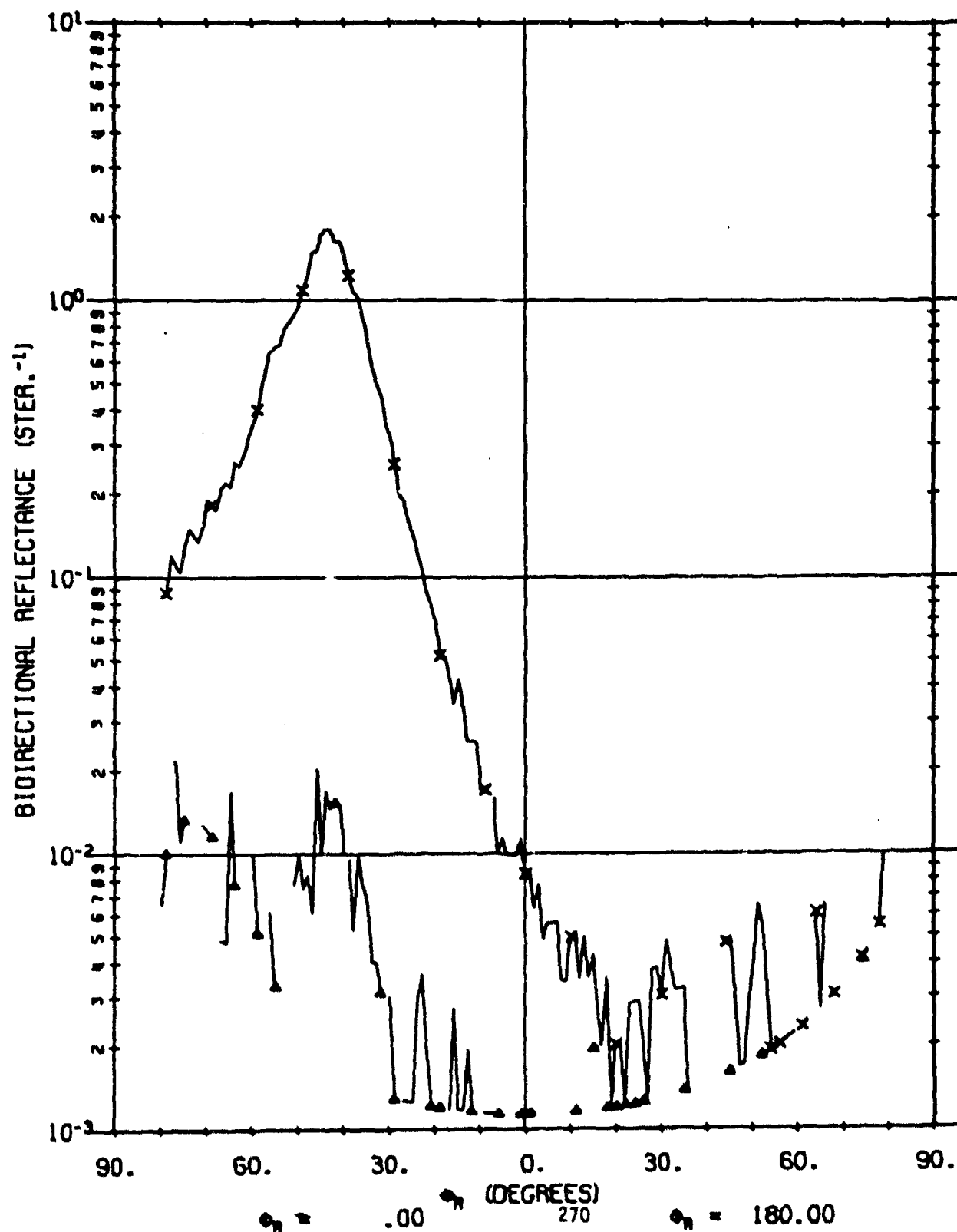
$\lambda = 3.39$   
 $\phi_i = 40.0$   
 $\phi_i = 180.0$





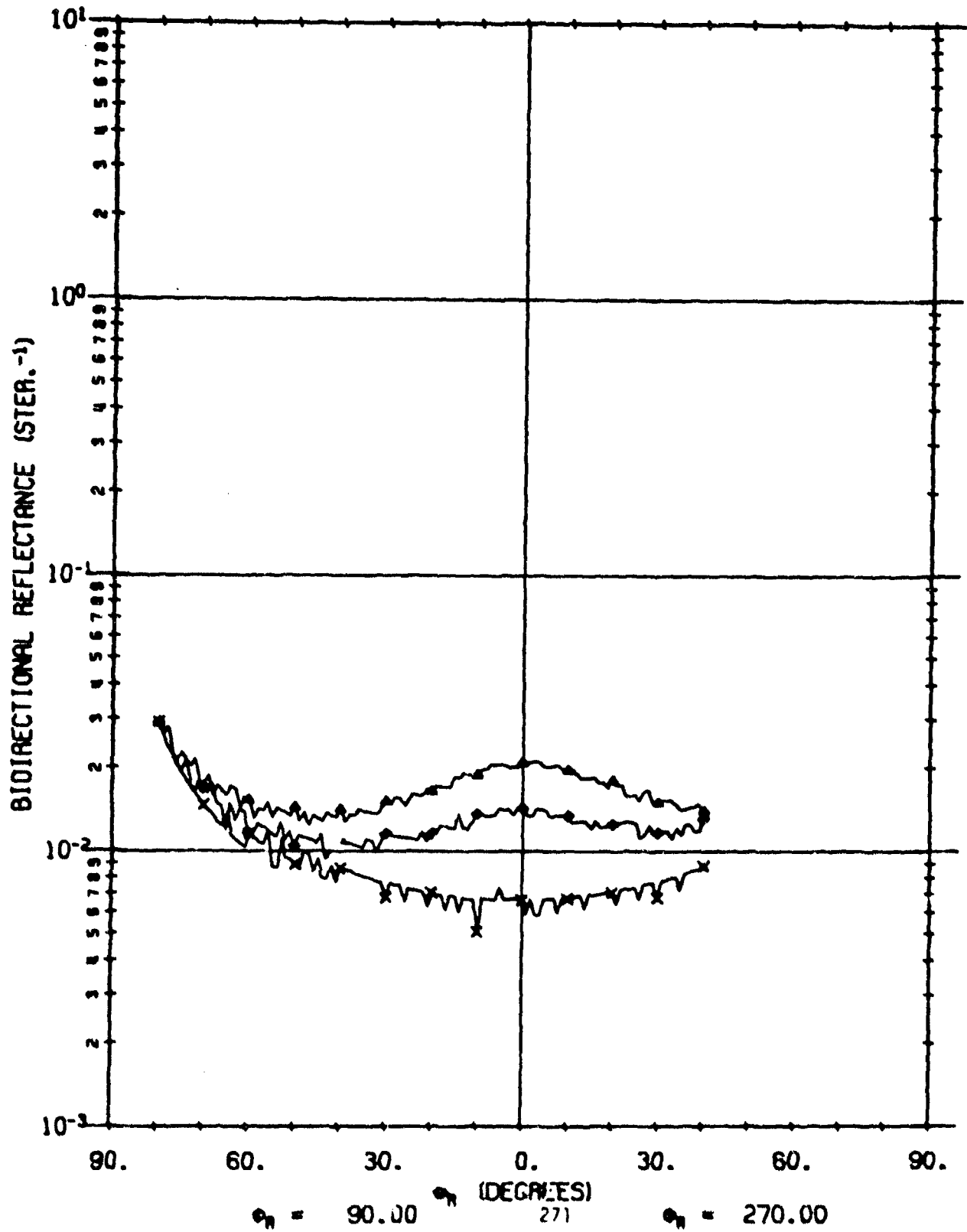
A02023 602

$\lambda = 10.60$   
 $\phi_i = 40.0$   
 $\phi_f = 180.0$



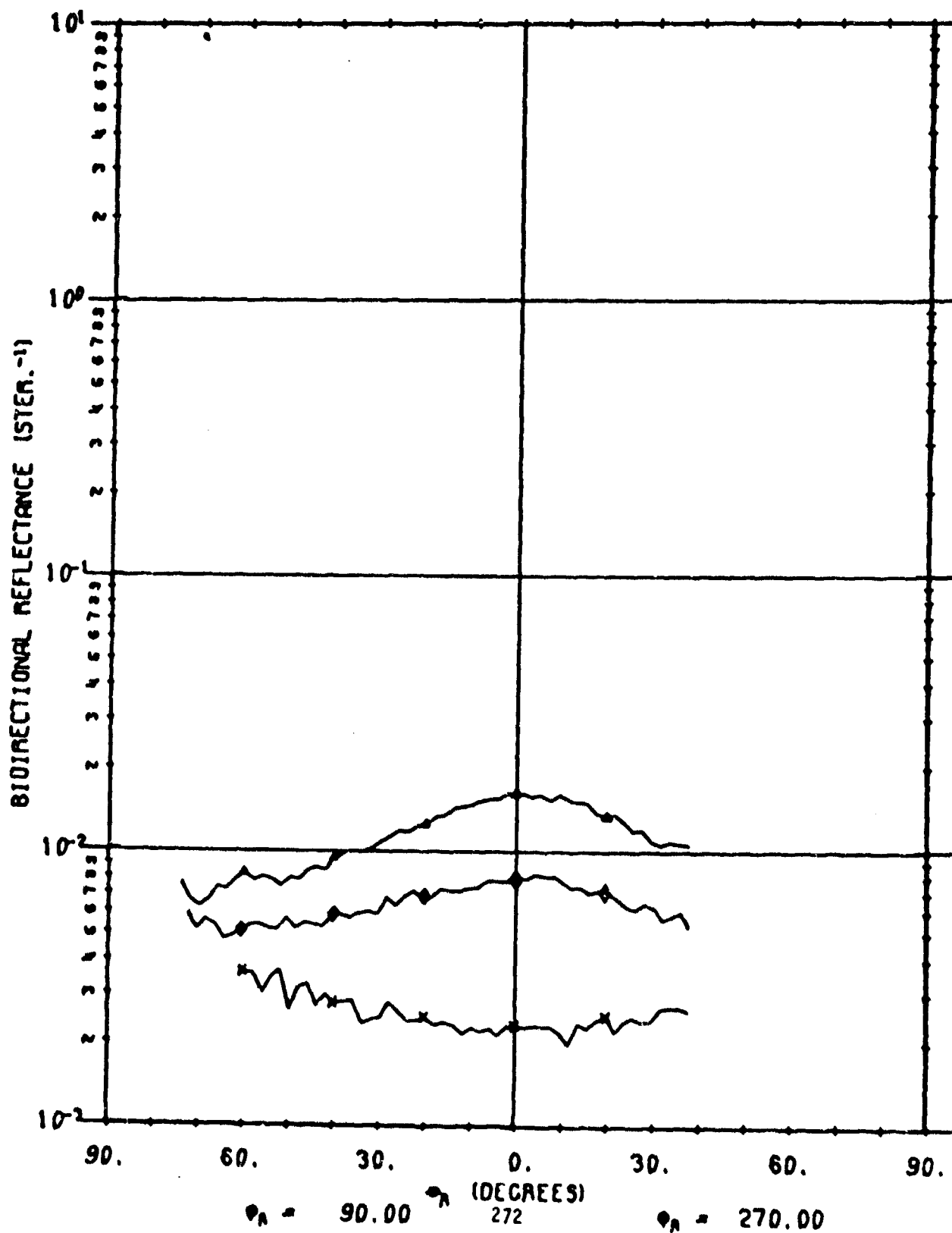
A02023 501

$\lambda = .63$   
 $\phi_i = 40.0$   
 $\phi_r = 180.0$



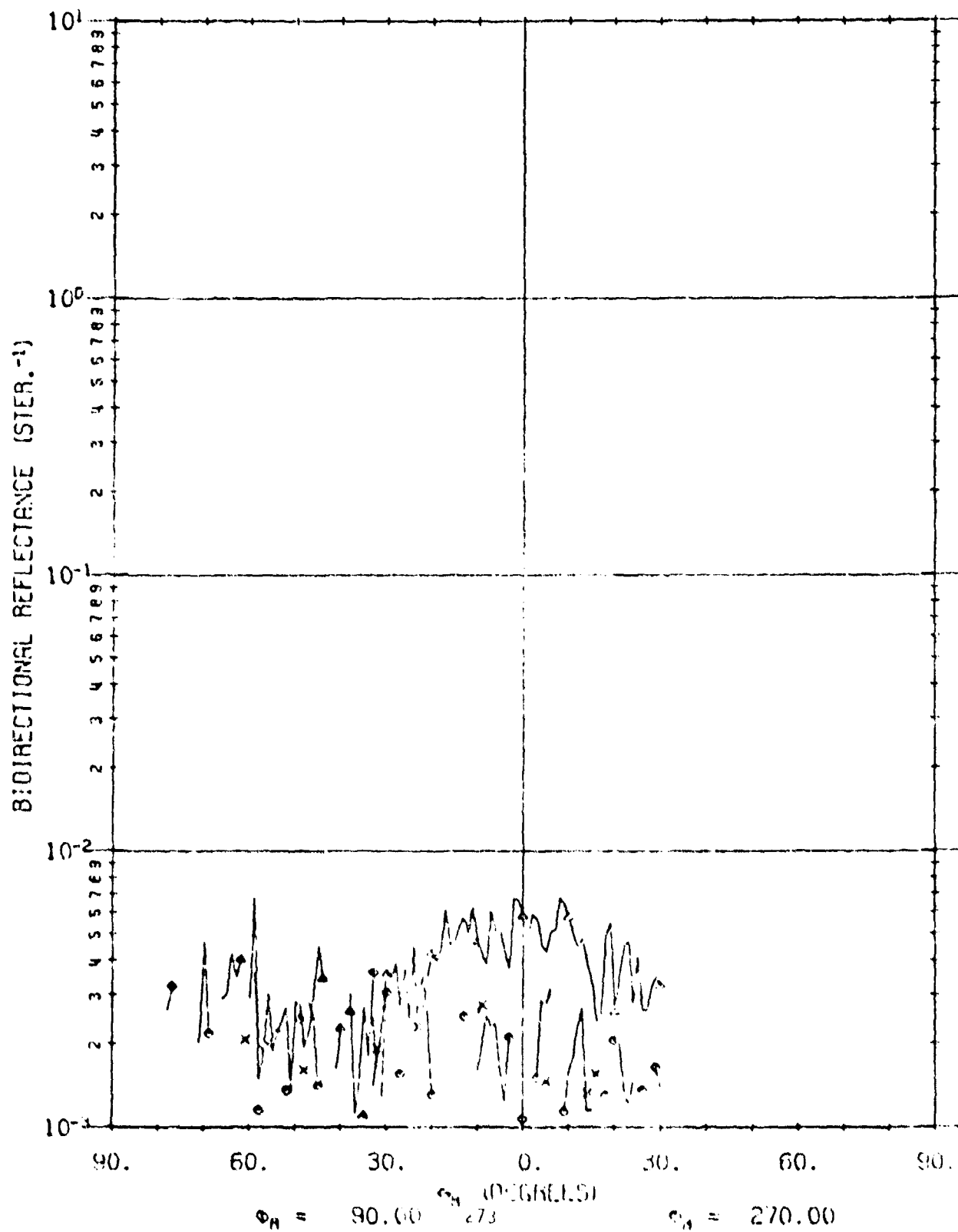
A02023 101

$\lambda = 1.06$   
 $\phi_i = 40.0$   
 $\phi_s = 180.0$



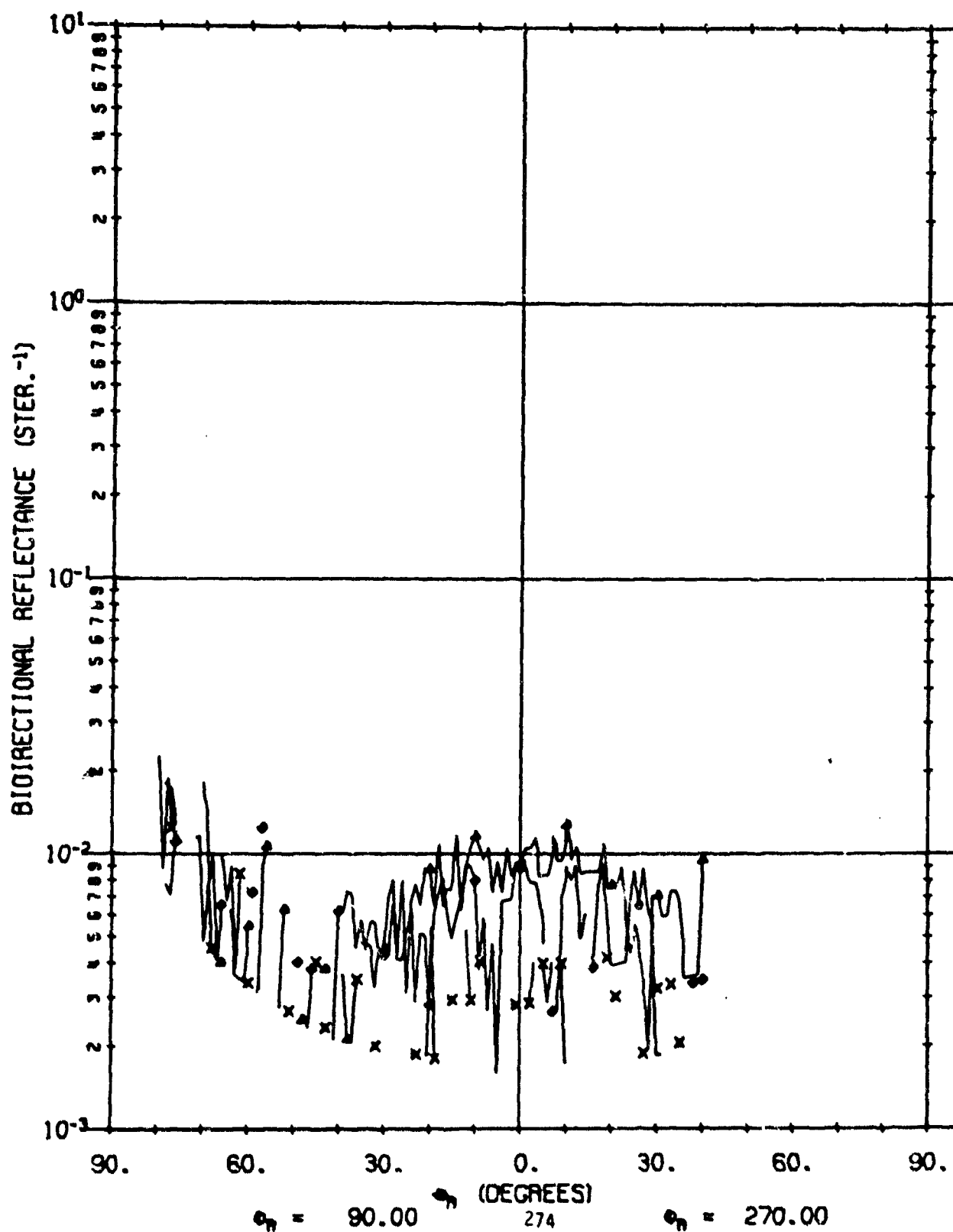
H02023 701

$\lambda = 3.39$   
 $\phi_1 = 40.0$   
 $\phi_2 = 180.0$



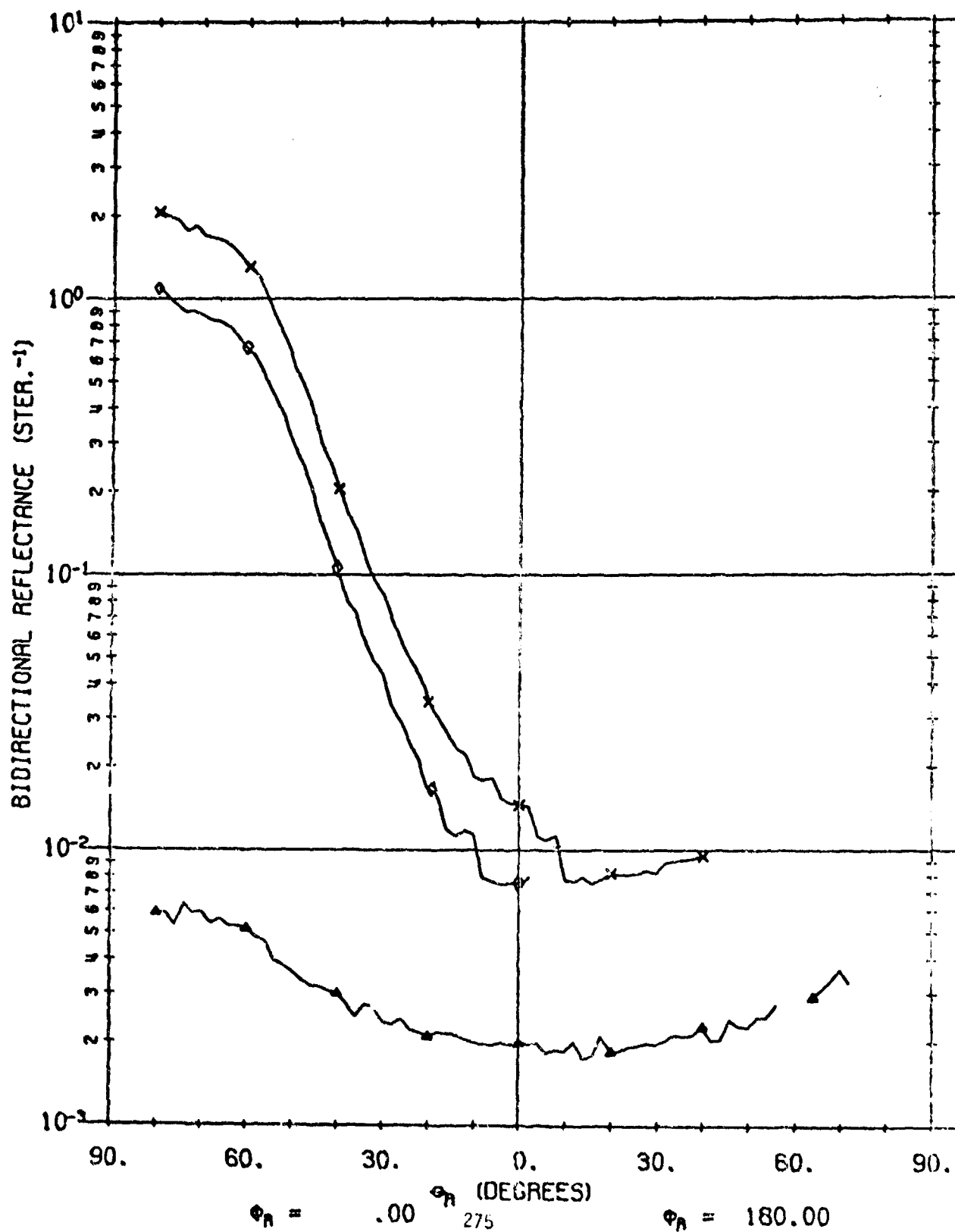
A02023 604

$\lambda = 10.60$   
 $\phi_i = 40.0$   
 $\phi_f = 180.0$



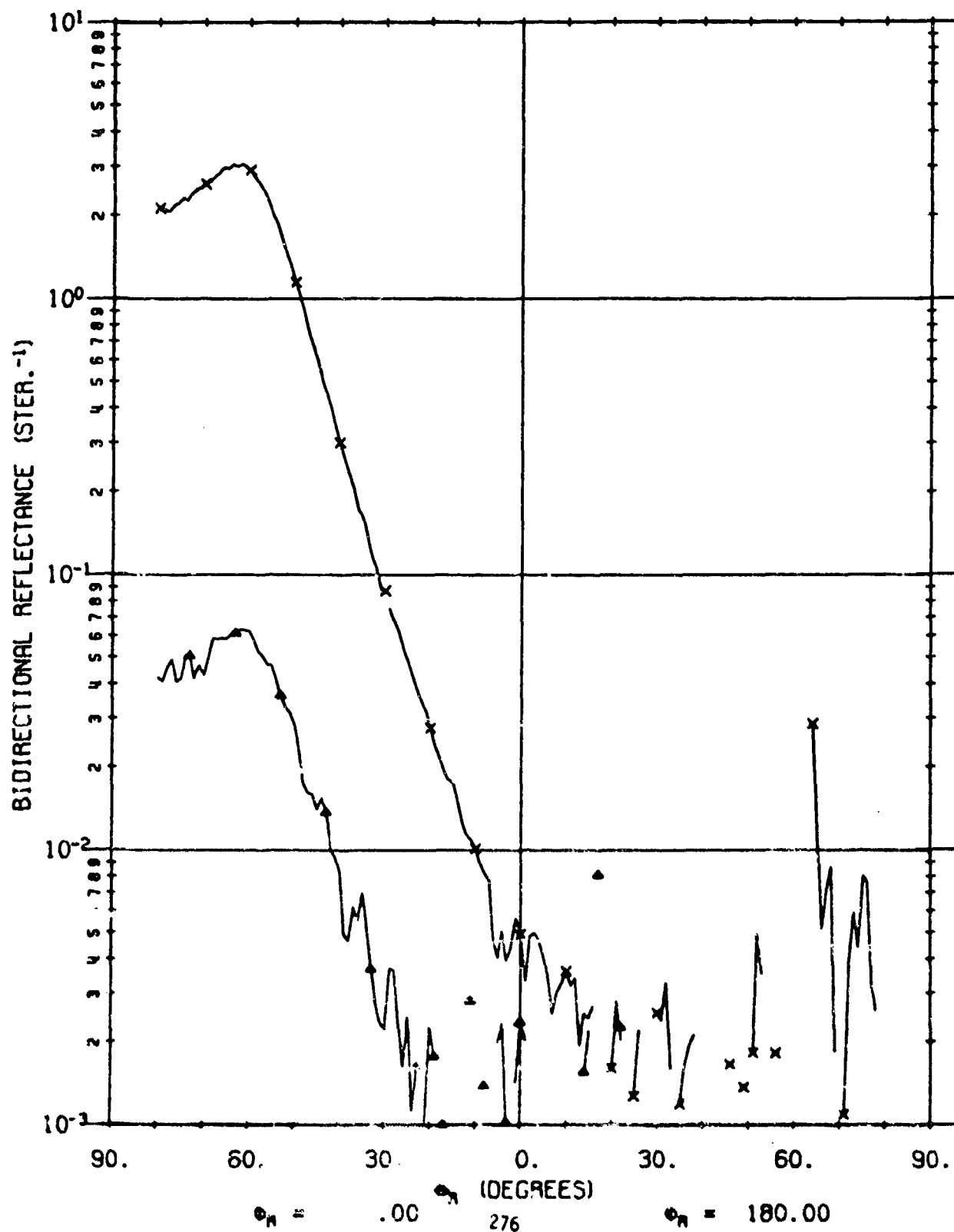
A02023 101

$\lambda = 1.06$   
 $\phi_i = 60.0$   
 $\phi_i = 180.0$



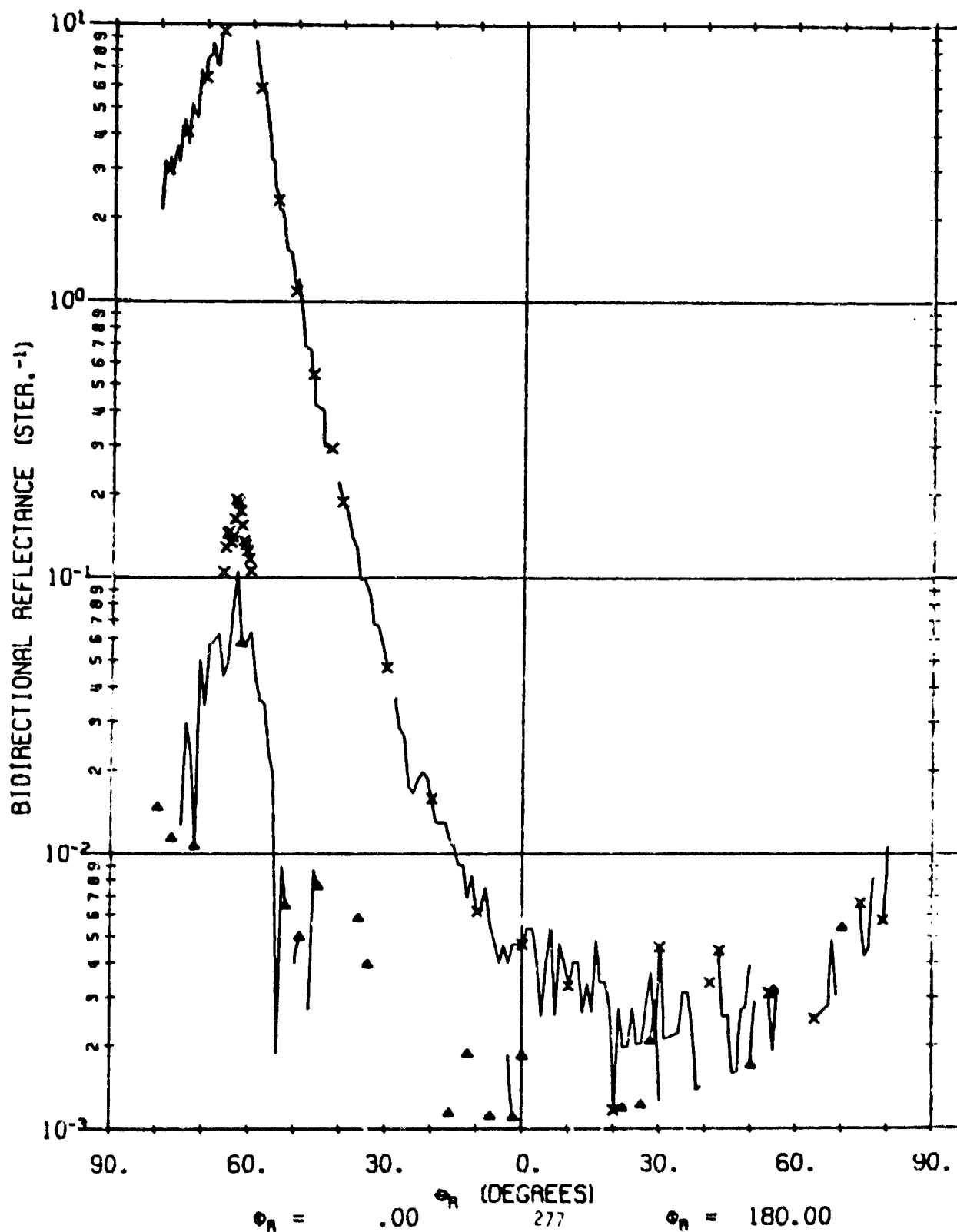
A02023 702

$\lambda = 3.39$   
 $\phi_i = 60.0$   
 $\phi_j = 180.0$



A02023 602

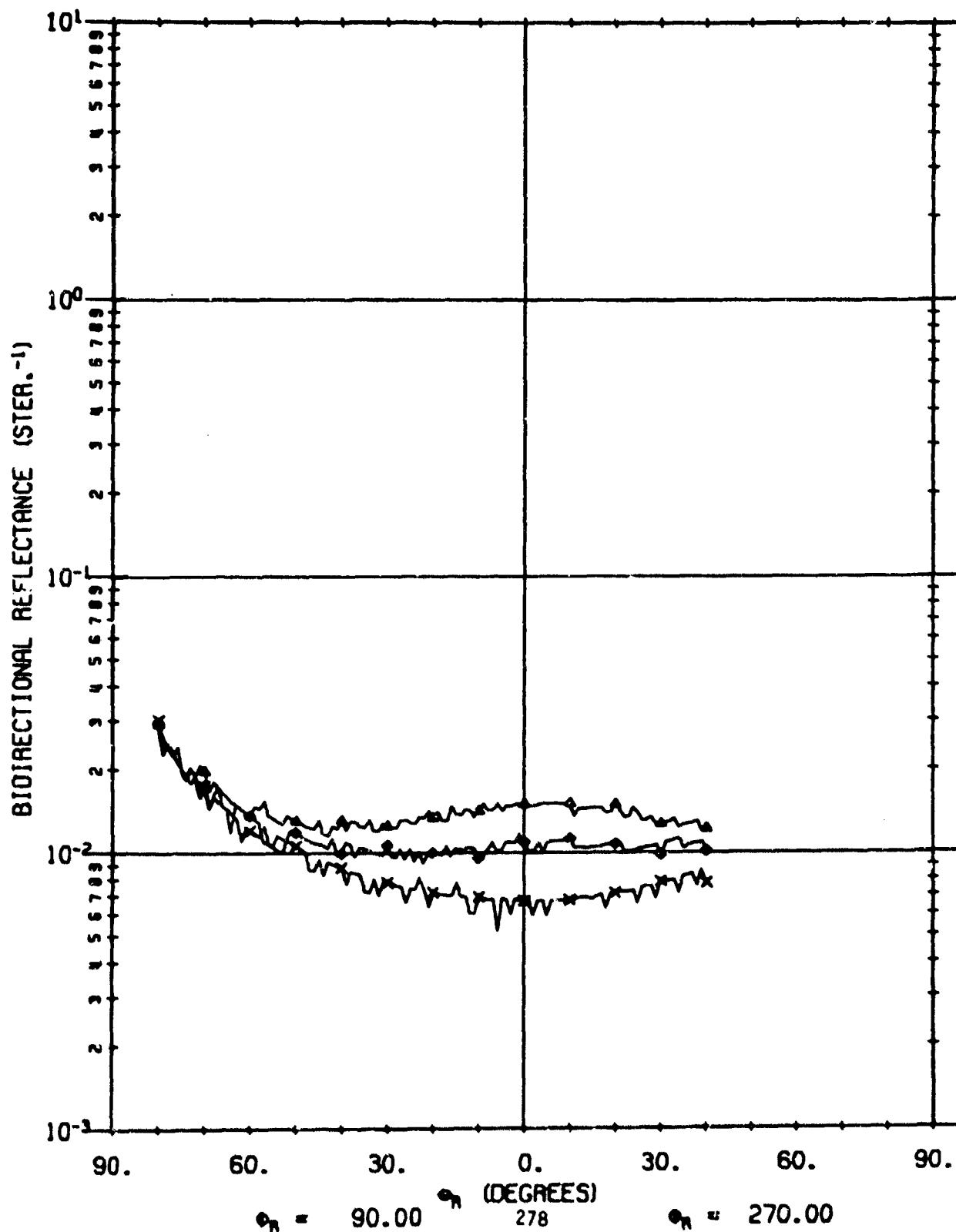
$\lambda = 10.50$   
 $\phi_i = 60.0$   
 $\phi_i = 180.0$





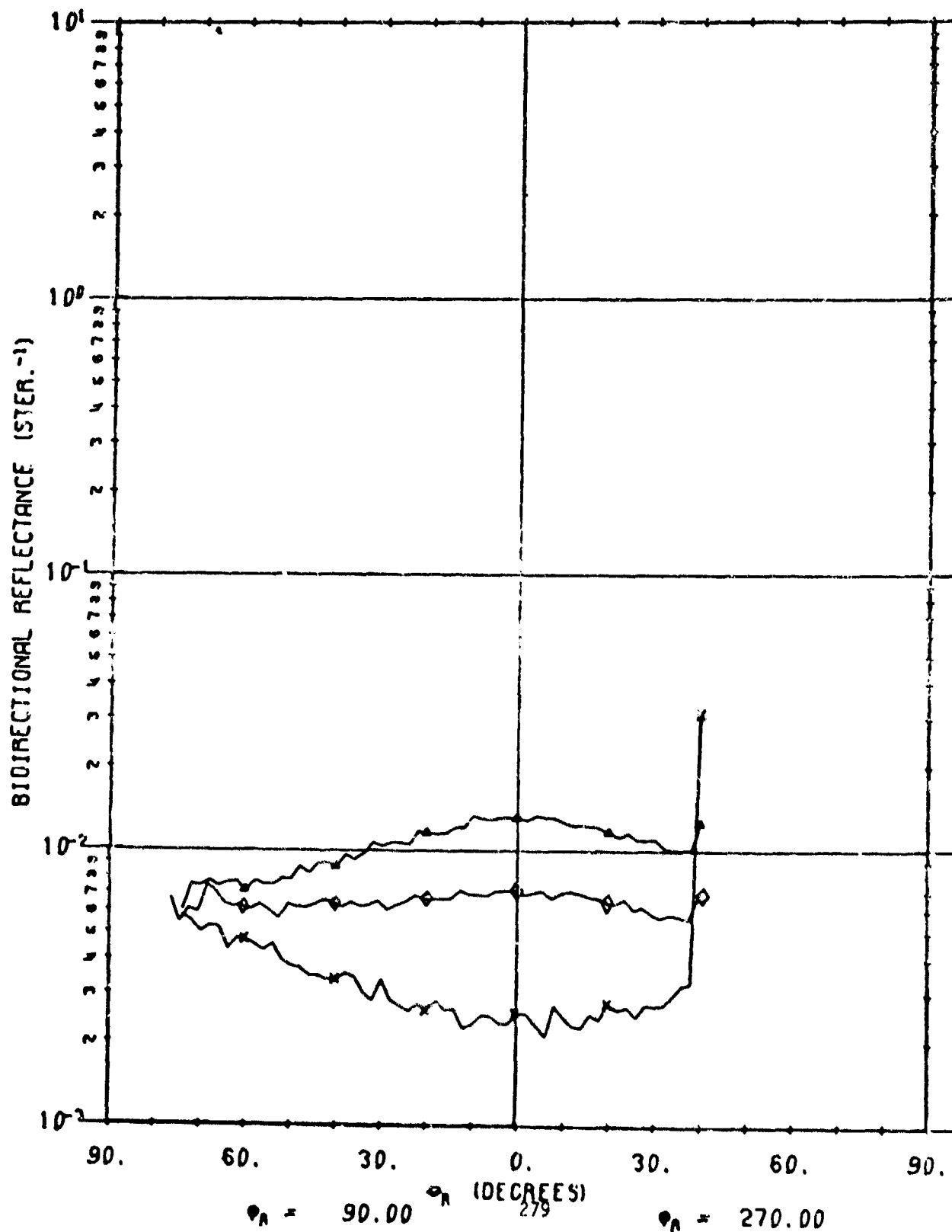
A02023 501

$\lambda = .63$   
 $\phi_i = 60.0$   
 $\phi_i = 180.0$



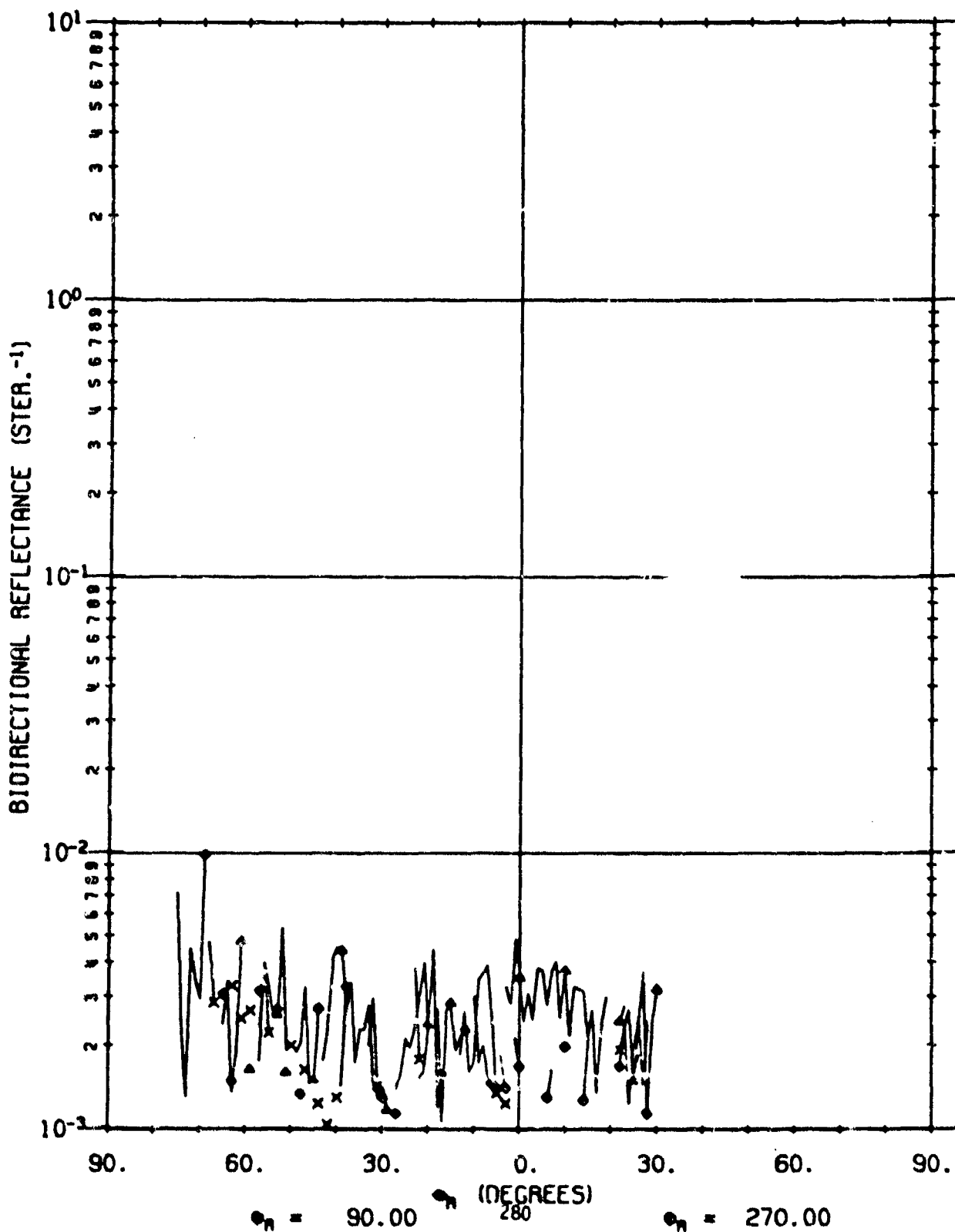
A02023 101

$\lambda = 1.06$   
 $\phi_i = 60.0$   
 $\phi_j = 180.0$



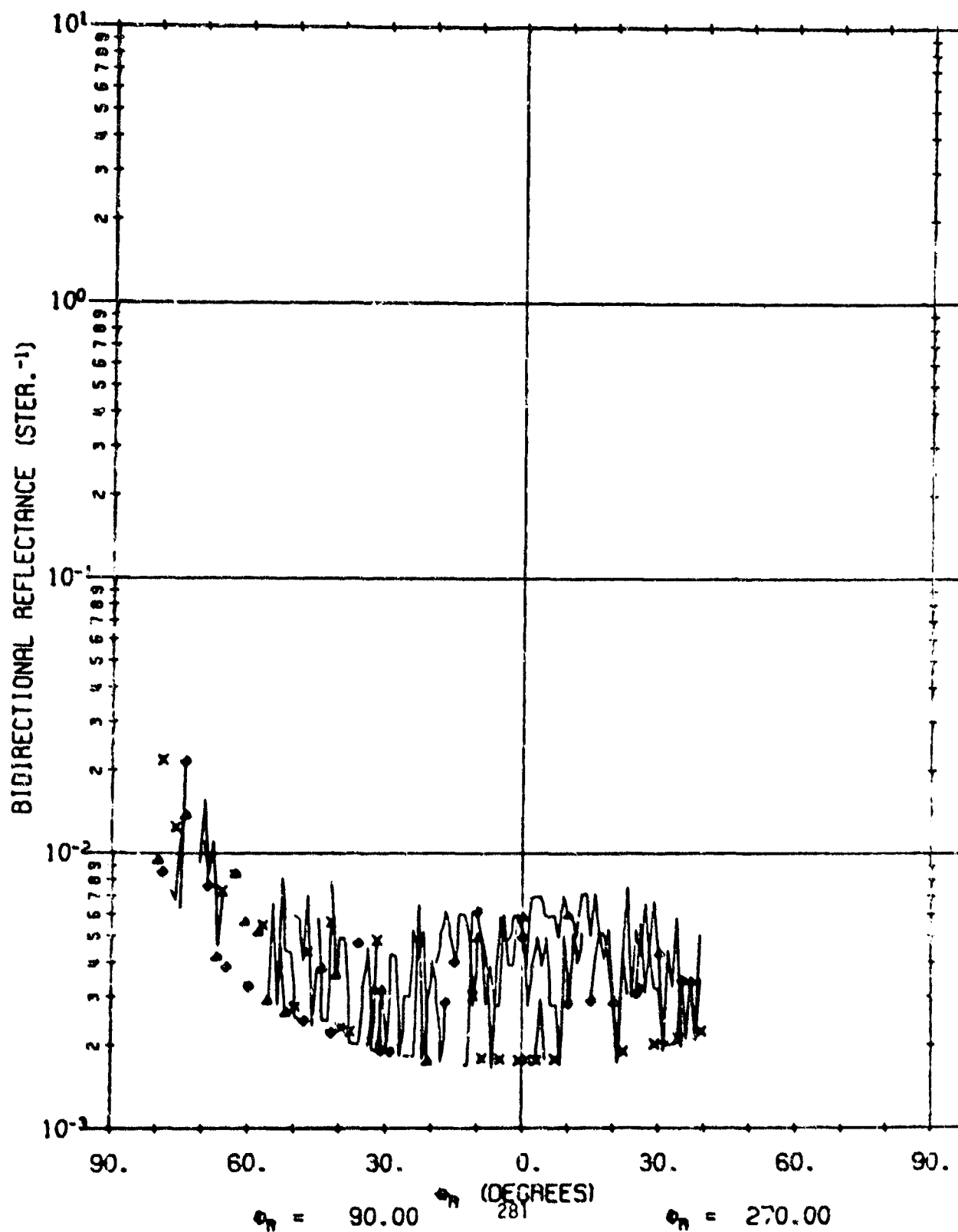
A02023 701

$\lambda = 3.39$   
 $\phi_i = 60.0$   
 $\phi_i = 180.0$



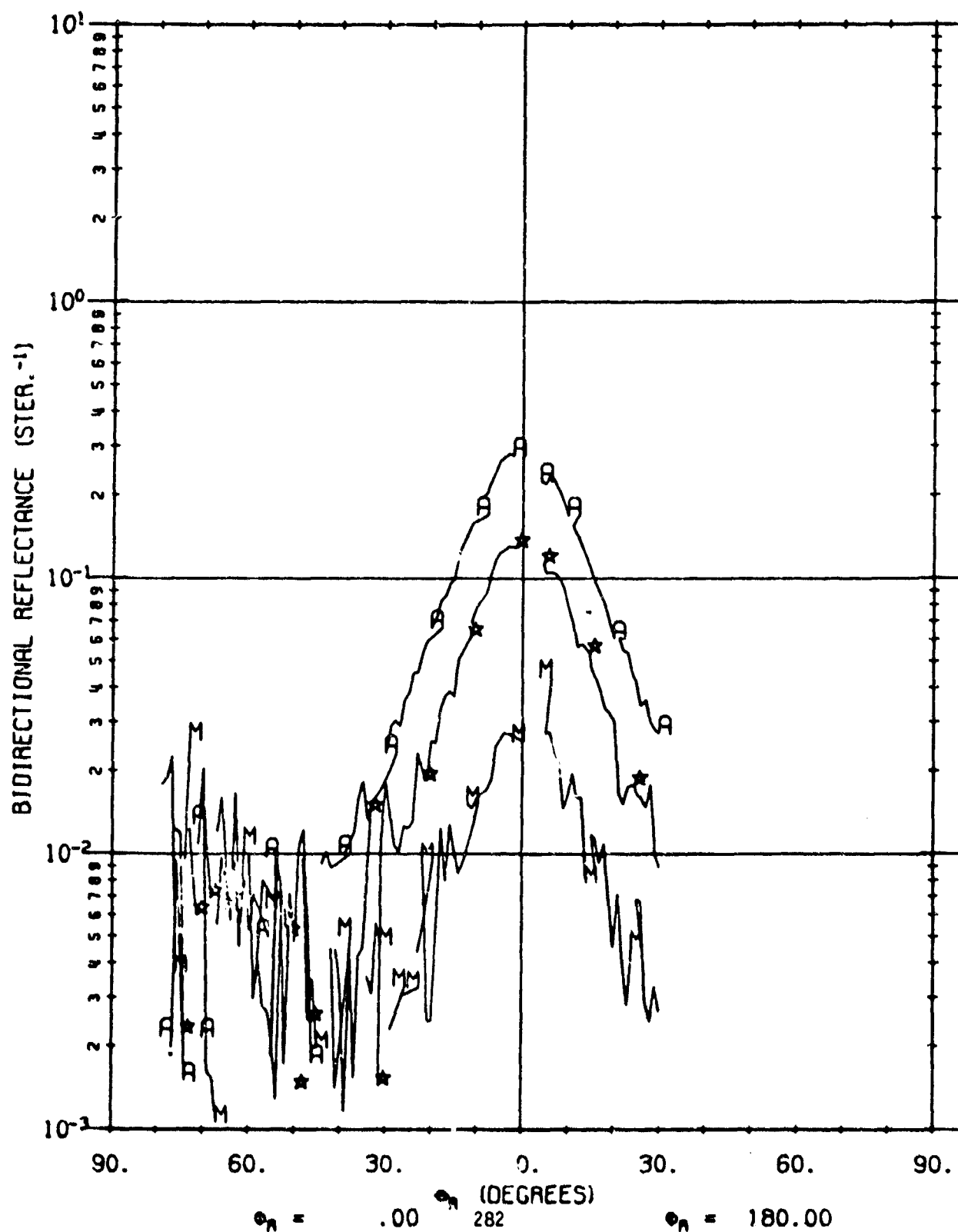
A02023 604

$\lambda = 10.60$   
 $\phi_i = 60.0$   
 $\phi_f = 180.0$



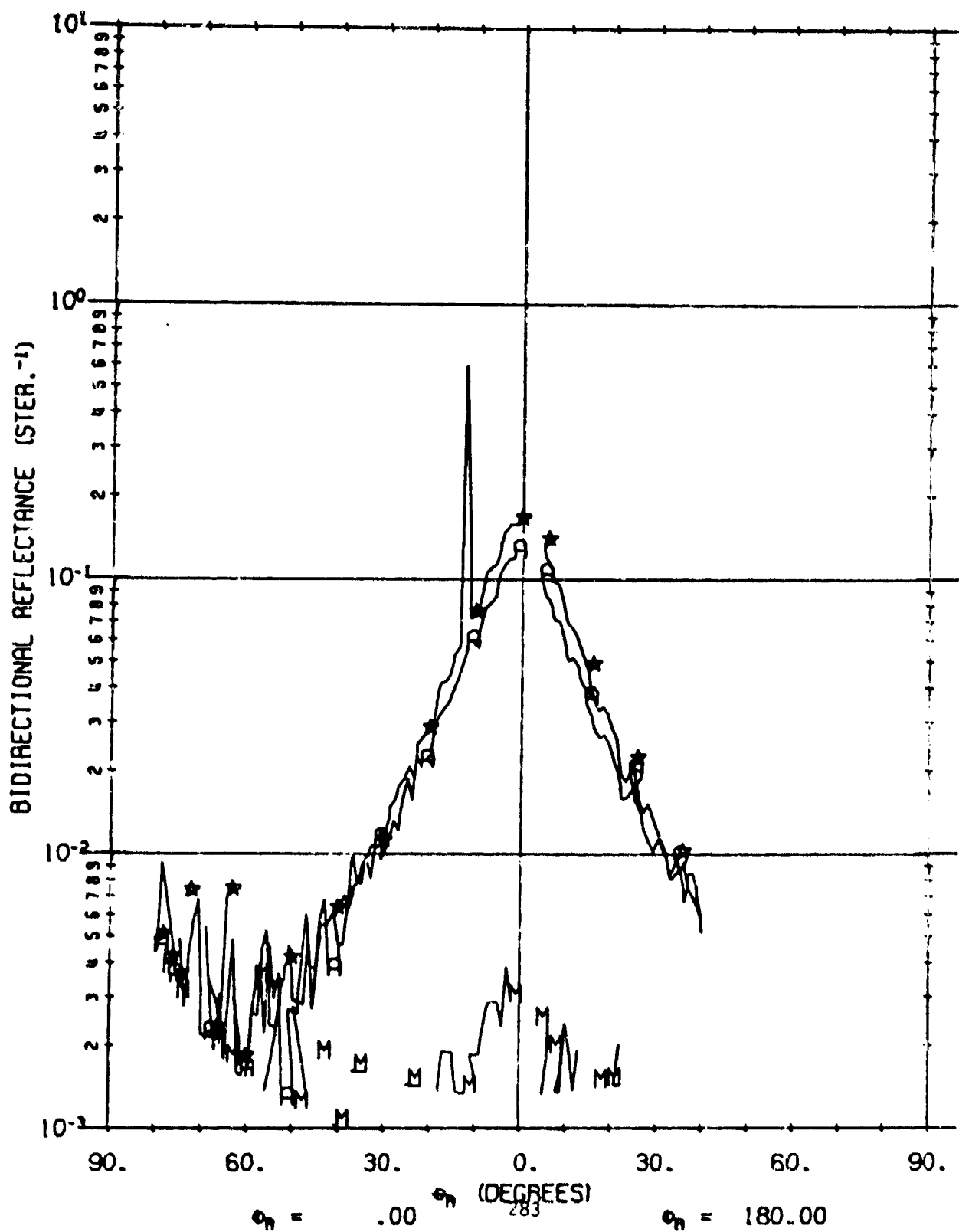
A02023 703

$\lambda = 3.39$   
 $\phi_i = .0$   
 $\phi_f = 180.0$



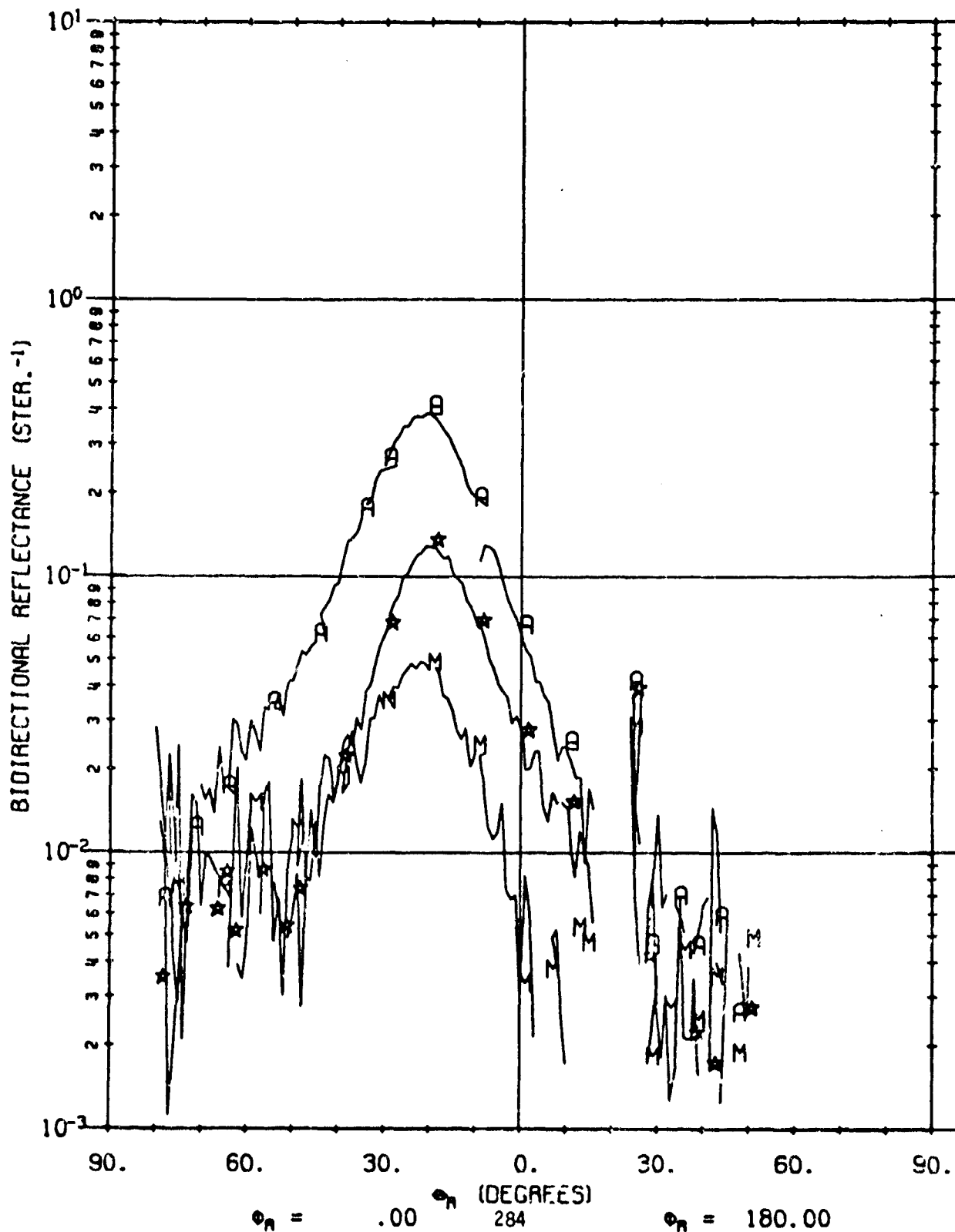
A02023 603

$\lambda = 10.60$   
 $\phi_i = .0$   
 $\phi_f = 180.0$



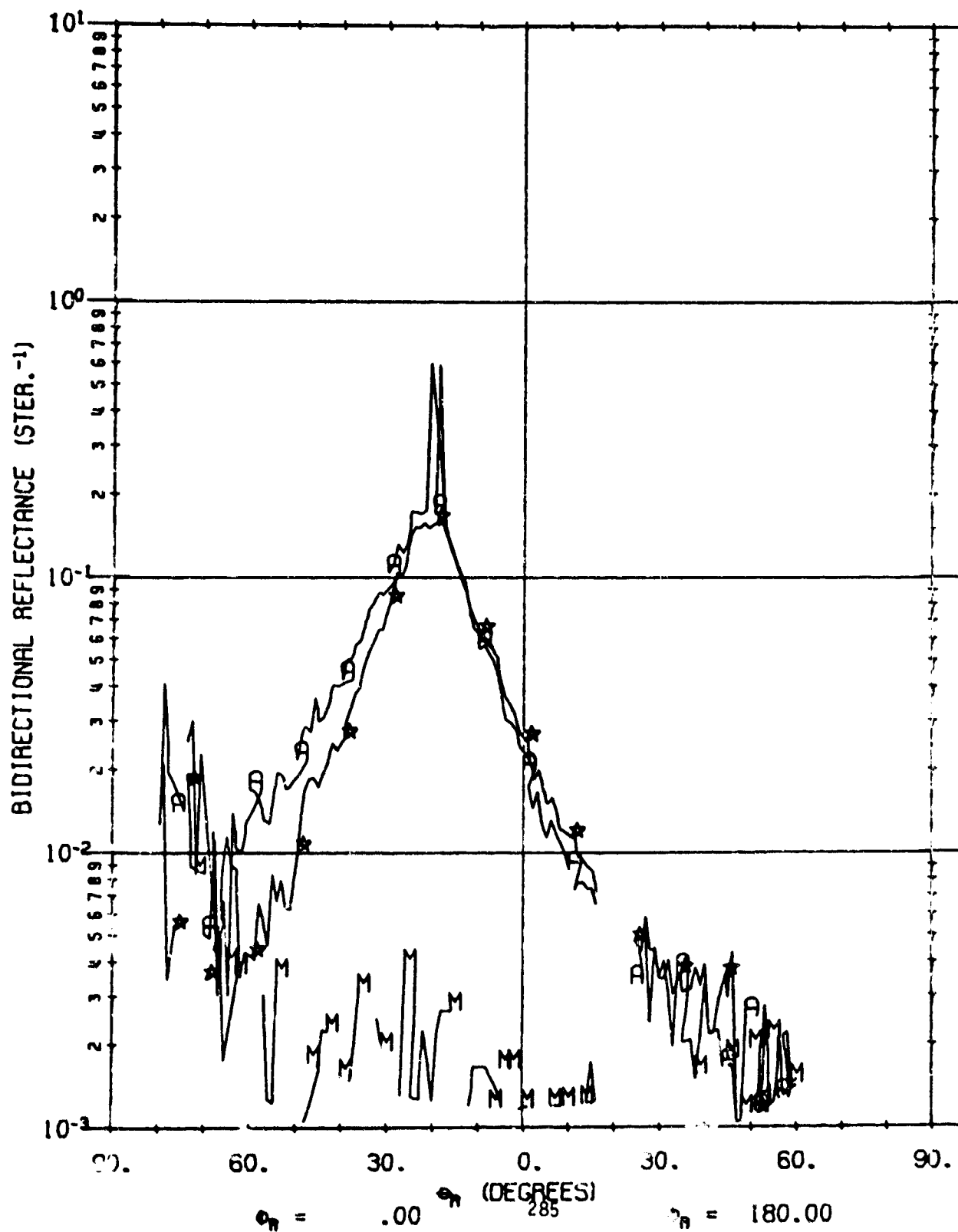
A02023 703

$\lambda$  = 3.39  
 $\phi_i$  = 20.0  
 $\phi_r$  = 180.0



A02023 603

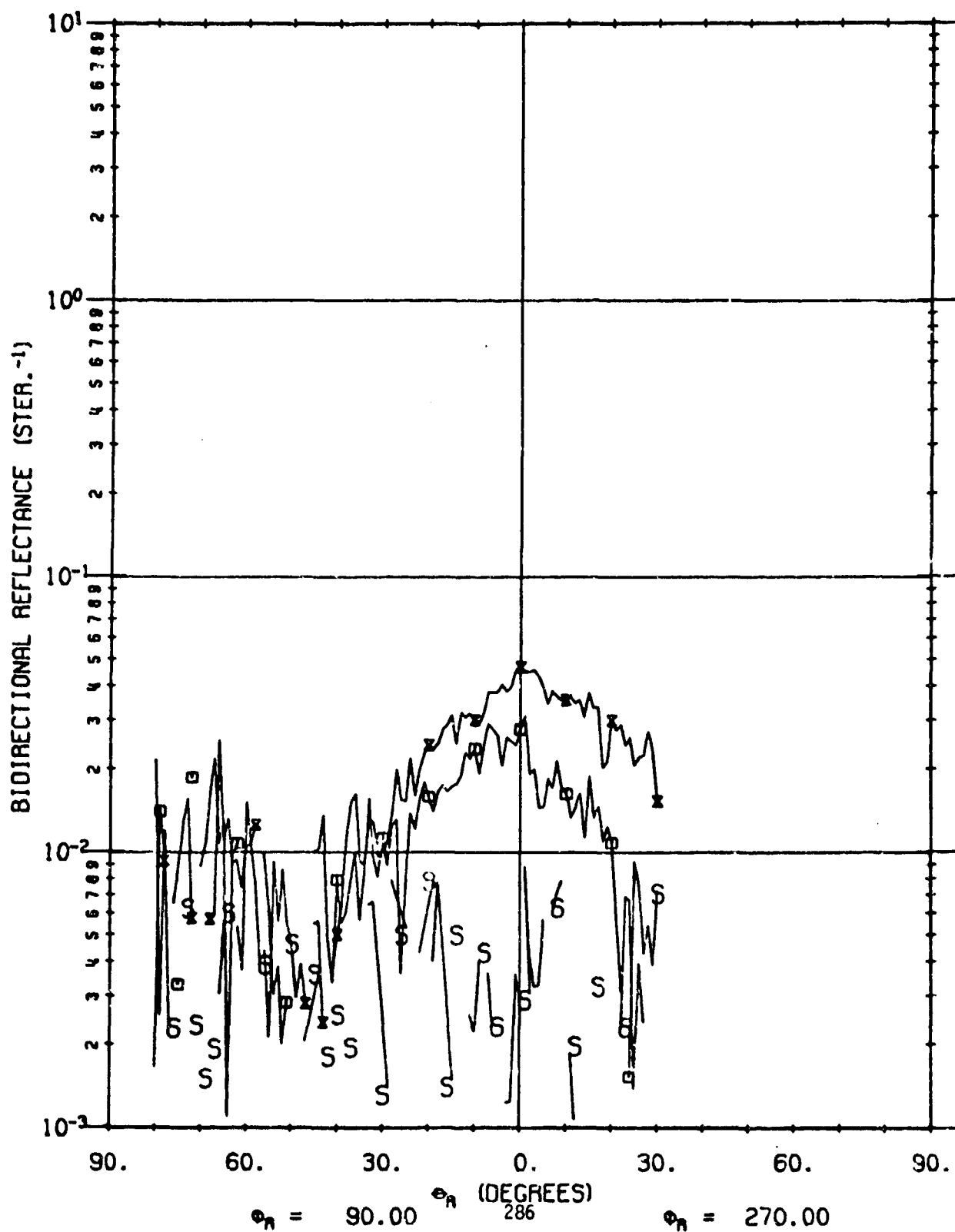
$\lambda = 10.60$   
 $\phi_i = 20.0$   
 $\phi_t = 180.0$





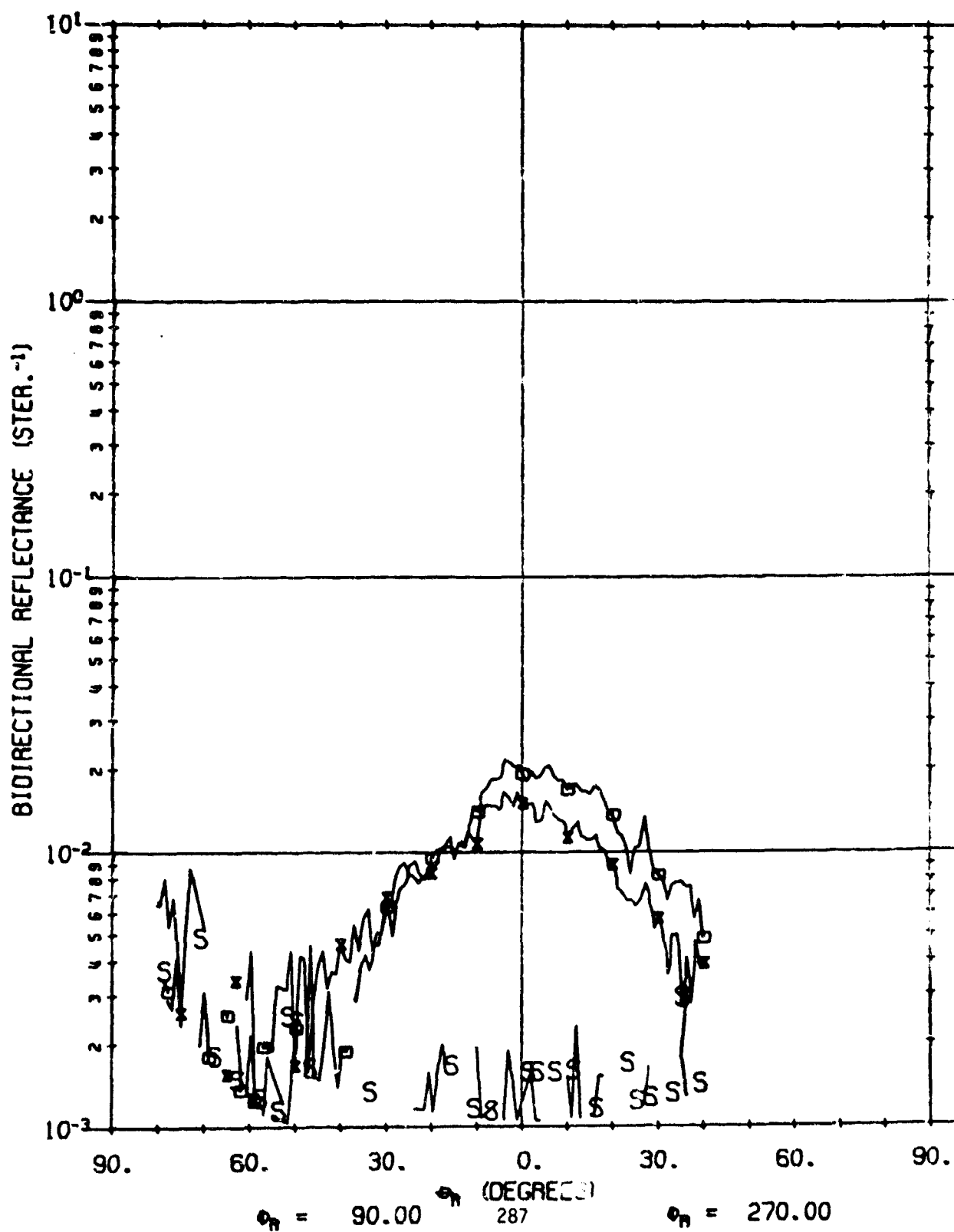
A02023 703

$\lambda = 3.39$   
 $\phi_1 = 20.0$   
 $\phi_2 = 180.0$



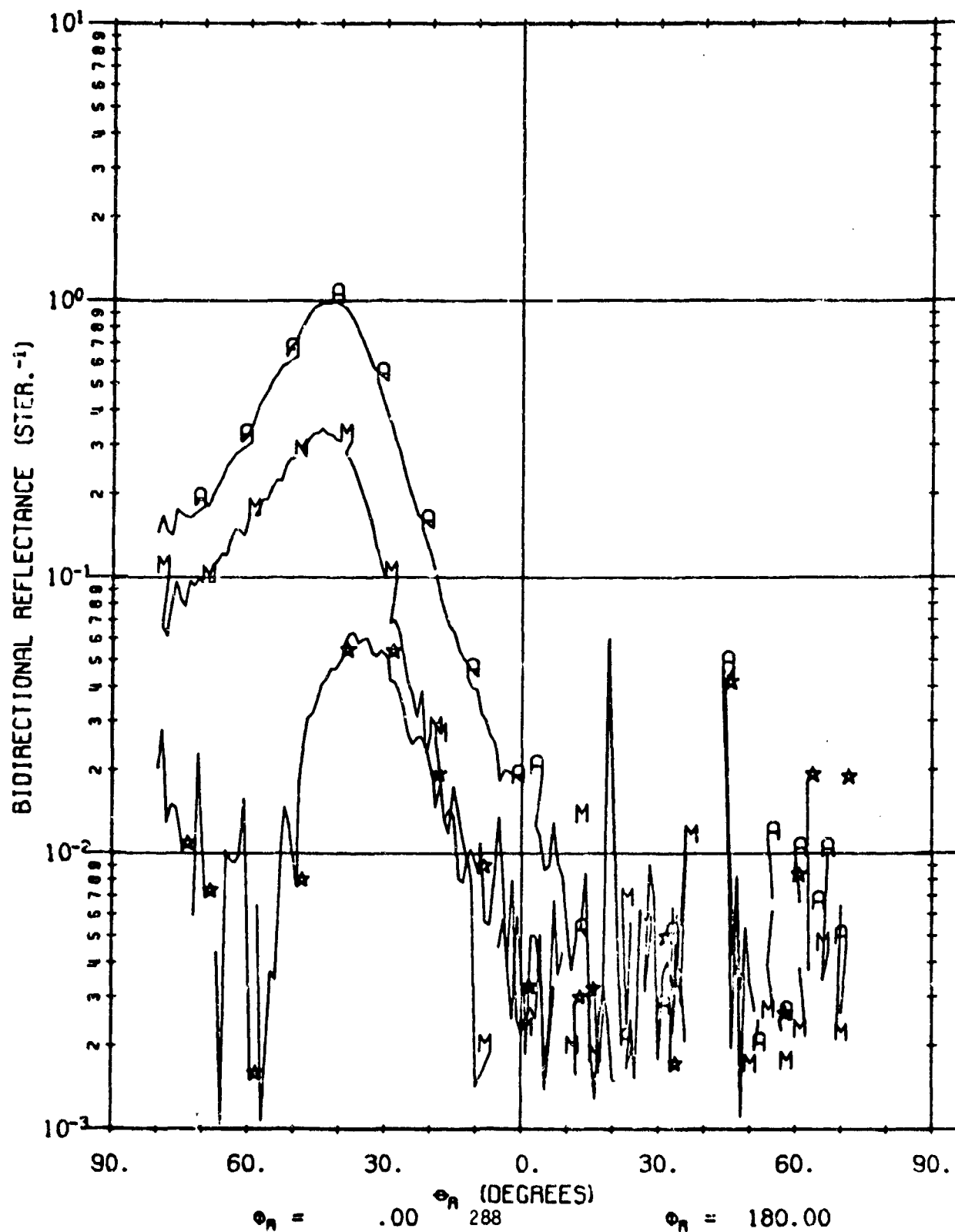
A02023 603

$\lambda = 10.60$   
 $\phi_i = 20.0$   
 $\phi_f = 180.0$



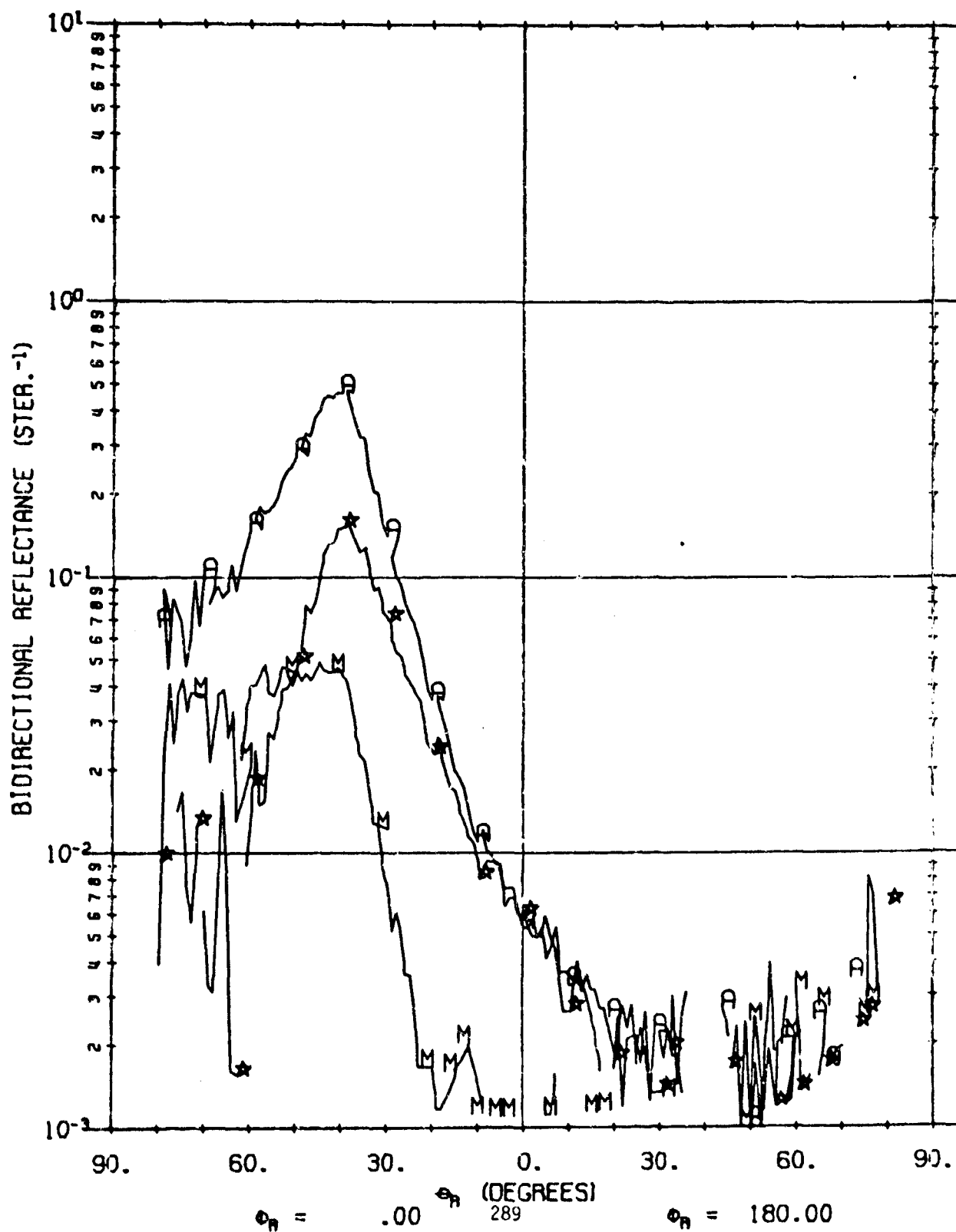
A02023 703

$\lambda = 3.39$   
 $\phi_i = 40.0$   
 $\phi_i = 180.0$



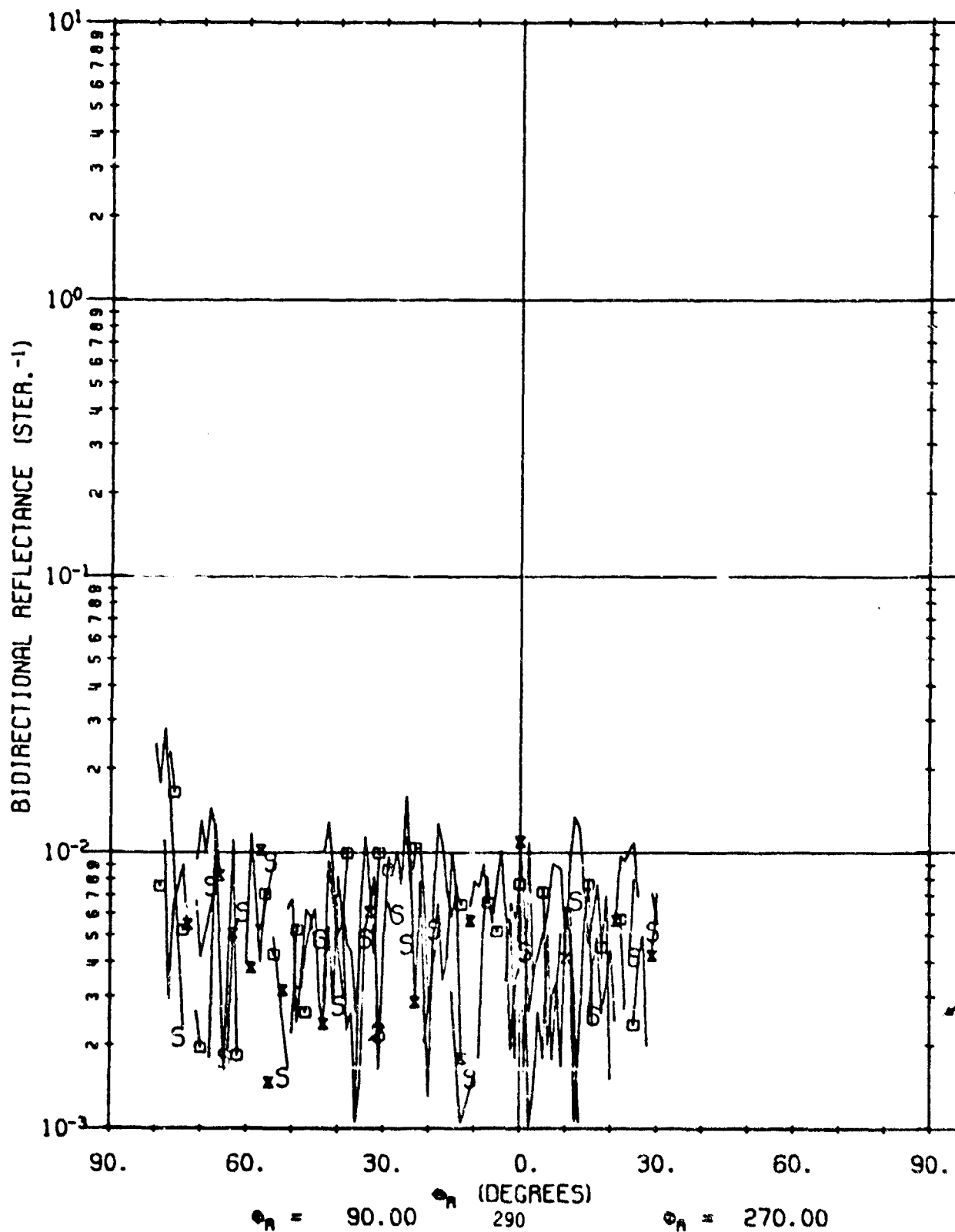
A02023 603

$\lambda = 10.60$   
 $\phi_i = 40.0$   
 $\phi_r = 180.0$



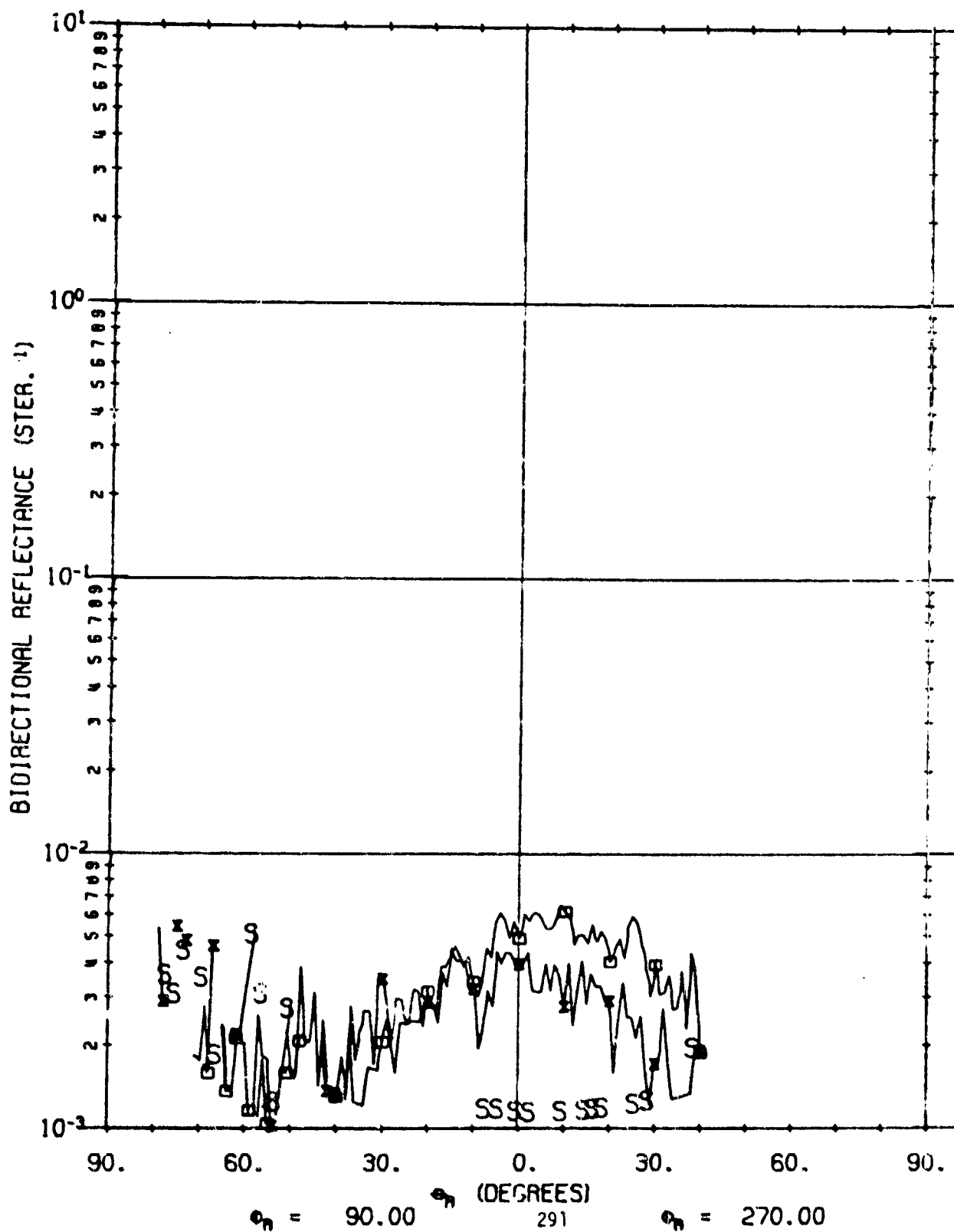
A02023 703

$\lambda = 3.39$   
 $\phi_1 = 40.0$   
 $\phi_2 = 180.0$



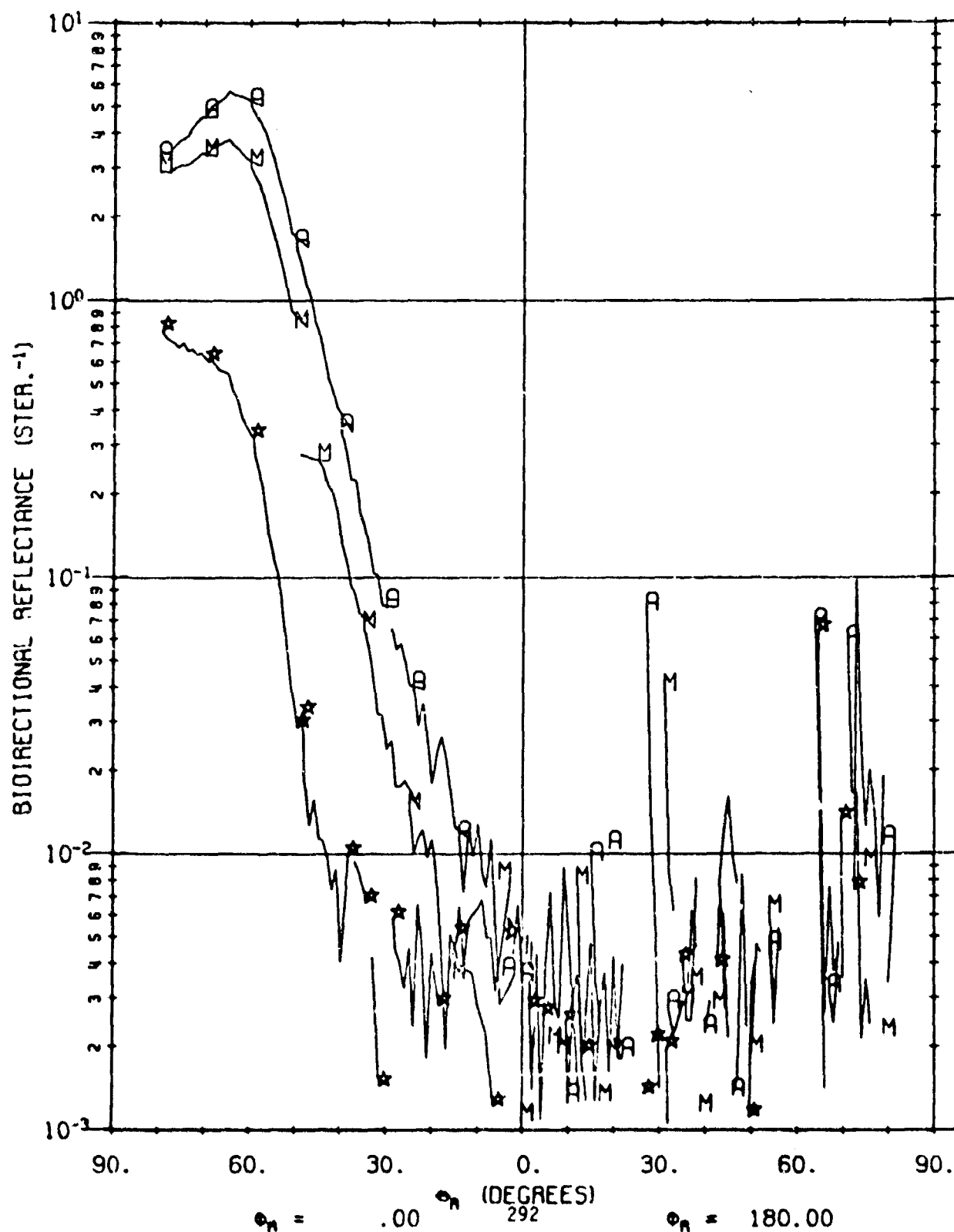
A02023 603

$\lambda = 10.60$   
 $\phi_i = 40.0$   
 $\phi_f = 180.0$



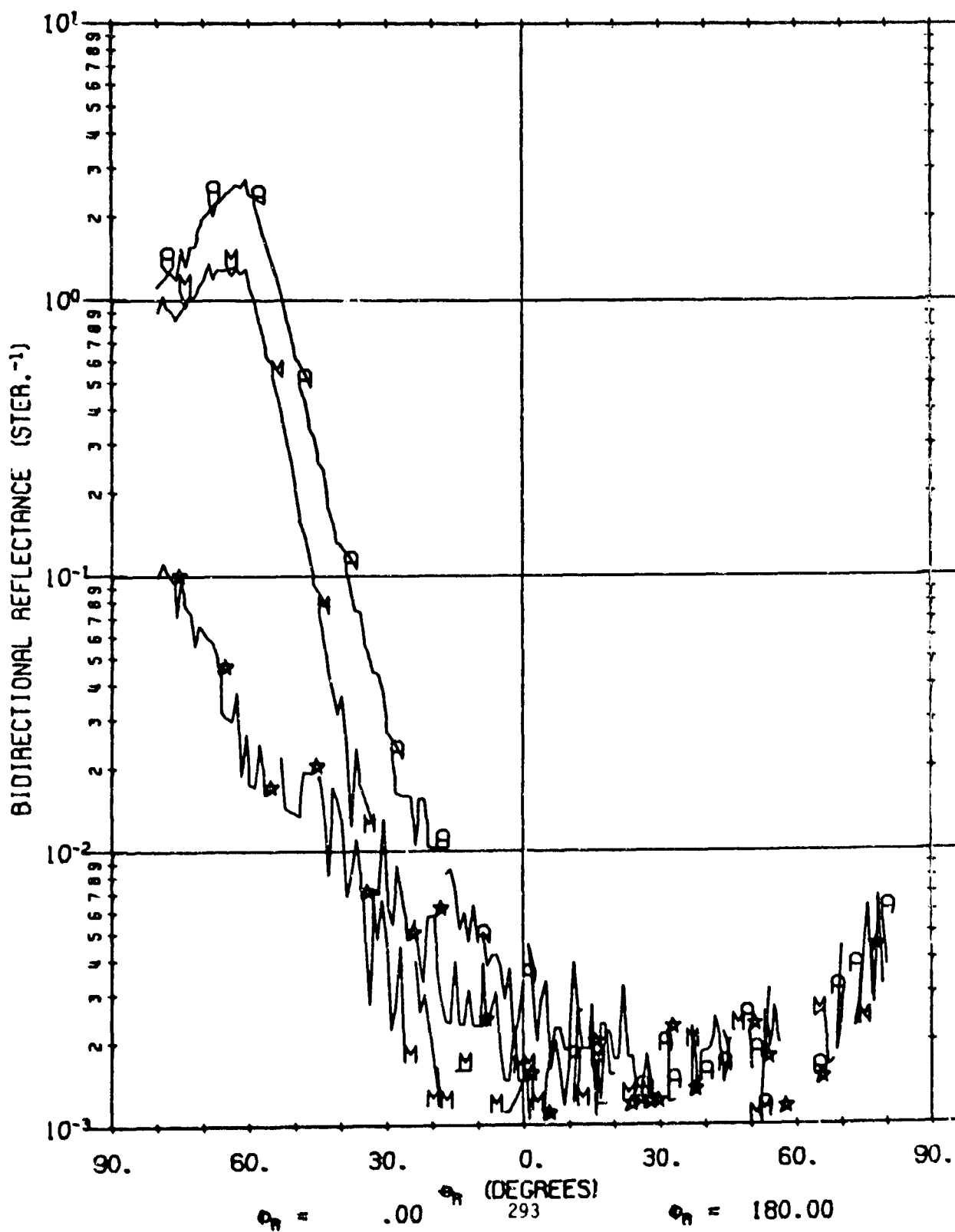
A02023 703

$\lambda = 3.39$   
 $\phi_1 = 60.0$   
 $\phi_2 = 180.0$



A02023 603

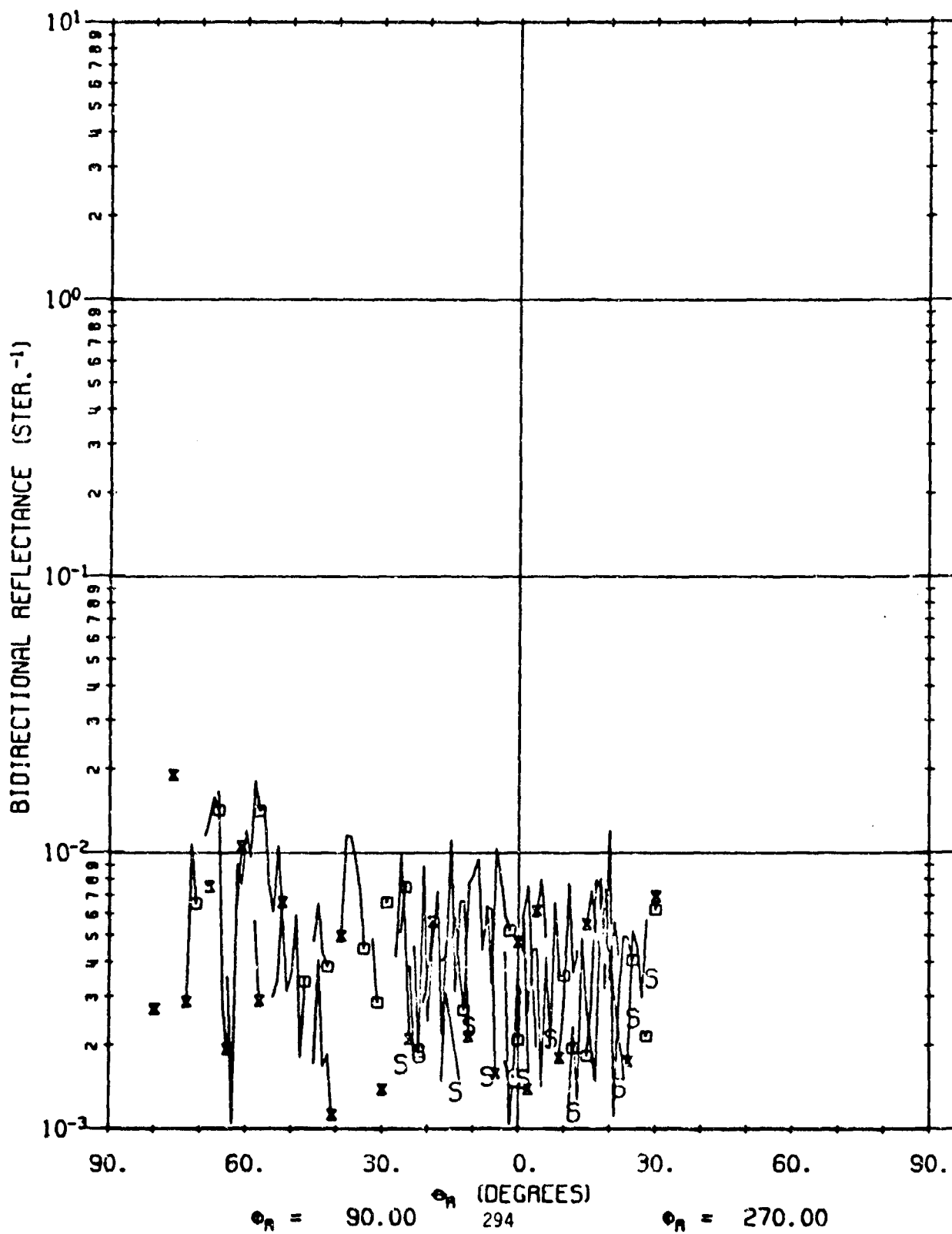
$\lambda = 10.60$   
 $\phi_i = 60.0$   
 $\phi_r = 180.0$





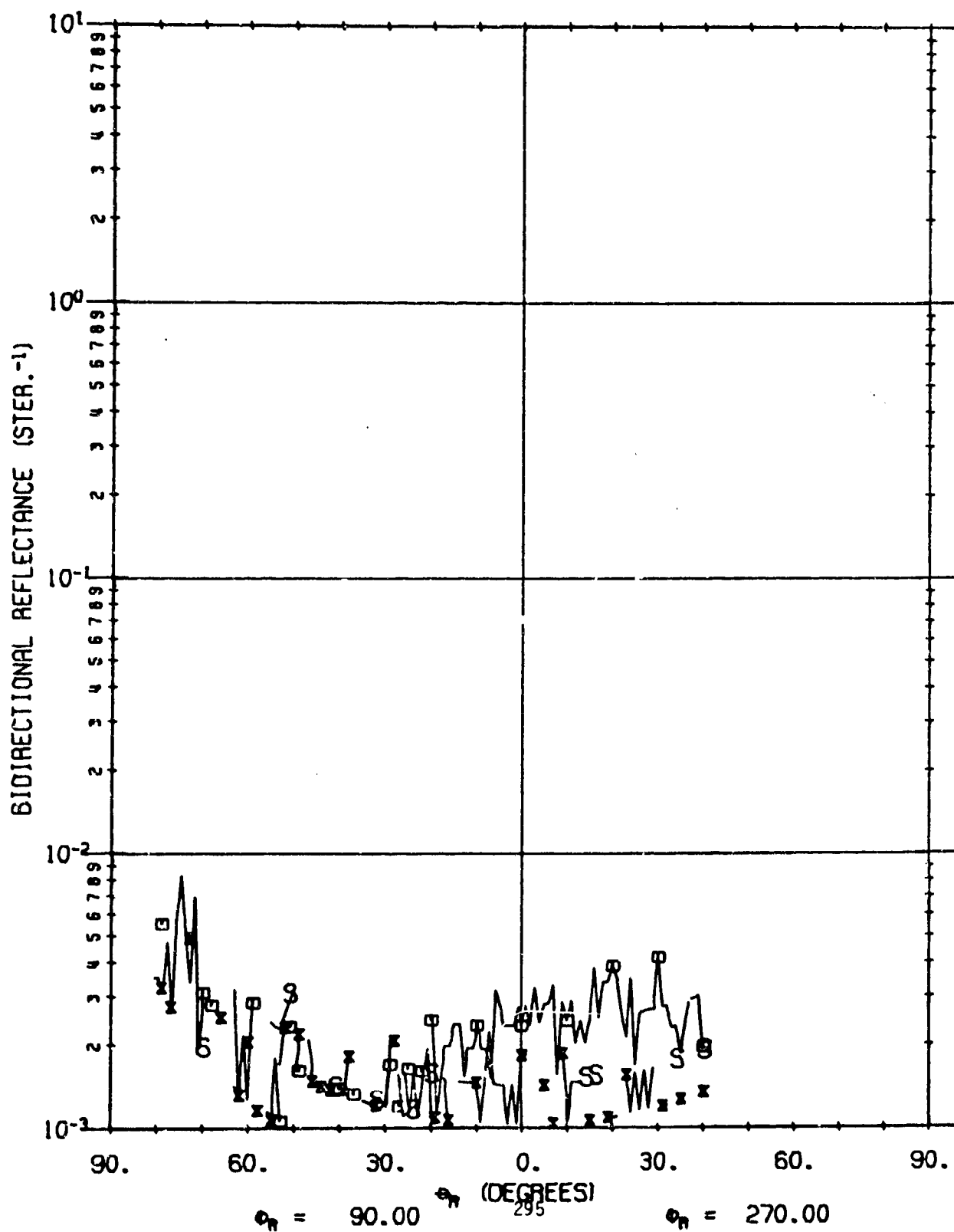
A02023 703

$\lambda = 3.39$   
 $\phi_1 = 60.0$   
 $\phi_2 = 180.0$



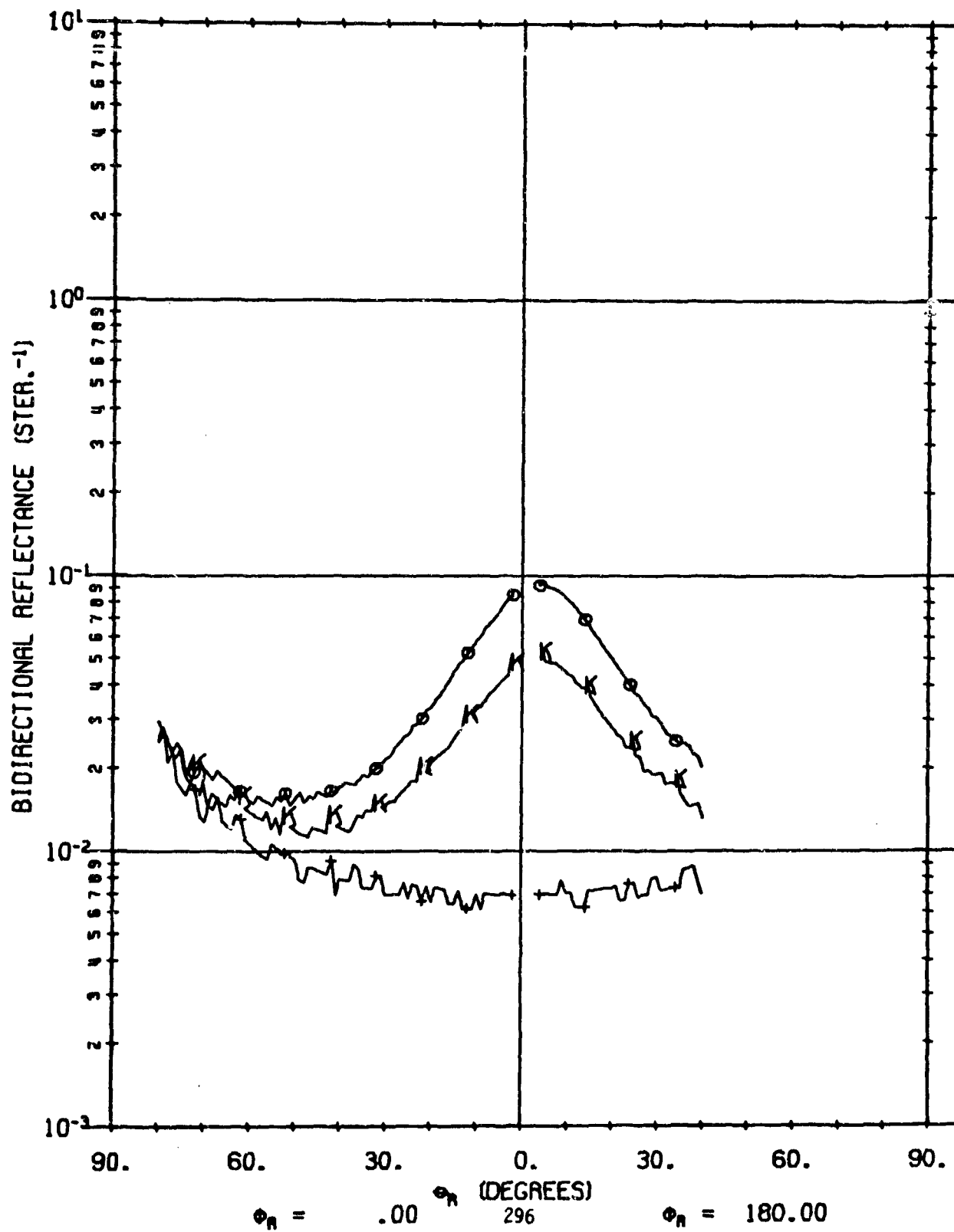
A02023 603

$\lambda = 10.60$   
 $\phi_i = 60.0$   
 $\phi_f = 180.0$



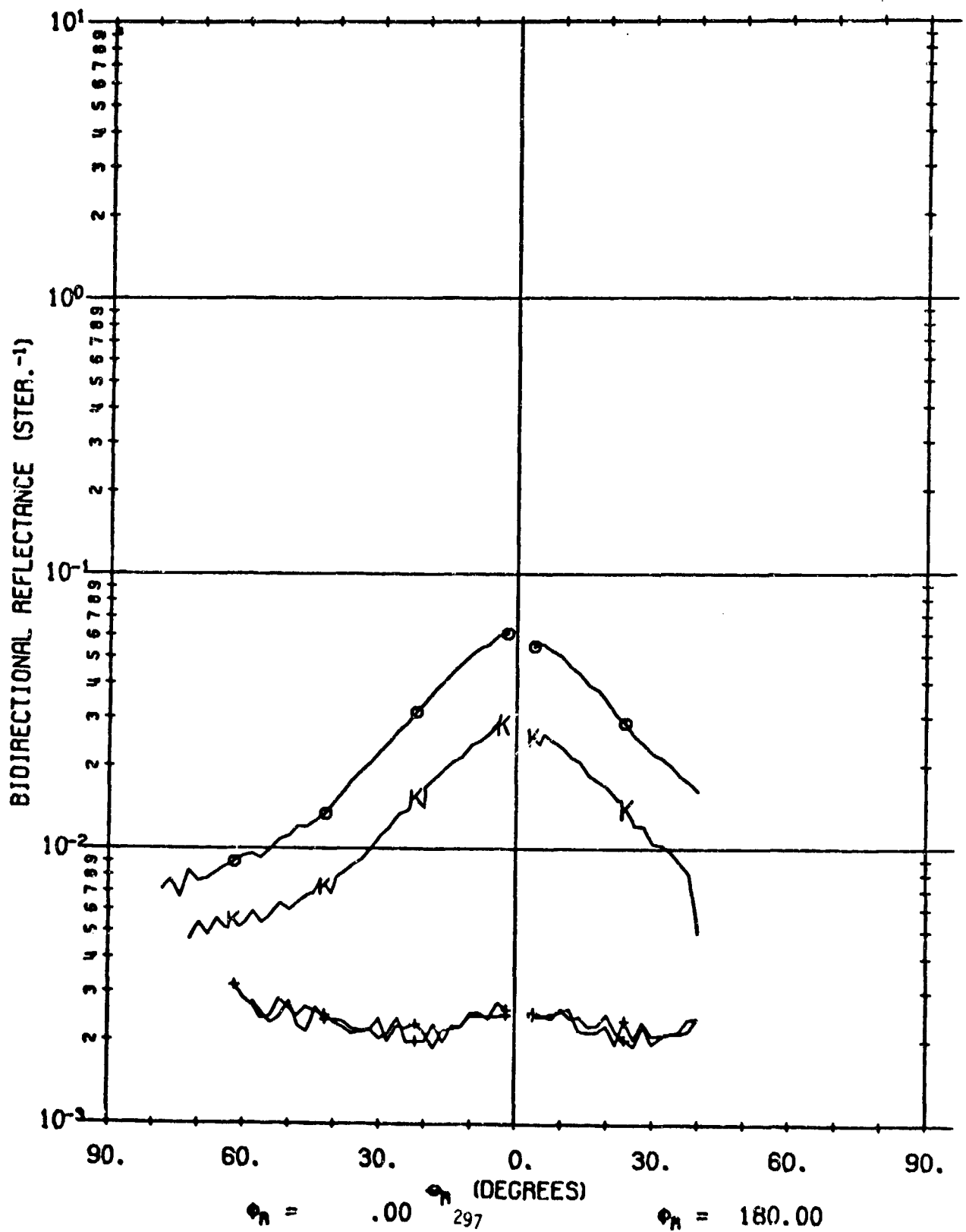
A02023 501

$\lambda = .63$   
 $\phi_i = .0$   
 $\phi_f = 180.0$



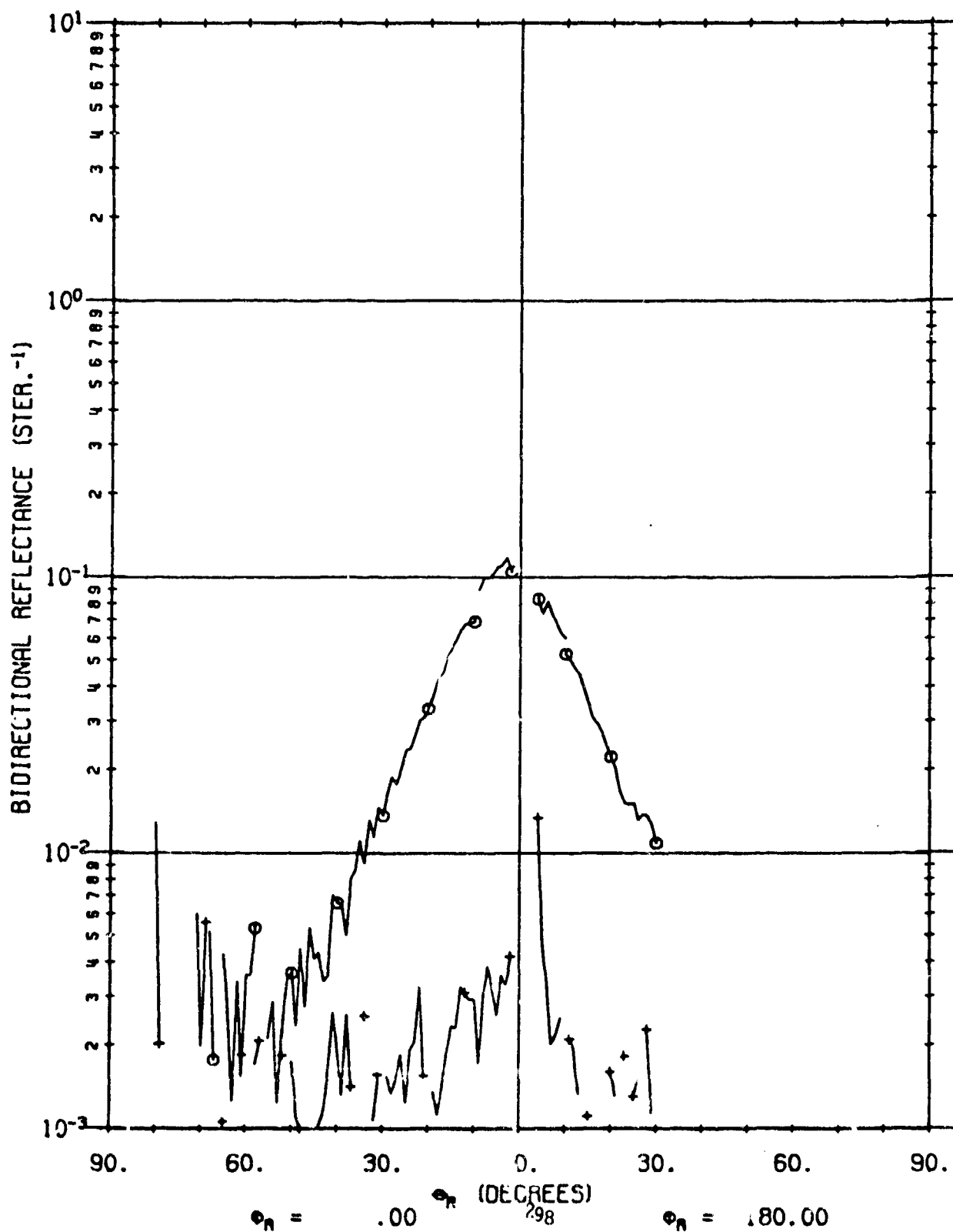
A02023 101

$\lambda = 1.06$   
 $\phi_j = 0$   
 $\phi_j = 180.0$



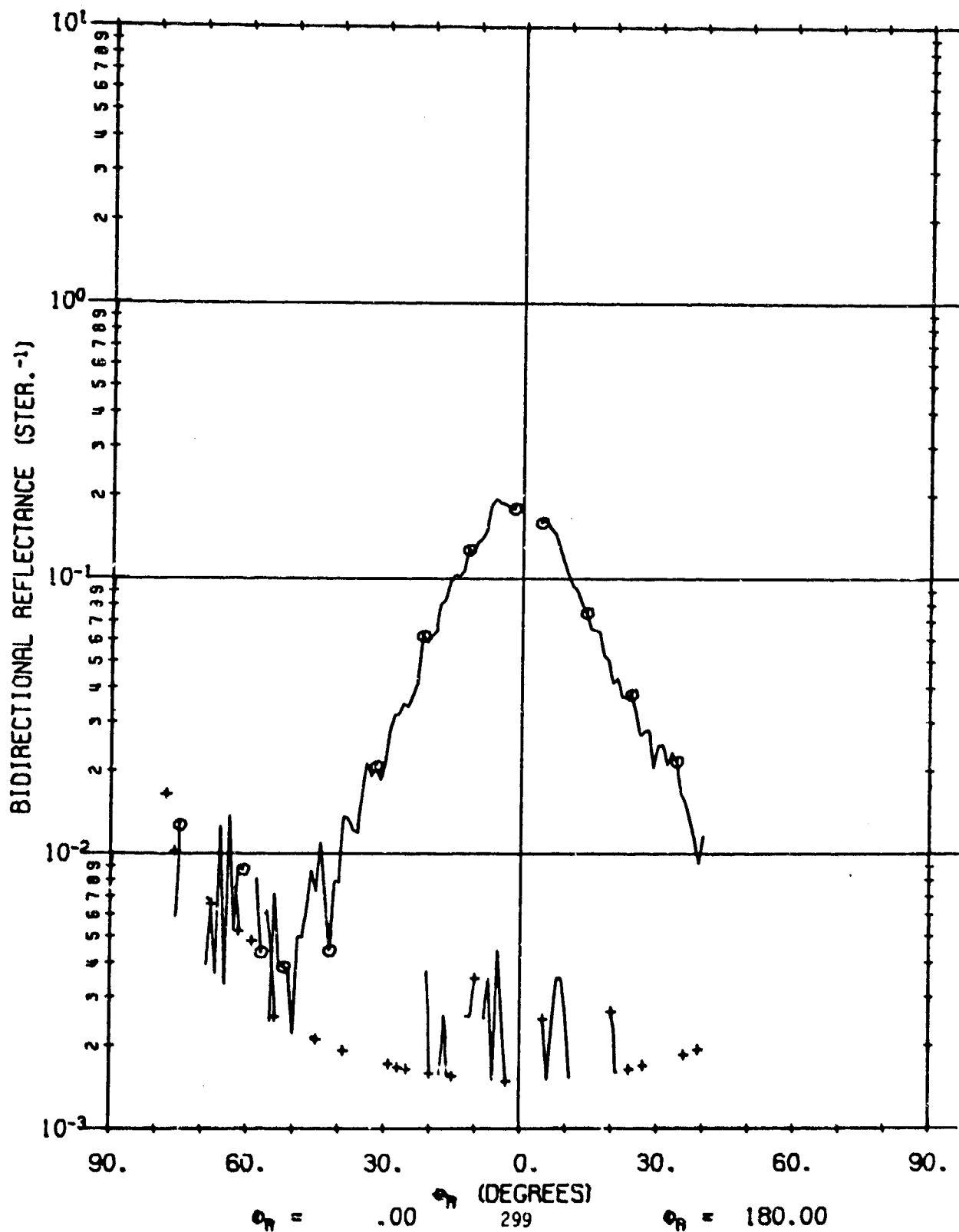
A02023 701

$\lambda = 3.39$   
 $\phi_1 = .0$   
 $\phi_2 = 180.0$



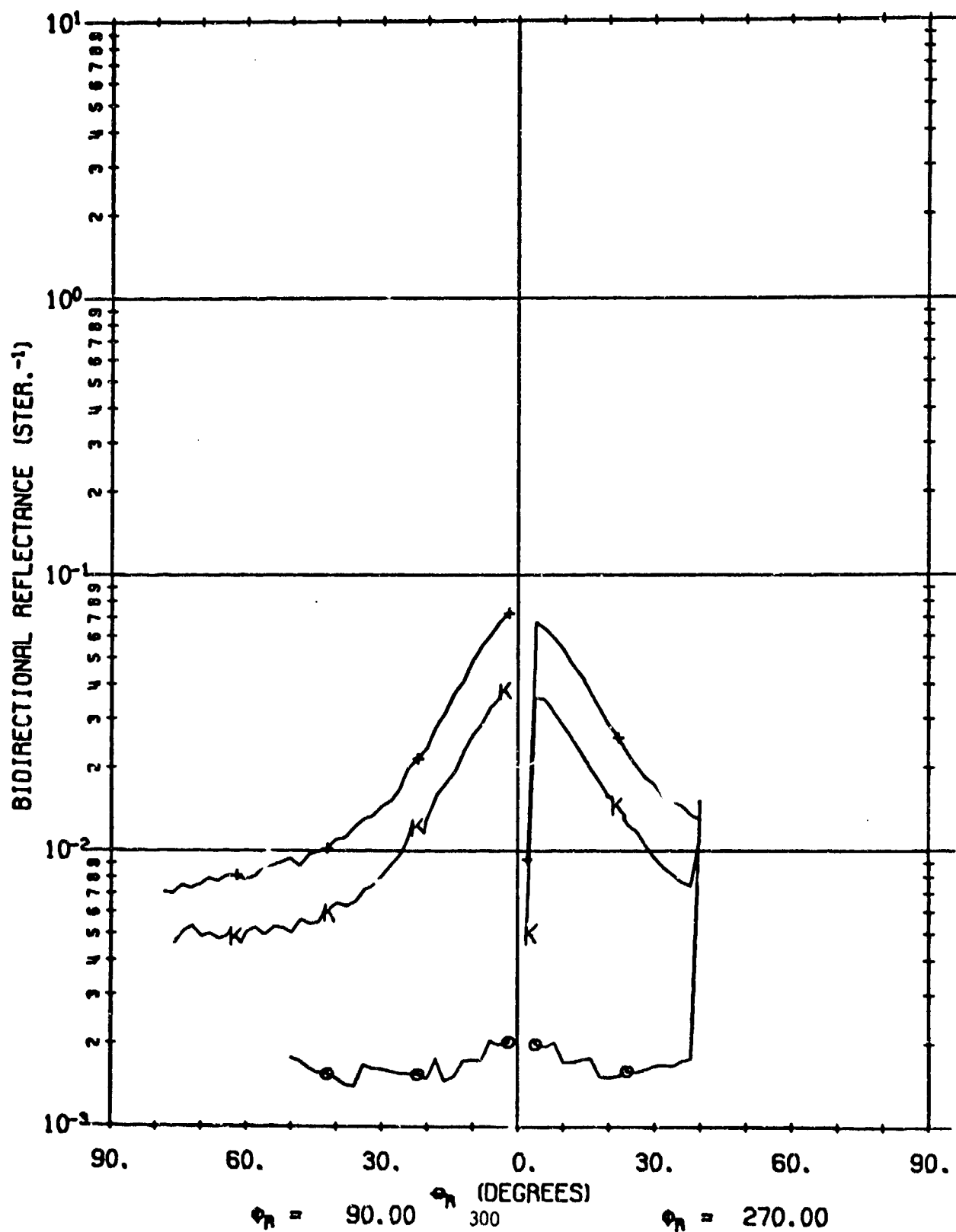
A02023 604

$\lambda = 10.60$   
 $\phi_i = .0$   
 $\phi_f = 180.0$



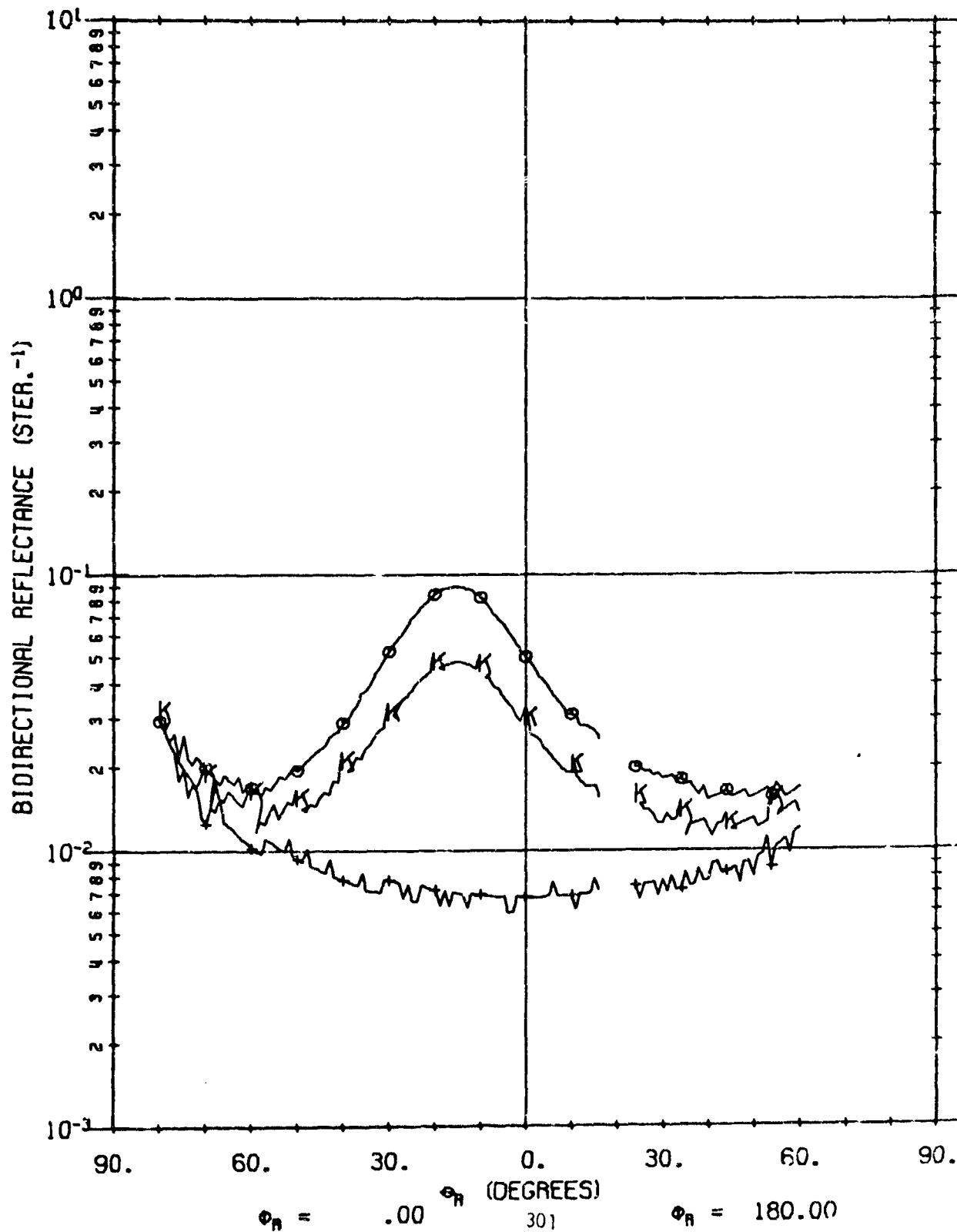
A02023 101

$\lambda = 1.06$   
 $\phi_i = 0$   
 $\phi_f = 180.0$



A02023 501

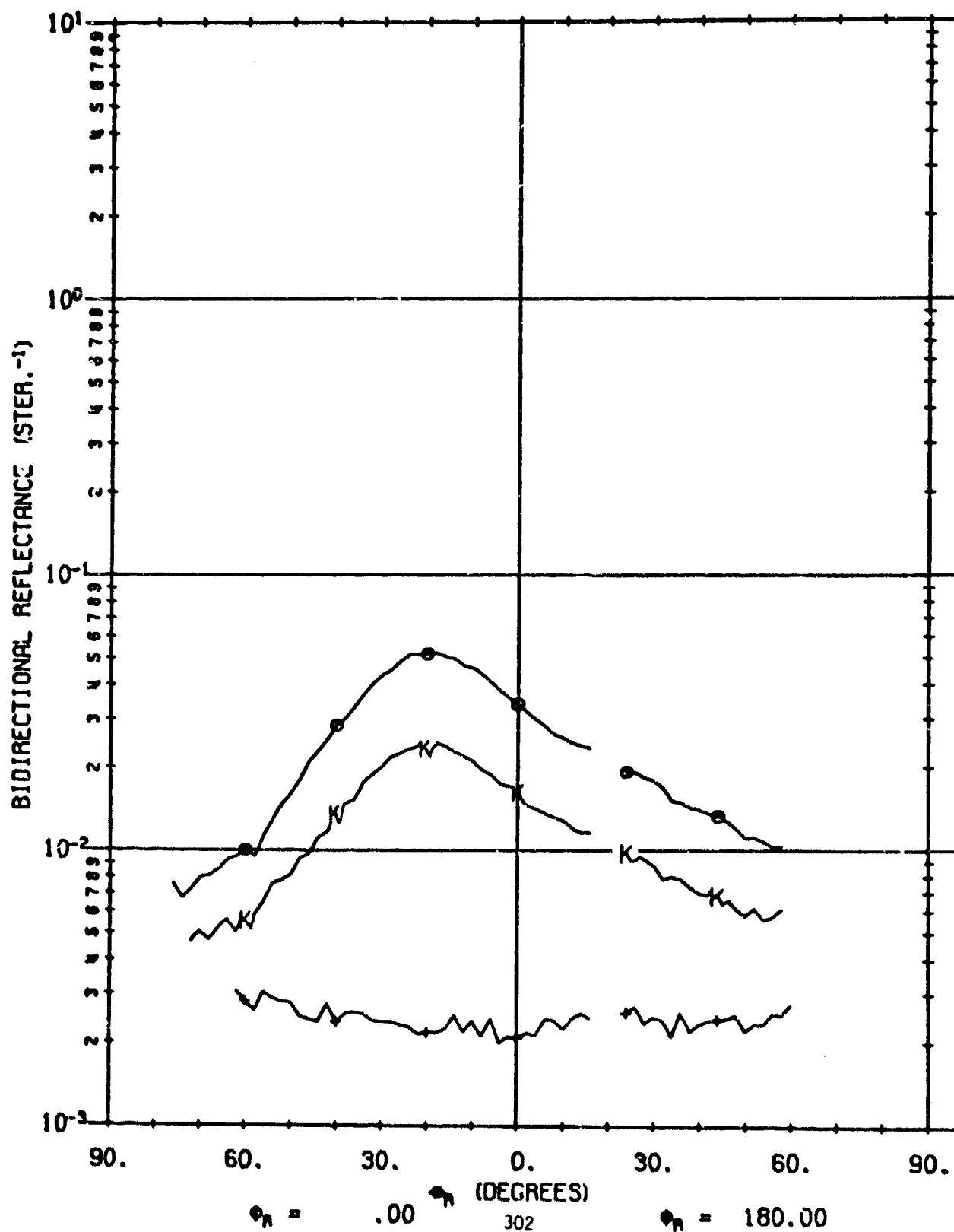
$\lambda = .63$   
 $\phi_i = 20.0$   
 $\phi_r = 180.0$





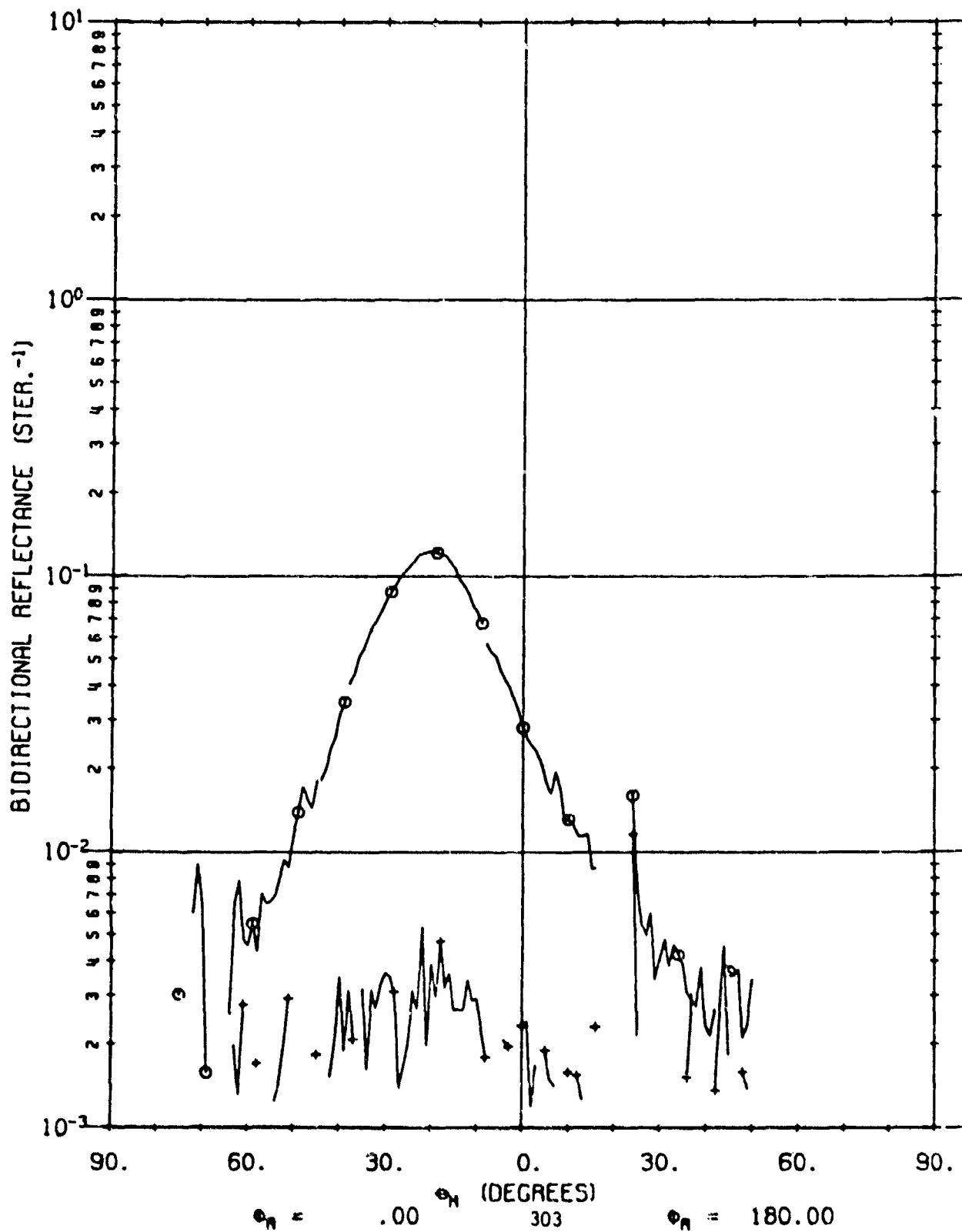
A02023 101

$\lambda = 1.06$   
 $\phi_i = 20.0$   
 $\phi_j = 180.0$



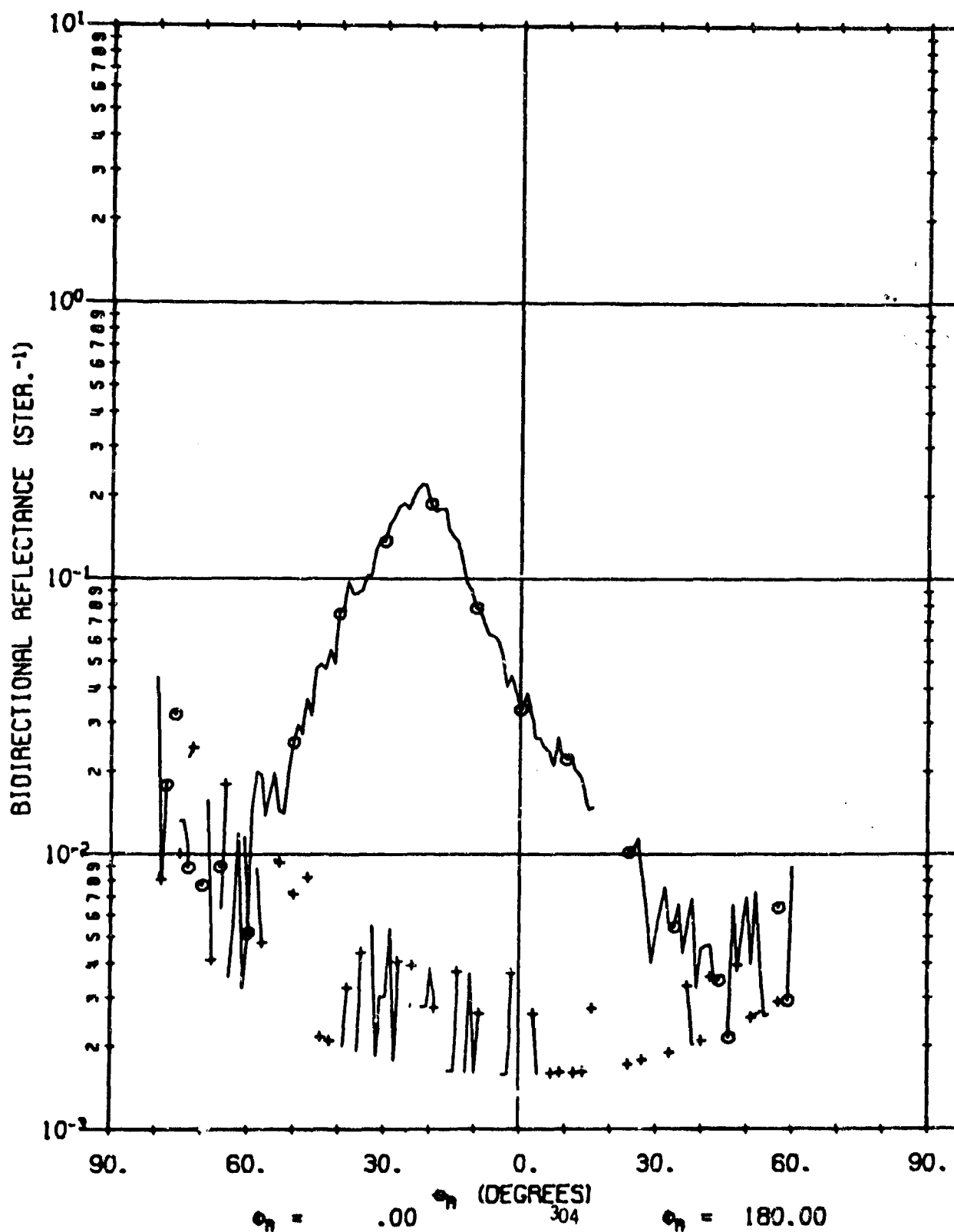
A02023 701

$\lambda = 3.39$   
 $\phi_i = 20.0$   
 $\phi_f = 180.0$



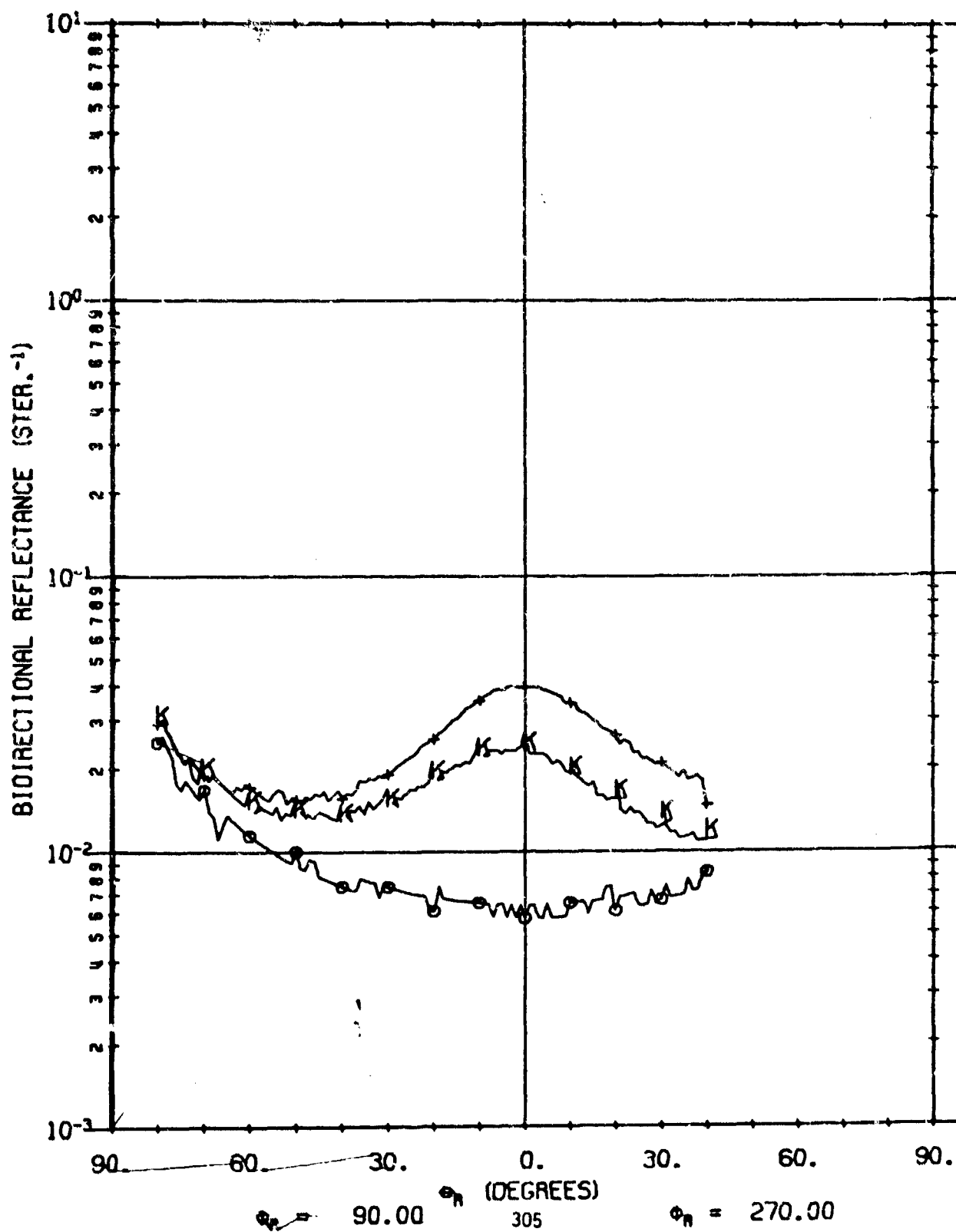
A02023 604

$\lambda = 10.60$   
 $\phi_i = 20.0$   
 $\phi_f = 180.0$



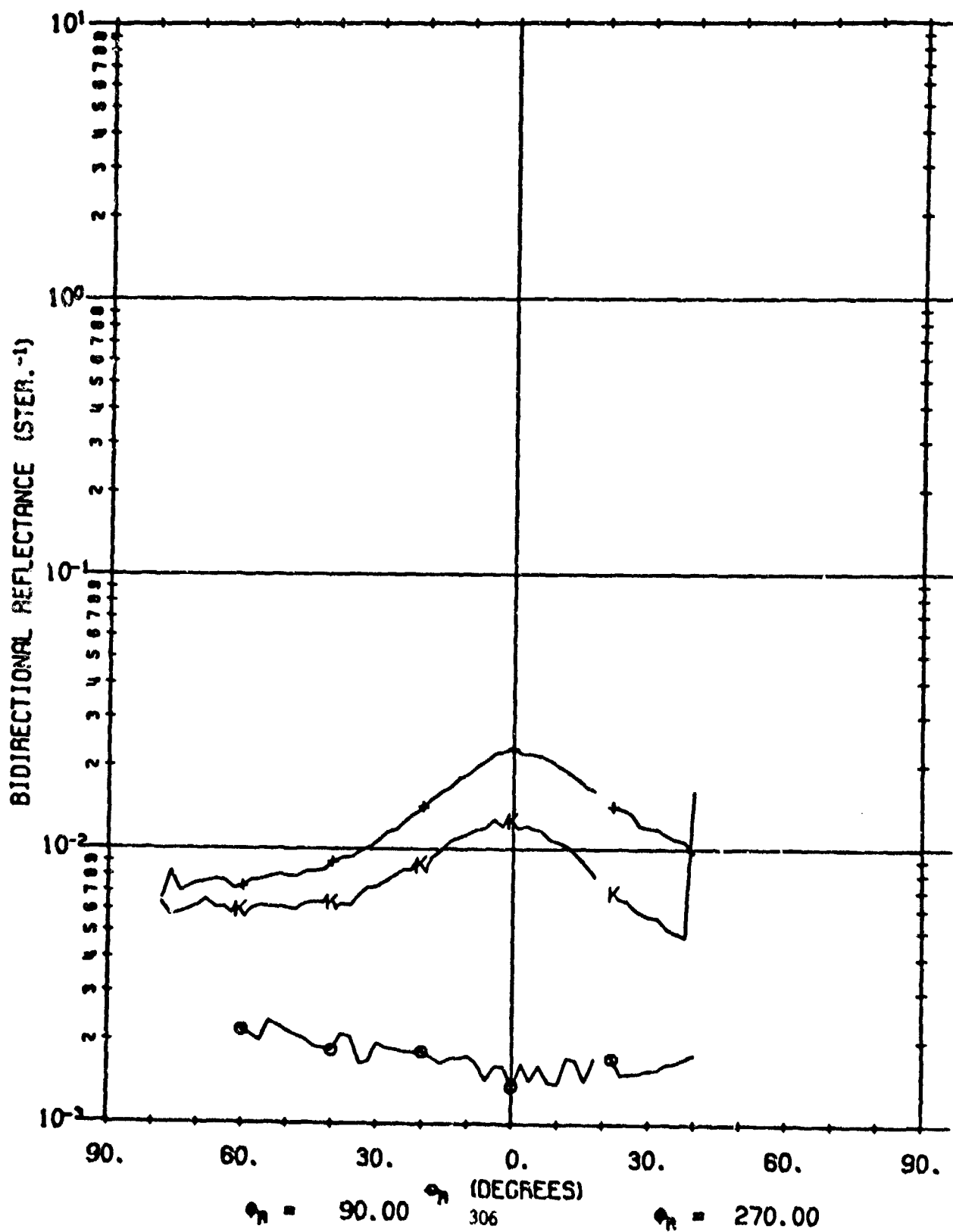
A02023 501

$\lambda = .63$   
 $\phi_i = 20.0$   
 $\phi_r = 180.0$



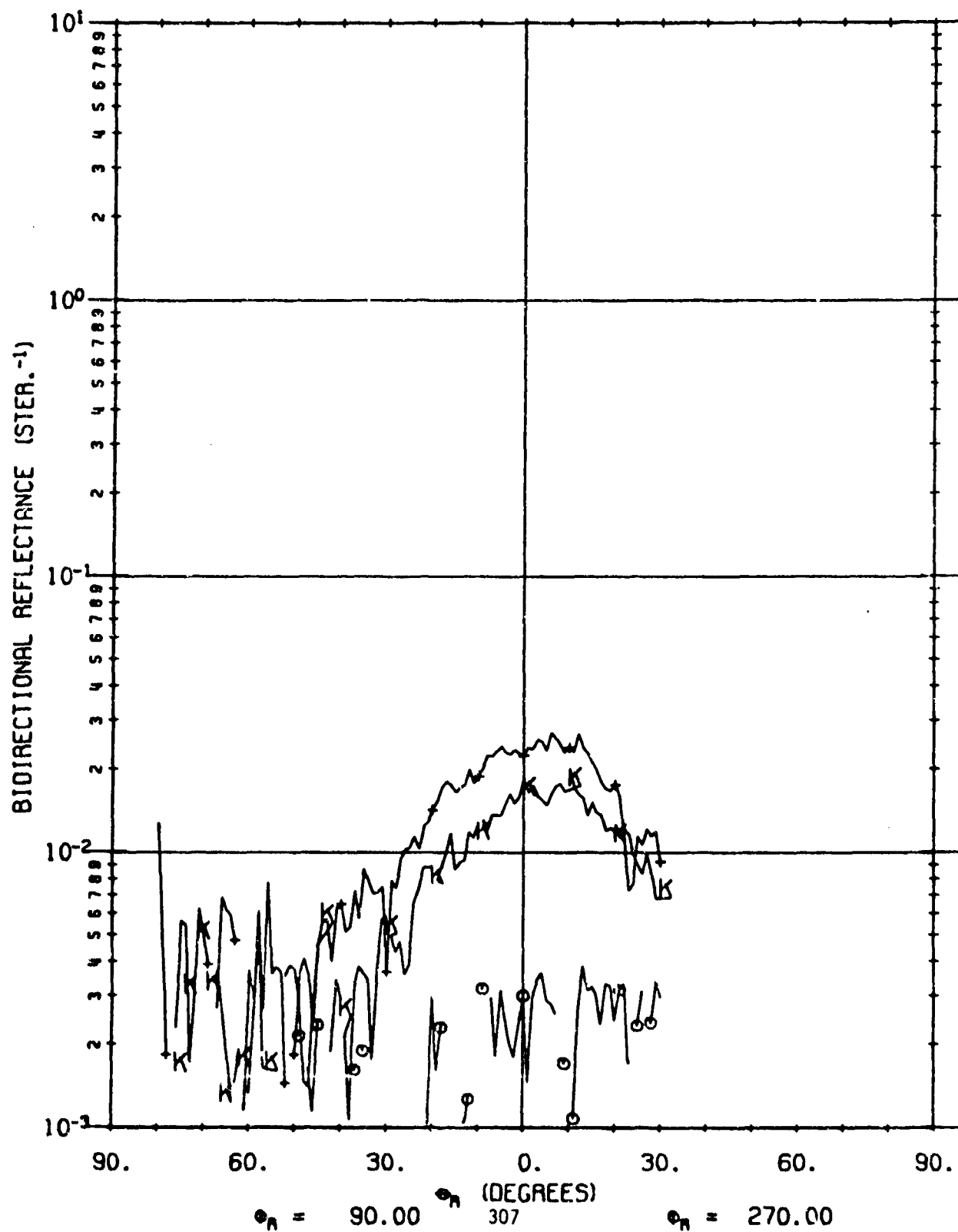
A02023 101

$\lambda = 1.06$   
 $\phi_i = 20.0$   
 $\phi_i = 180.0$



A02023 702

$\lambda = 3.39$   
 $\phi_i = 20.0$   
 $\phi_j = 180.0$



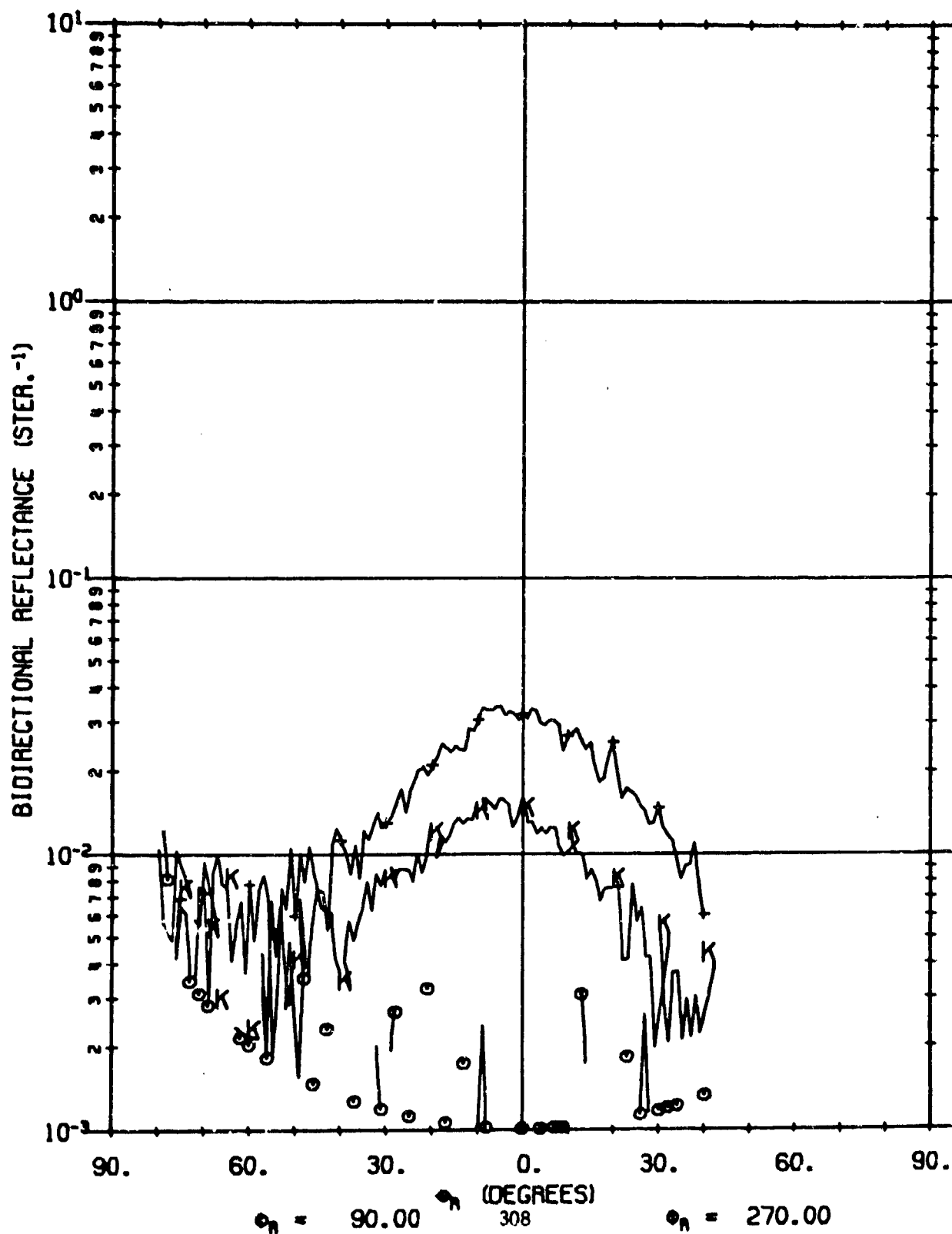
A02023

602

$\lambda = 10.60$

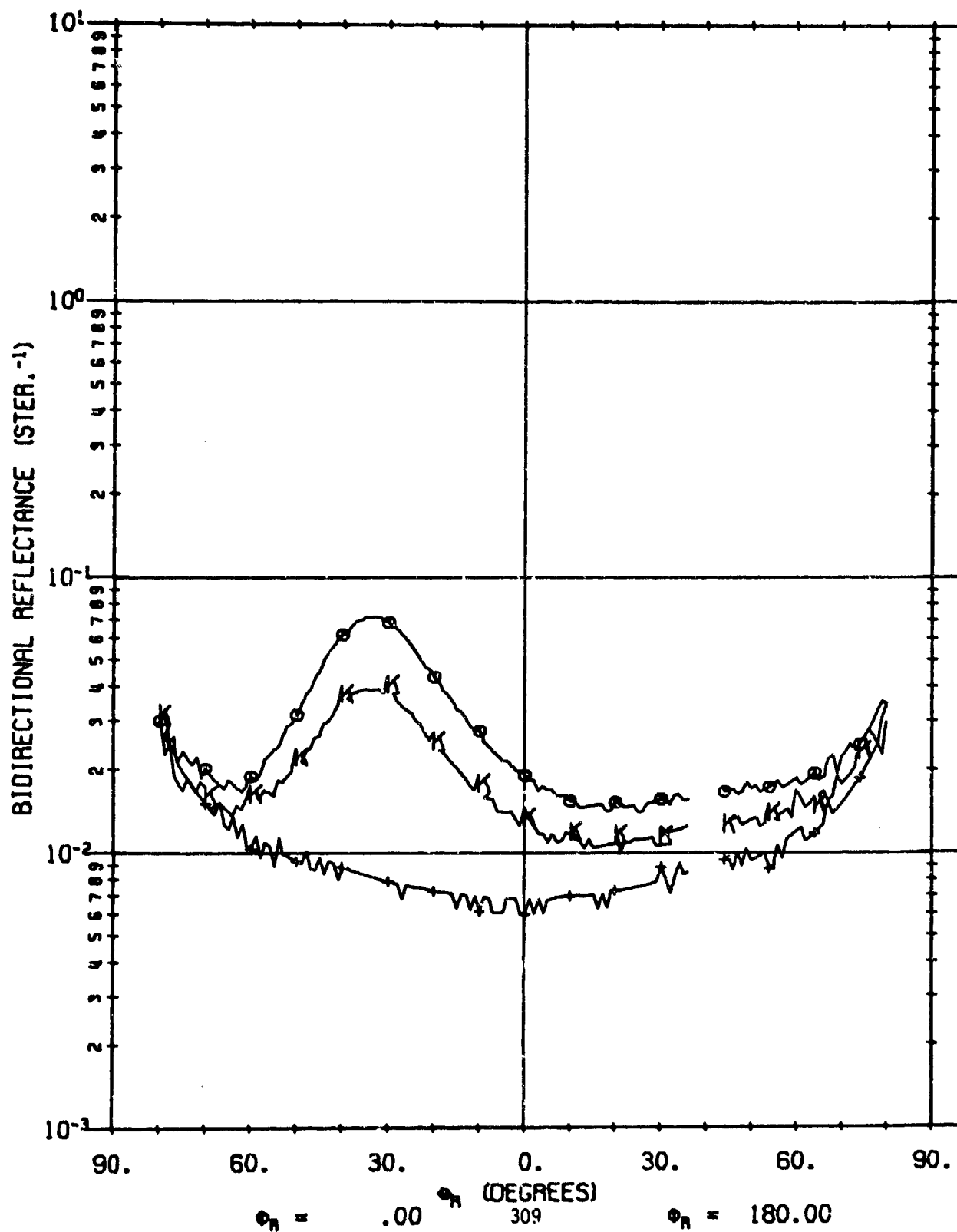
$\phi_i = 20.0$

$\phi_f = 180.0$



A02023 501

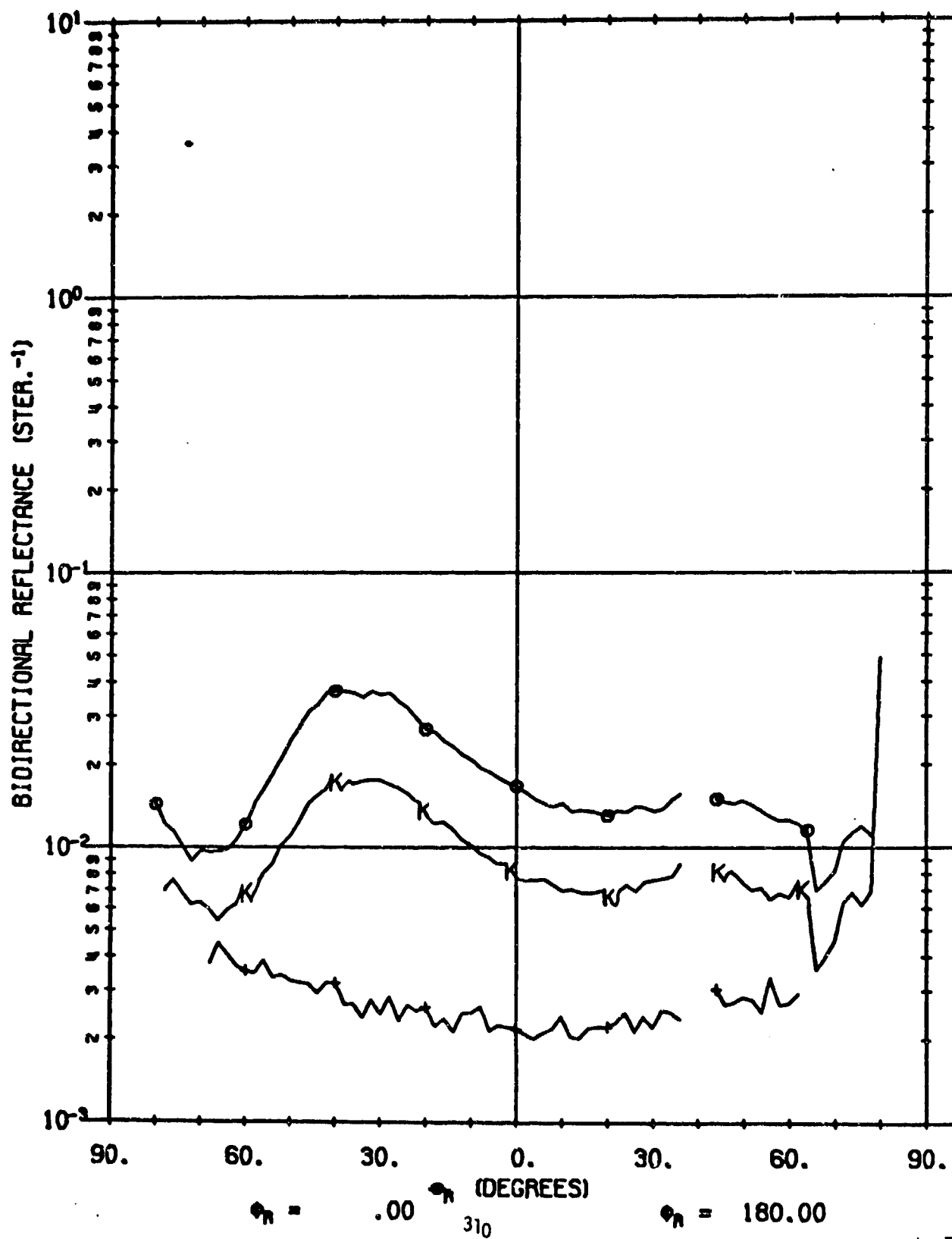
$\lambda = .63$   
 $\phi_i = 40.0$   
 $\phi_i = 180.0$





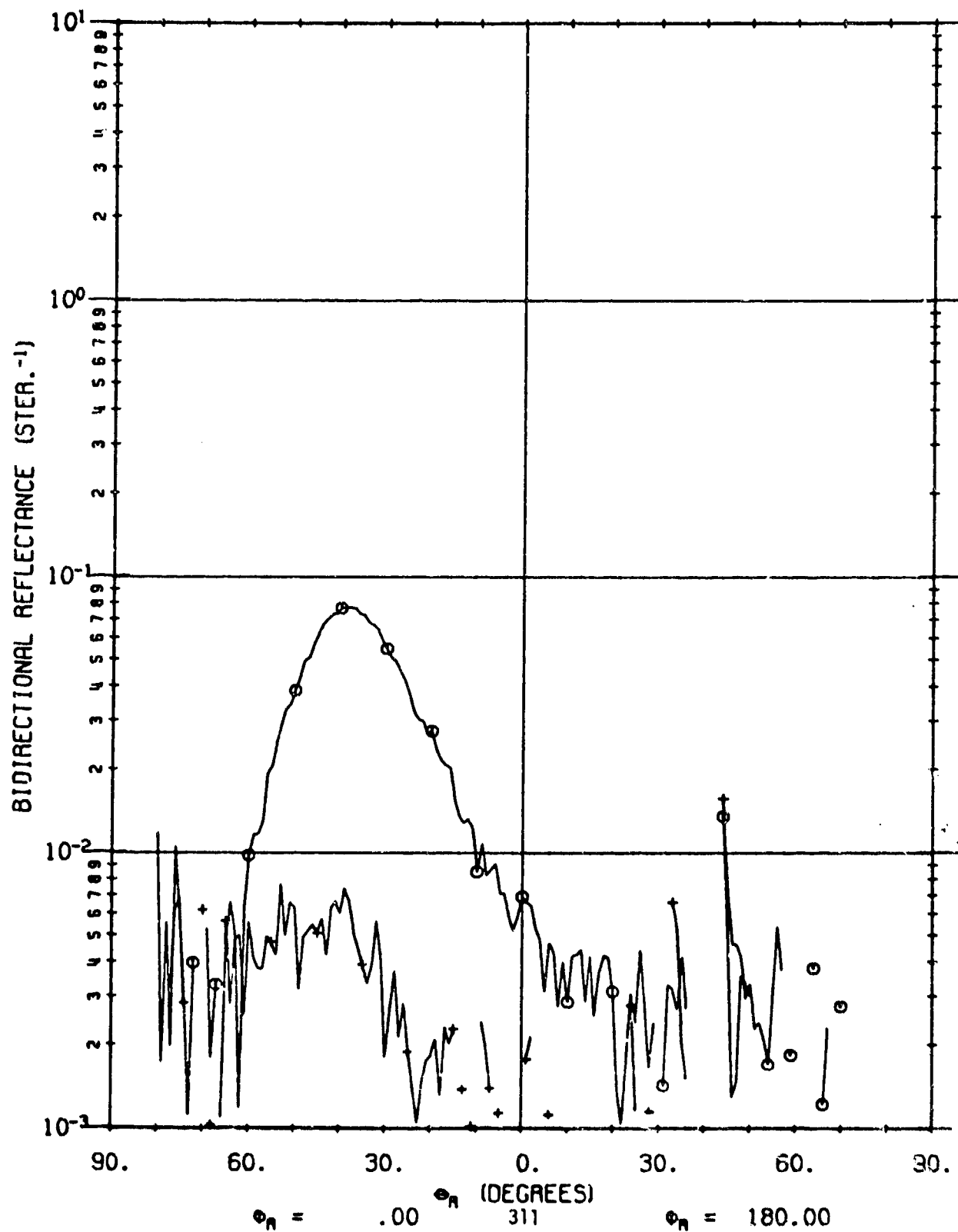
A02023 101

$\lambda = 1.06$   
 $\phi_i = 40.0$   
 $\phi_f = 180.0$



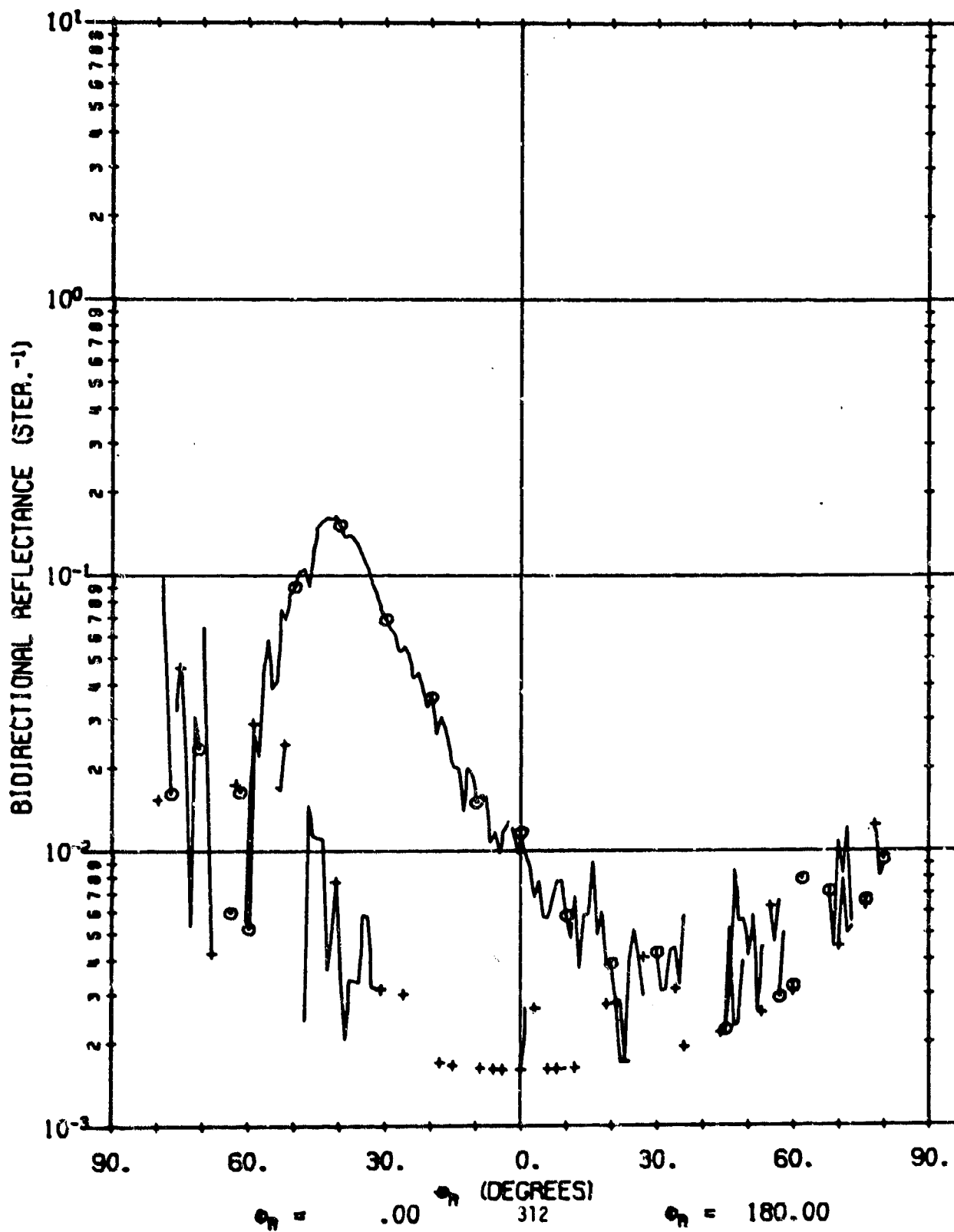
A02023 701

$\lambda = 3.39$   
 $\phi_i = 40.0$   
 $\phi_j = 180.0$



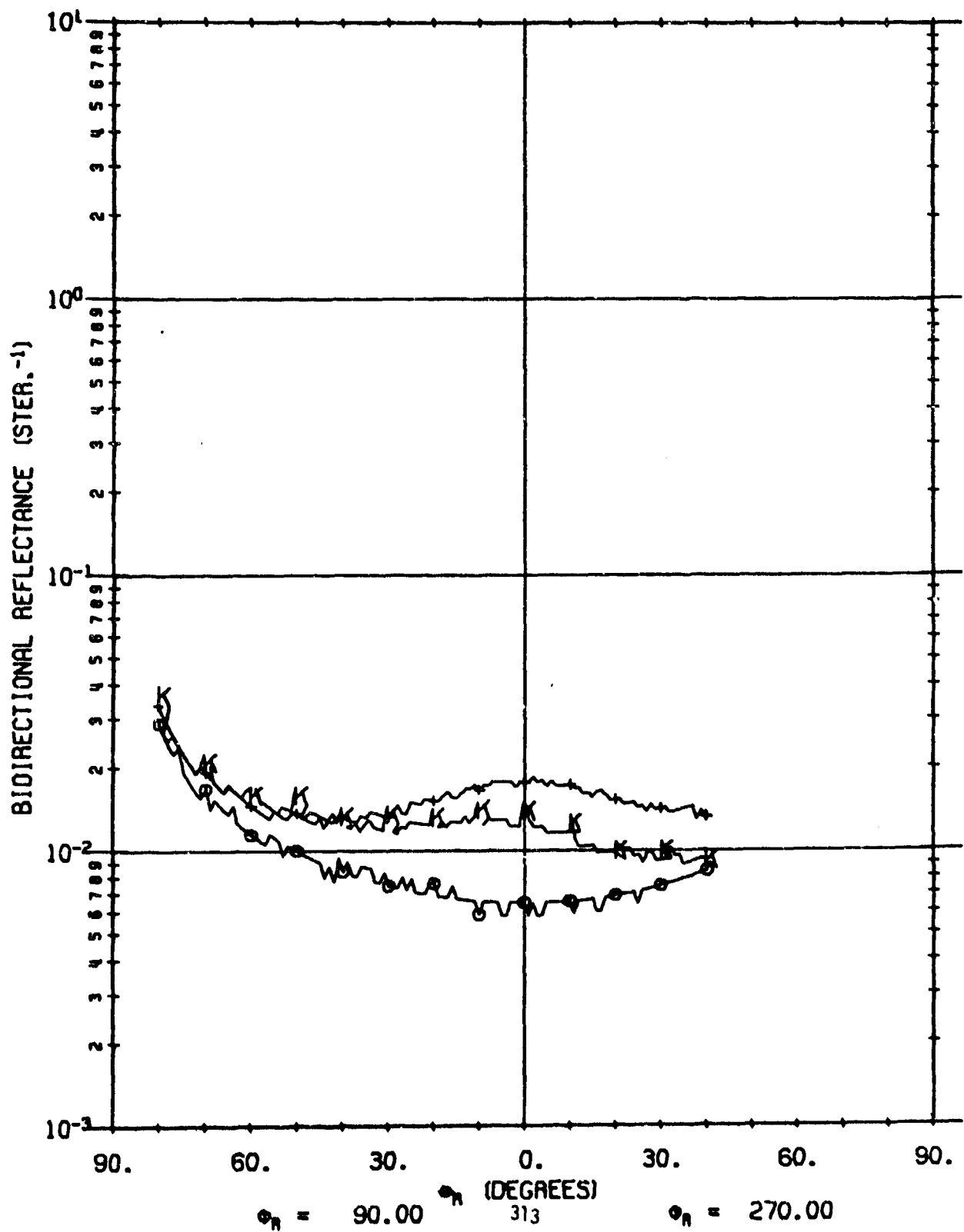
A02023

604

 $\lambda = 10.60$   
 $\theta_i = 40.0$   
 $\theta_r = 180.0$ 

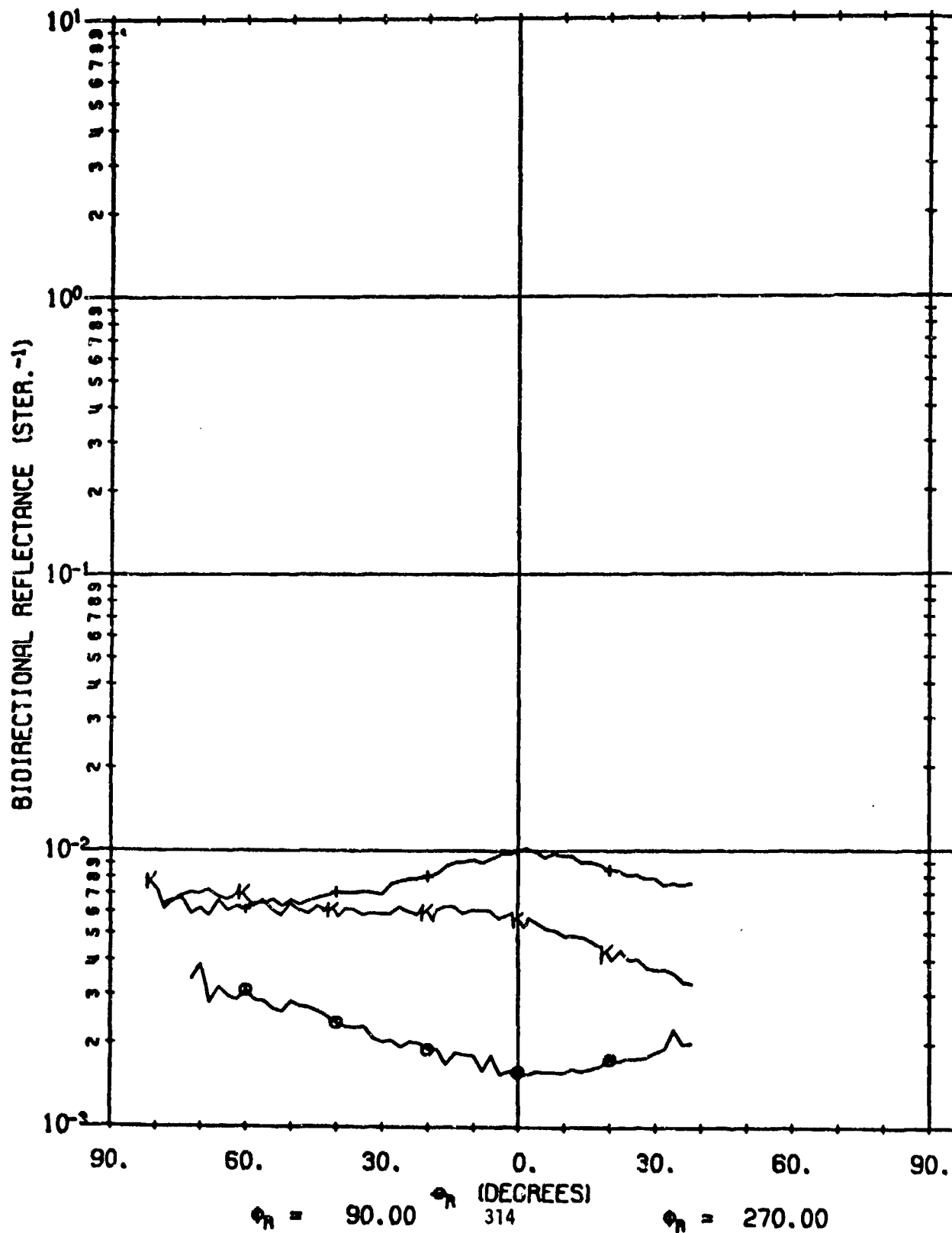
A02023 501

$\lambda = .63$   
 $\phi_i = 40.0$   
 $\phi_i = 180.0$



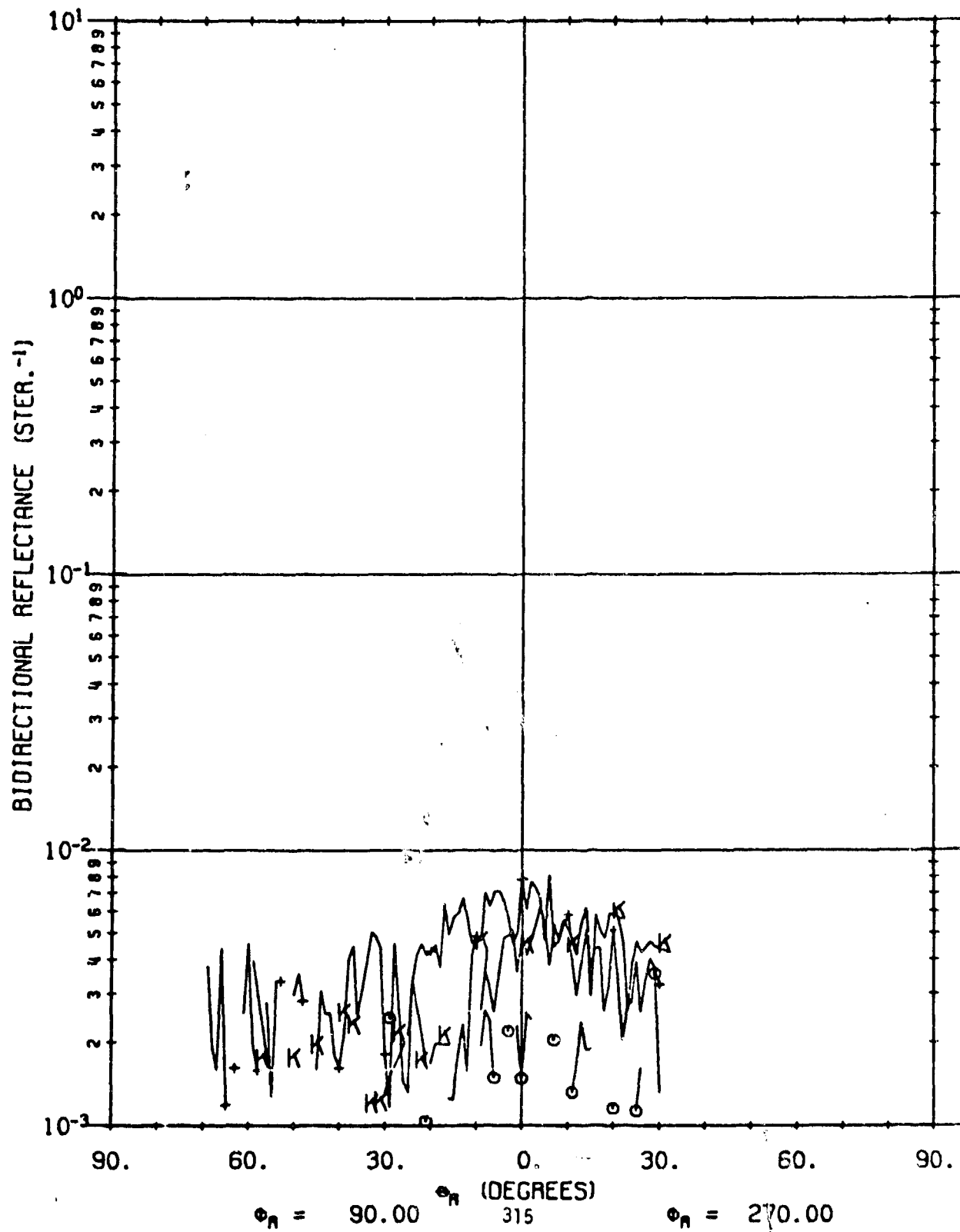
A02023 101

$\lambda = 1.06$   
 $\phi_j = 40.0$   
 $\phi_i = 180.0$



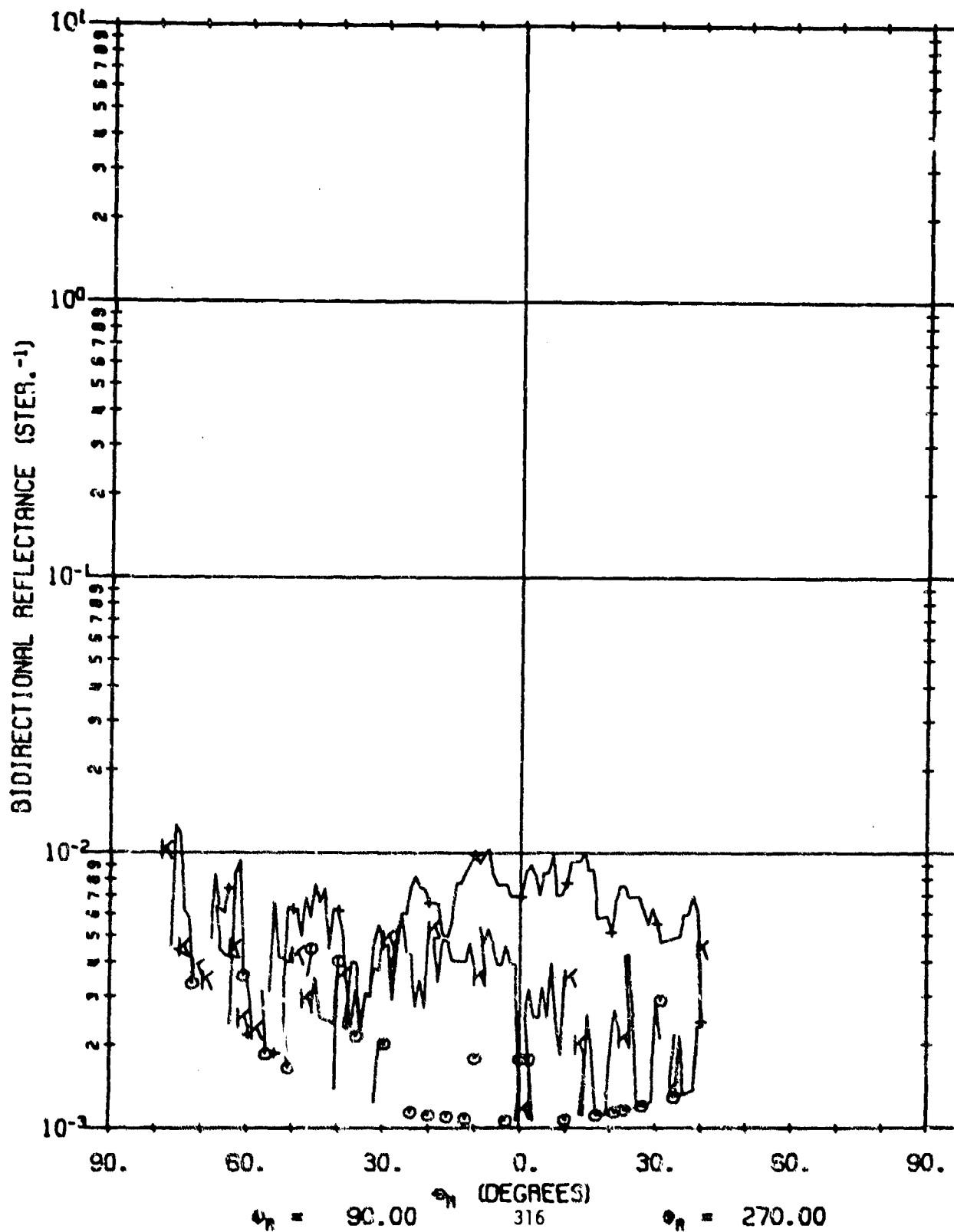
A02023 702

$\lambda = 3.39$   
 $\phi_j = 40.0$   
 $\phi_i = 180.0$



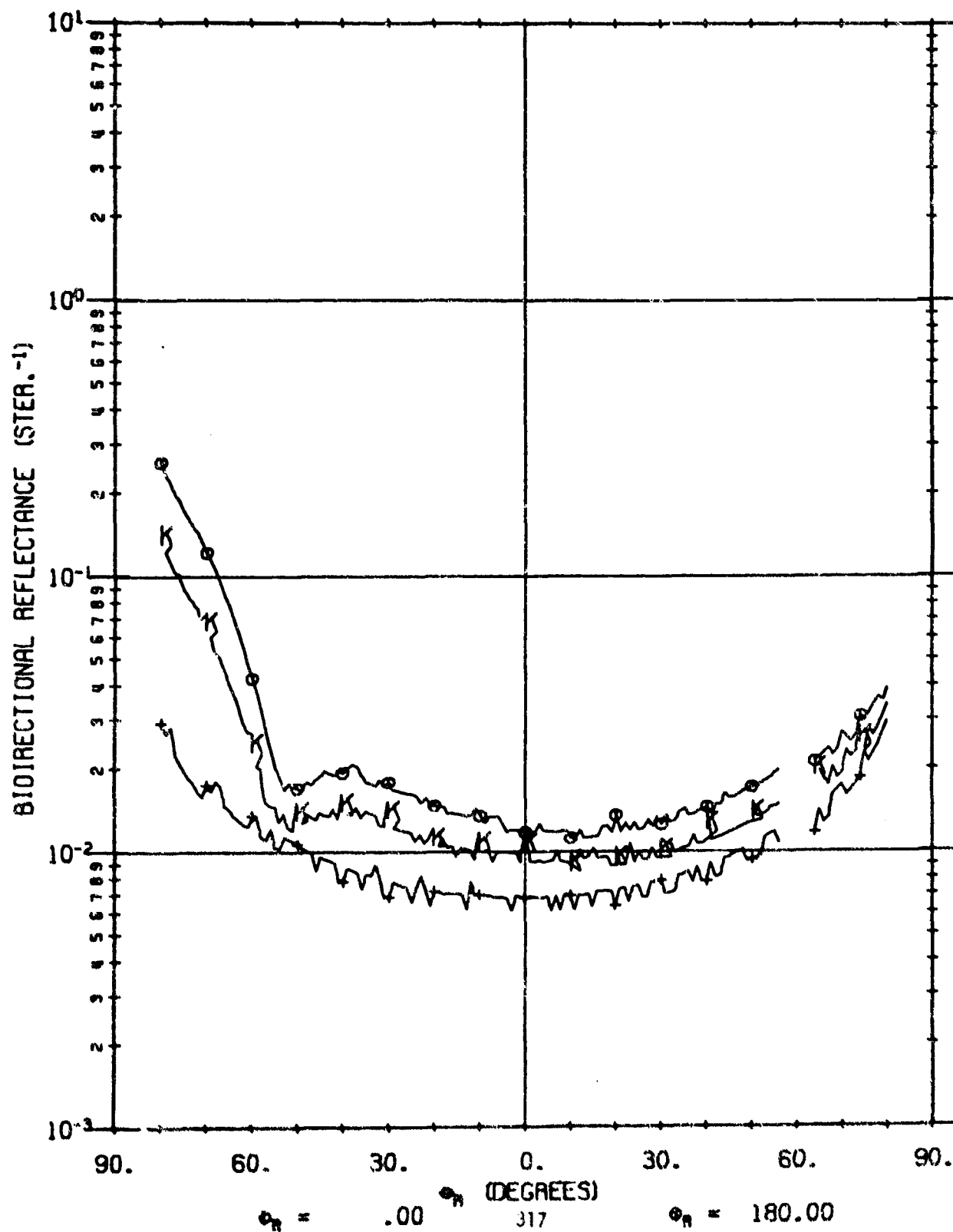
A02023 602

$\lambda = 10.60$   
 $\phi_i = 40.0$   
 $\phi_t = 180.0$



A02023 501

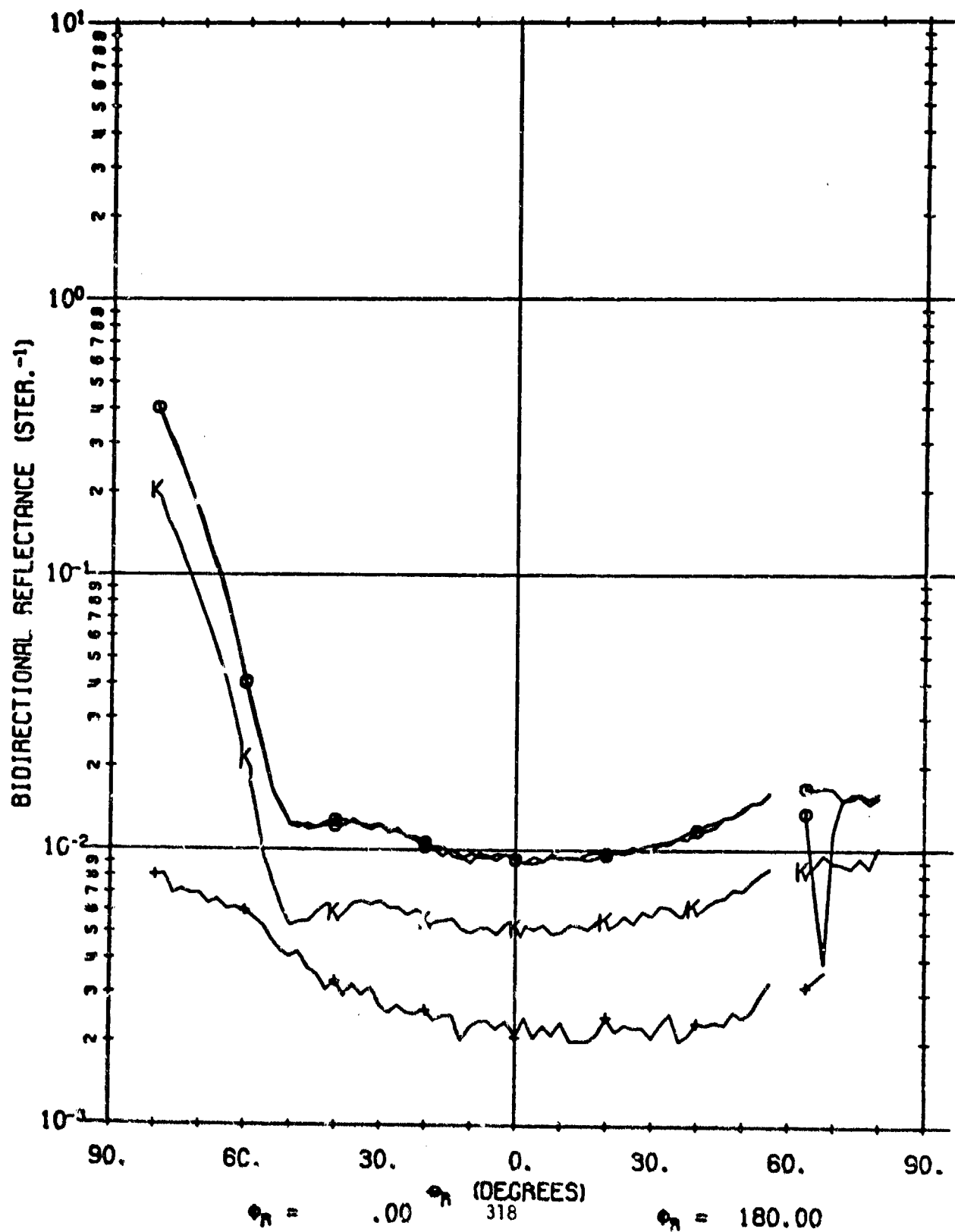
$\lambda = .63$   
 $\phi_i = 60.0$   
 $\phi_f = 180.0$





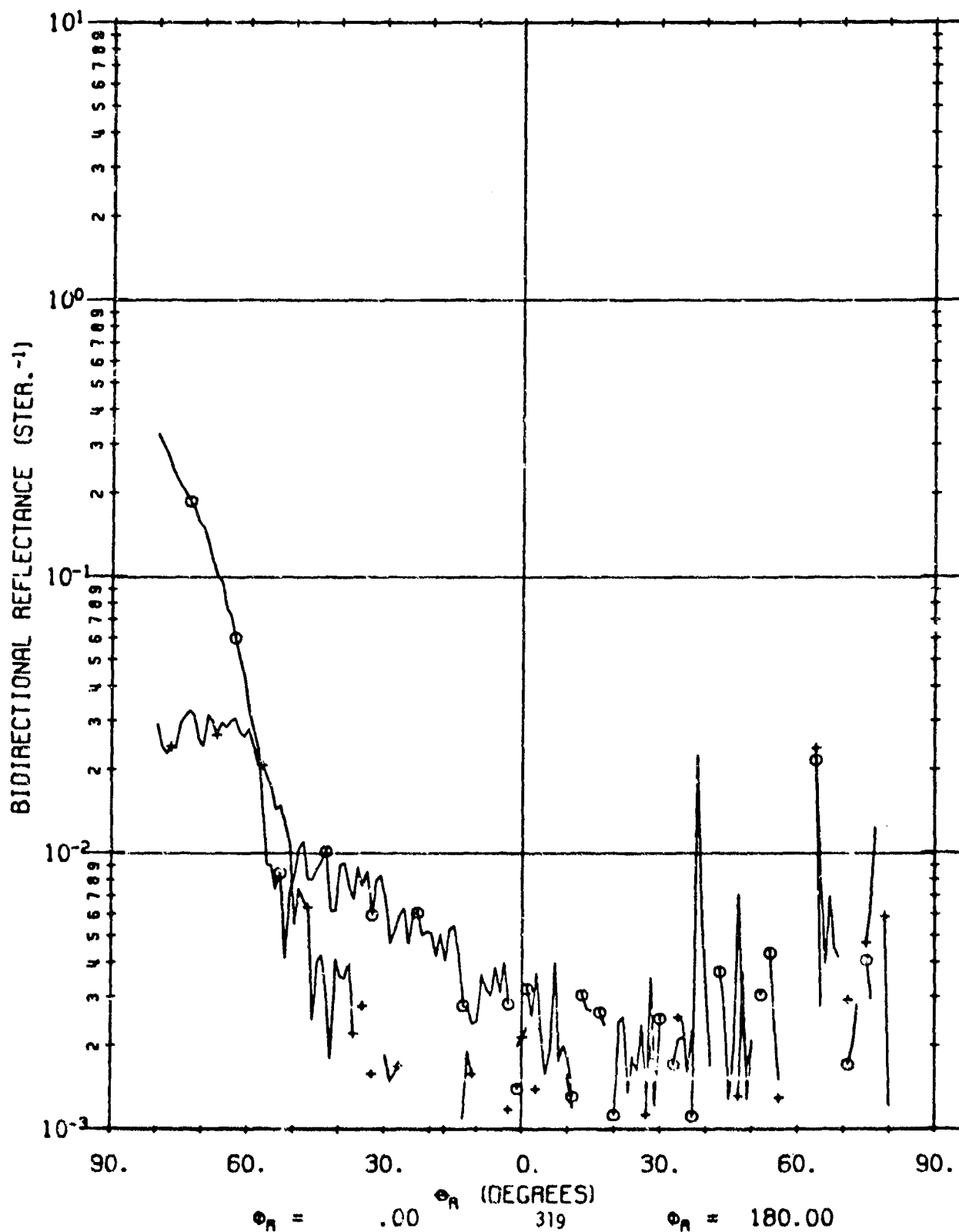
A02023 101

$\lambda = 1.06$   
 $\phi_1 = 60.0$   
 $\phi_2 = 180.0$



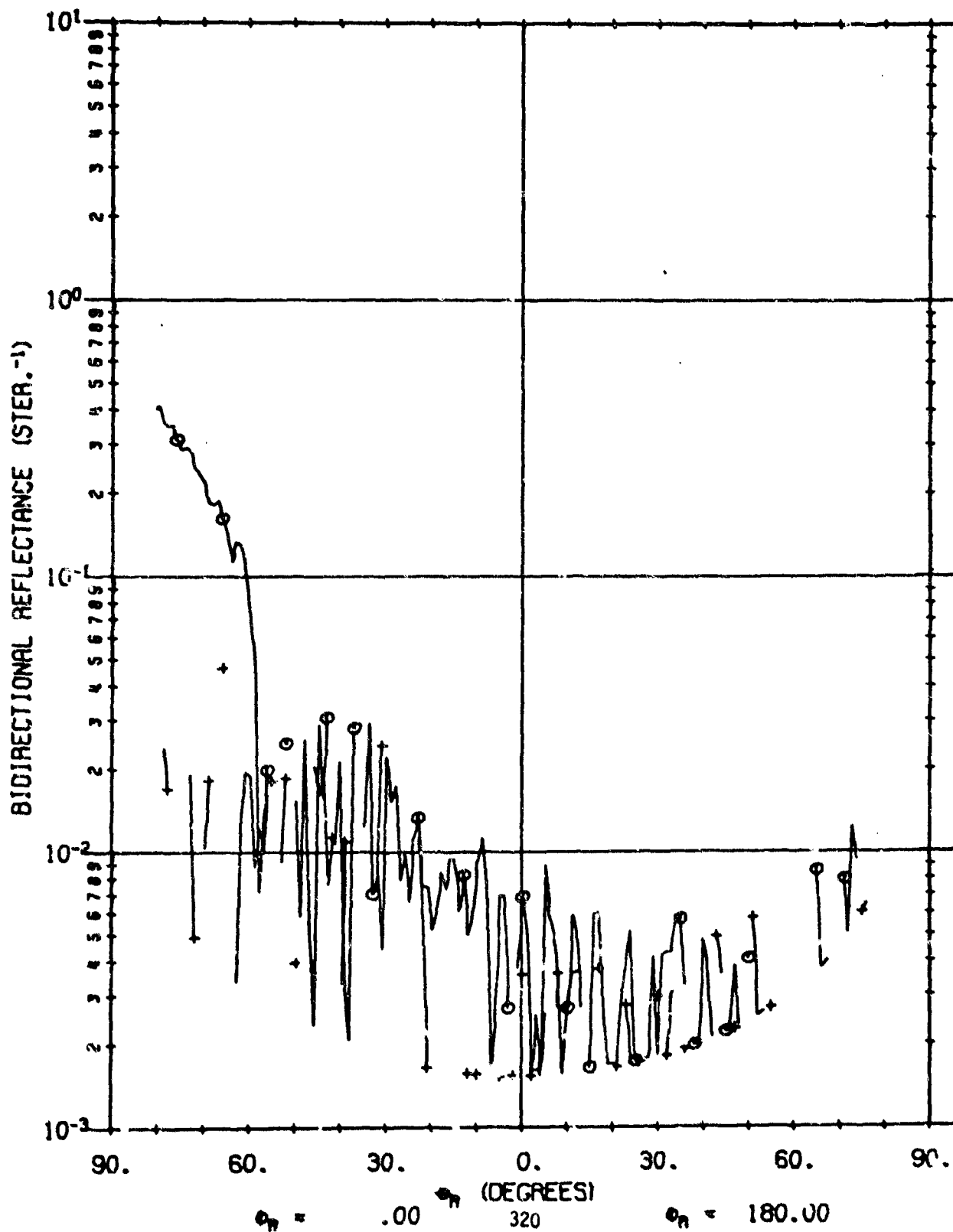
A02023 701

$\lambda = 3.39$   
 $\phi_i = 60.0$   
 $\phi_j = 180.0$



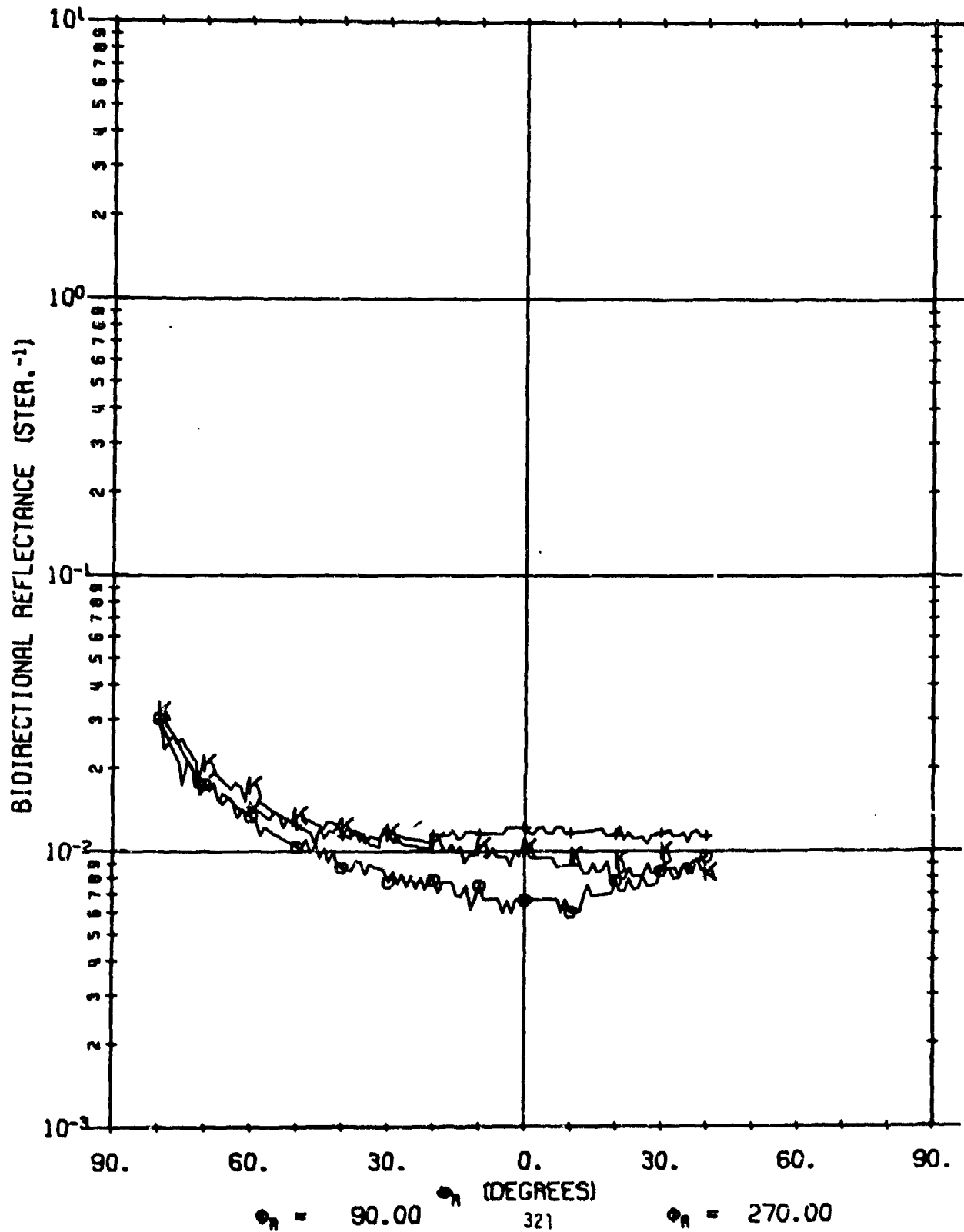
A02023 604

$\lambda = 10.60$   
 $\phi_i = 60.0$   
 $\phi_f = 180.0$



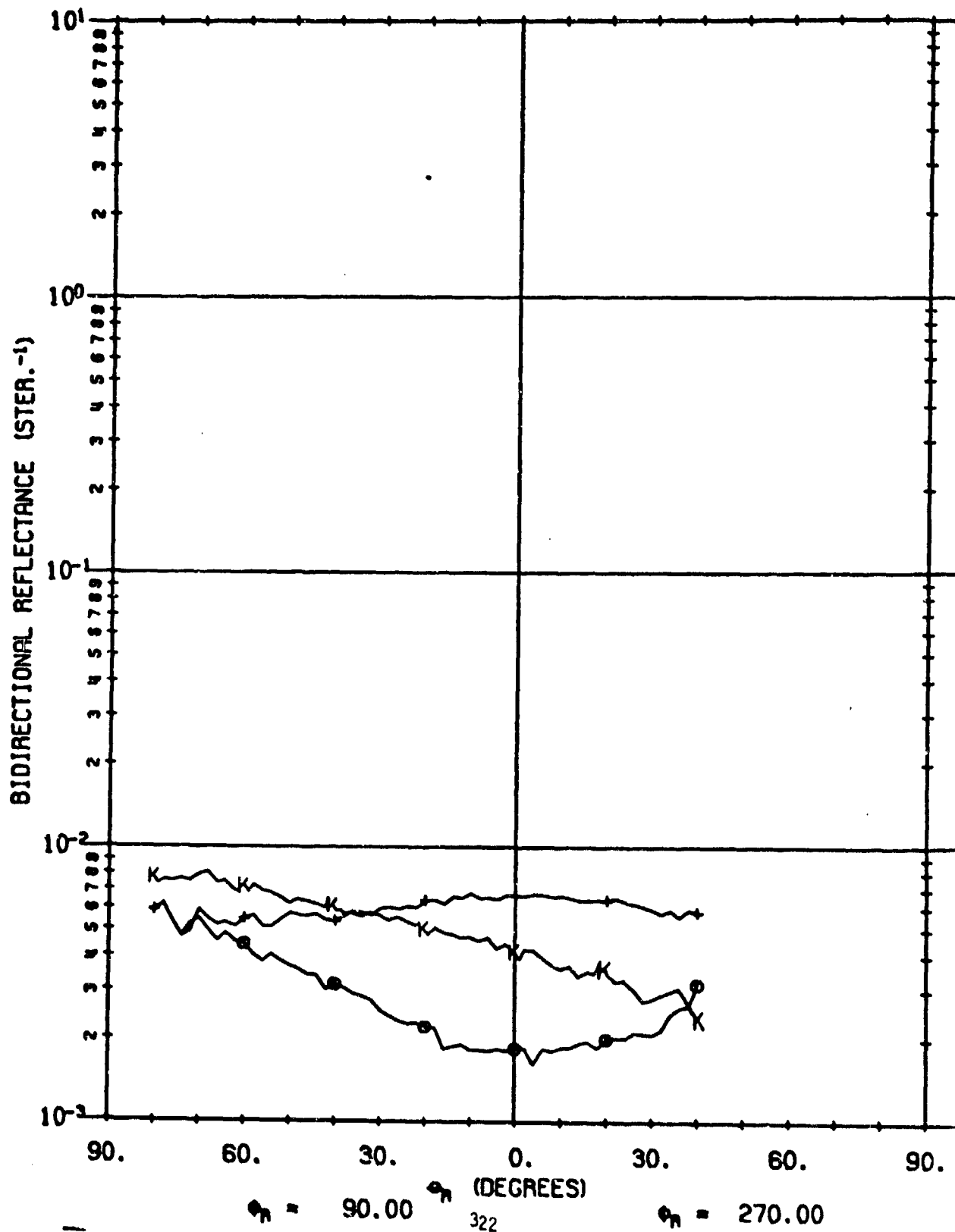
A02023 501

$\lambda = .63$   
 $\phi_i = 60.0$   
 $\phi_i = 180.0$



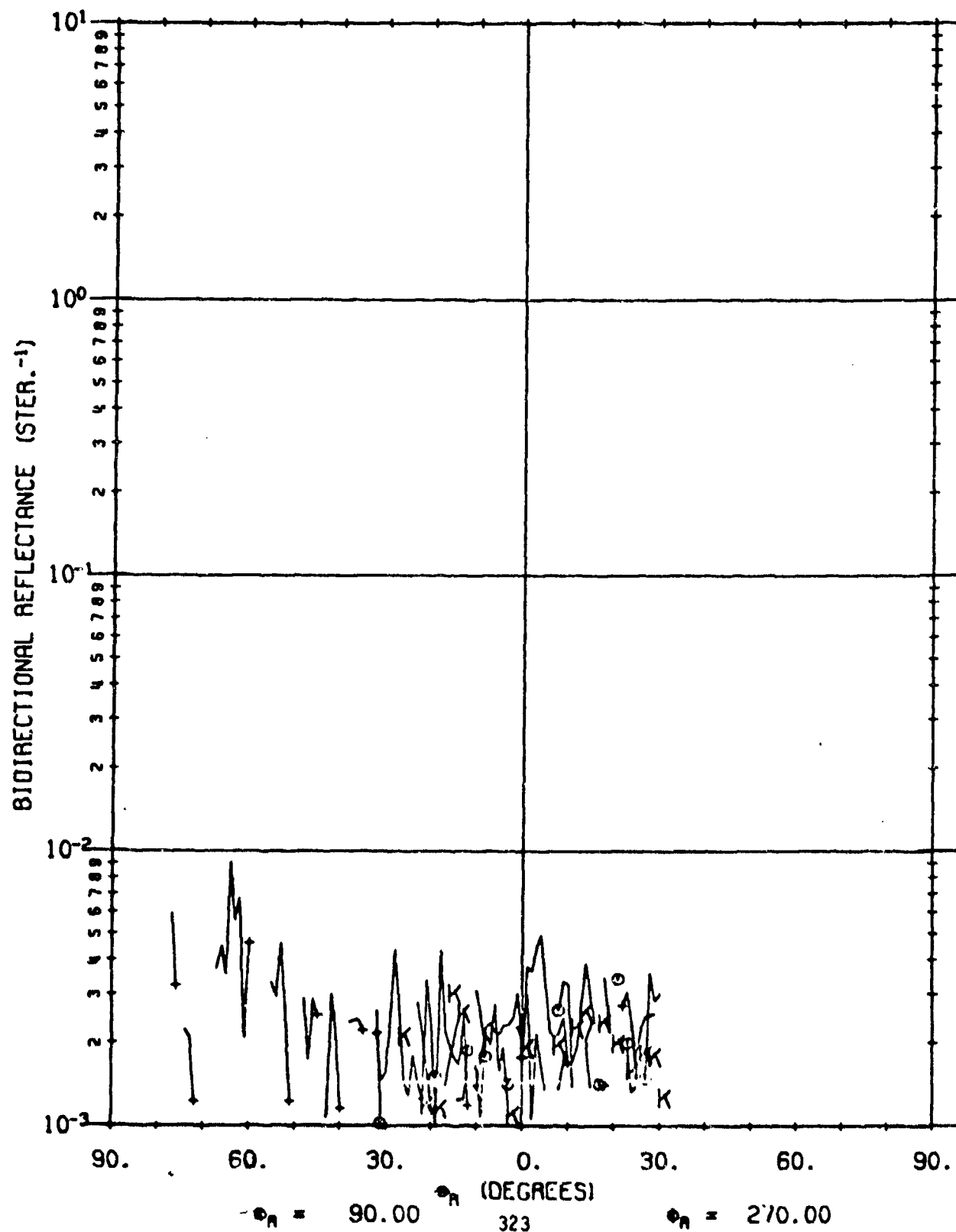
A02023 101

$\lambda = 1.06$   
 $\phi_i = 60.0$   
 $\phi_j = 180.0$



A02023 702

$\lambda = 3.39$   
 $\phi_i = 60.0$   
 $\phi_i = 180.0$



A02023 602

$\lambda = 10.60$   
 $\phi_i = 60.0$   
 $\phi_f = 180.0$

